

Fifth Aerodynamics Prediction Challenge (APC-V)  
2018/07/01, Tokyo



# Unsteady Aerodynamic Prediction of 30P30N Using Hierarchical Cartesian Mesh and Adaptive Mesh Refinement

○ SUGAYA Keisuke, SHU Kembun, IMAMURA Taro  
(The University of Tokyo)

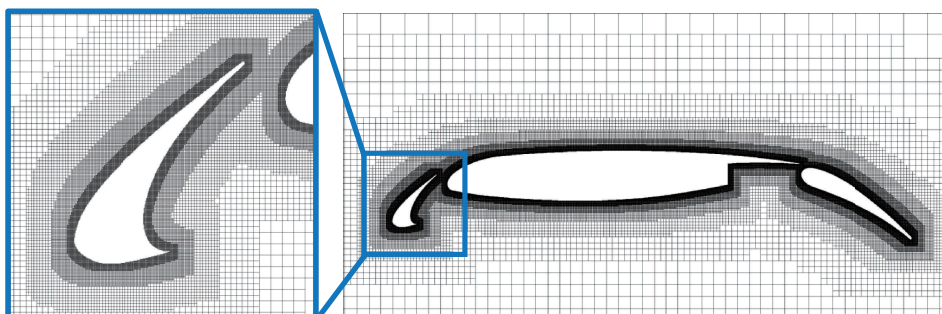
YOSHIHARA Tamaki  
(Tohoku University)



## Cartesian Grid method



- UTCart (The **U**niversity of **T**okyo **C**artesian grid based automatic flow solver)
    - Easy resolution control around the wall boundary.
    - Controlling spatial resolution is sometimes difficult.
      - Unsteady Simulation with AMR → Regenerating grids is needed.
      - Manual refinement → Empirical knowledge is needed.
- ⇒ **New approach is needed.**





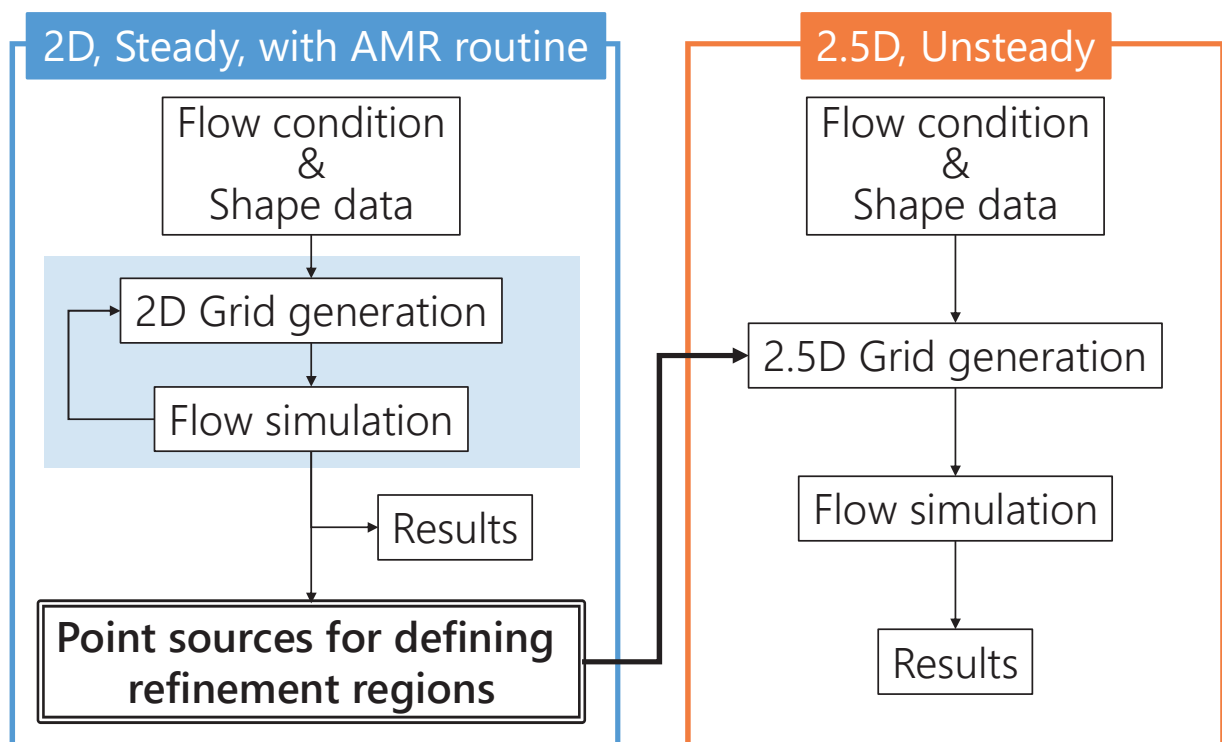
# Objectives

- New workflow for unsteady flow simulation.
  - **2D steady grid generation with AMR**  
+ **2.5D unsteady flow simulation**
    - Without grid regeneration.
    - Without empirical knowledge.
- Examine a potential capability of the proposed workflow.
- Case 1-3 (Unsteady flow), and Case 3-1 (Near field acoustics)
  - 5.5, 9.5 [deg]

3



## Analysis workflow

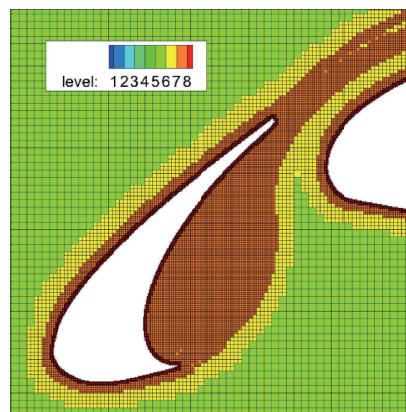
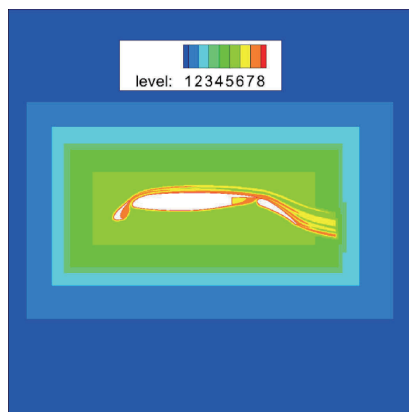


4



## Computational grid

- Unstructured hierarchical Cartesian grid
  - Forest of octrees + Cell-based refinement.
  - Refinement box enclosing the airfoil
    - + [Solution adaptive mesh refinement](#).
- Domain size :  $100 c_{ref} \times 100 c_{ref} \times (2/18) c_{ref}$
- Total Cells :  $18 \times 10^6$  (5.5 [deg]),  $19 \times 10^6$  (9.5 [deg])
- Minimum grid size :  $4.3 \times 10^{-4} c_{ref}$



Cell volume distribution

$$\Delta x = \Delta x_{max} \times 1/2^{level}$$

5



## Numerical method

- Governing equations : RANS (3D)
- Turbulence model : [SA-noft2-DDES-p<sup>\(1\)</sup>](#)
  - RANS region is protected even when the stream-wise grid size is small.
- Wall boundary condition : [Immersed boundary method](#)
  - + [SA wall model<sup>\(2\)</sup>](#)
- Time integration : 3rd order TVD Runge-Kutta
- Spatial accuracy (Inviscid) : [4th order upwind-biased scheme<sup>\(3\)</sup>](#)
- Spatial accuracy (Viscous) : 2nd order central difference

1) 玉置 *et al.*, 第49期 年会講演会講演集, 2018  
 2) Tamaki, and Imamura, AIAA J., Vol 56, 2018.  
 3) 玉置, and 今村, ながれ33, 2014

6



## Case 1-3

# Unsteady flow simulation

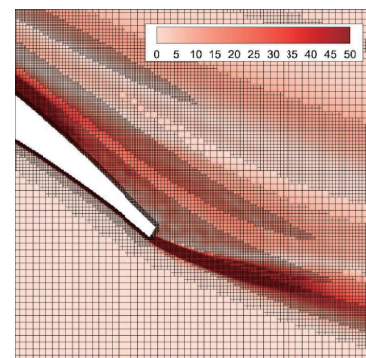
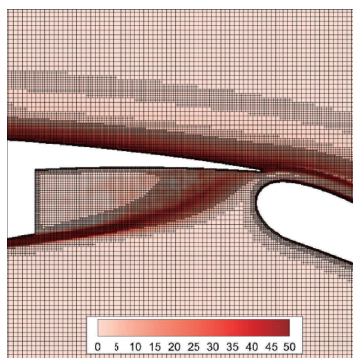
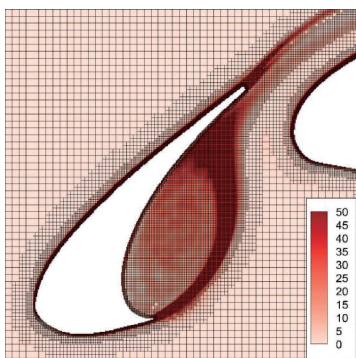
7

## Time averaged flow : Vorticity



- In 2D steady AMR calculations, two indicators are used.
  - Rotation / Entropy
- In 2.5D averaged flow, refined cells are generated where the vorticity magnitude is large.

2.5D, Time averaged flow, 5.5 [deg], Vorticity magnitude

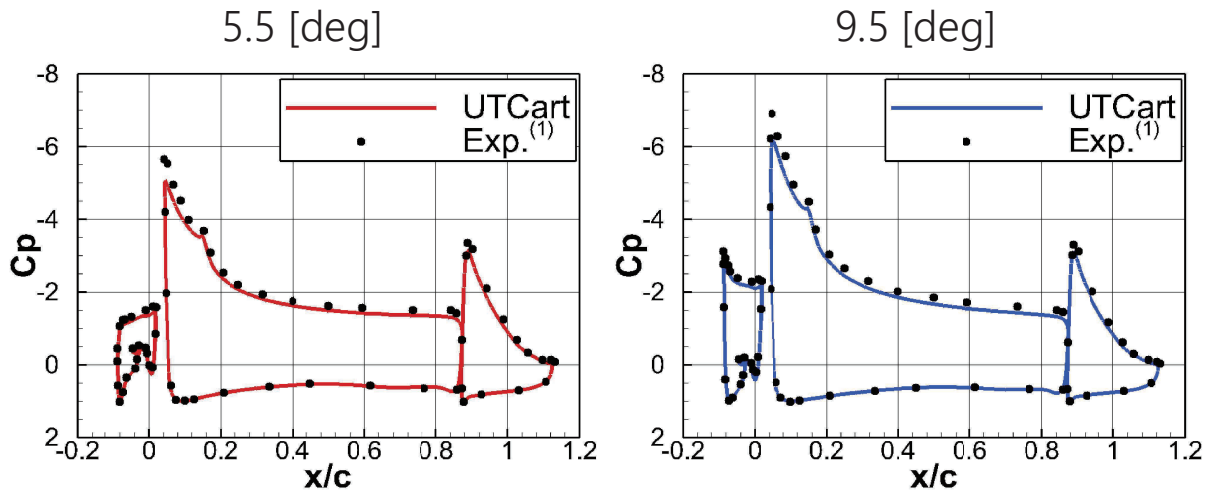


8



## Time averaged flow : $C_p$

- $C_p$  distributions agree with experimental results.



1) Murayama *et al.*, AIAA 2018-3460, 2018

2) Fourth Aerodynamics Prediction Challenge

※ CFD prediction for 5.5, 9.5 [deg] are approximately aligned with wind tunnel measurements at 7.0, 11.0 [deg], respectively.

9



## Time averaged flow : CL

- CL of this study agree with APC-IV result reasonably.
- Time averaged flow is well simulated.**

CL comparison (2.5D unsteady)

AoA (CFD) [deg]	5.5	9.5
Exp. <sup>(1)</sup>	2.9	3.4
Tamaki <i>et al.</i> <sup>(2)</sup>	2.82	3.23
Kojima <i>et al.</i> <sup>(2)</sup>	2.78	3.13
Burns <i>et al.</i> <sup>(2)</sup>	2.86	
Yamamoto <i>et al.</i> <sup>(2)</sup>	2.72	
This study	2.77	3.22

1) Murayama *et al.*, AIAA 2018-3460, 2014

2) Fourth Aerodynamics Prediction Challenge

※ CFD prediction for 5.5, 9.5 [deg] are approximately aligned with wind tunnel measurements at 7.0, 11.0 [deg], respectively.

10



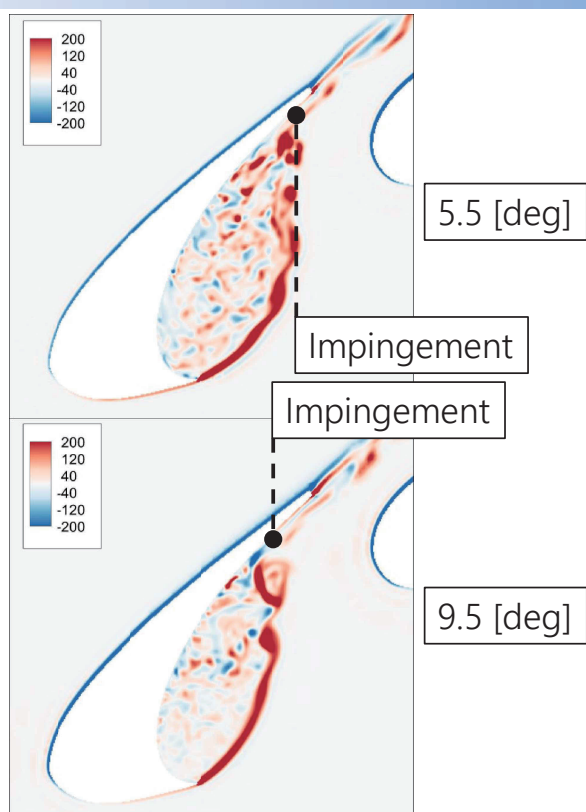
## Case 3-1

### Near field acoustics

11



### Instantaneous flow : Vorticity



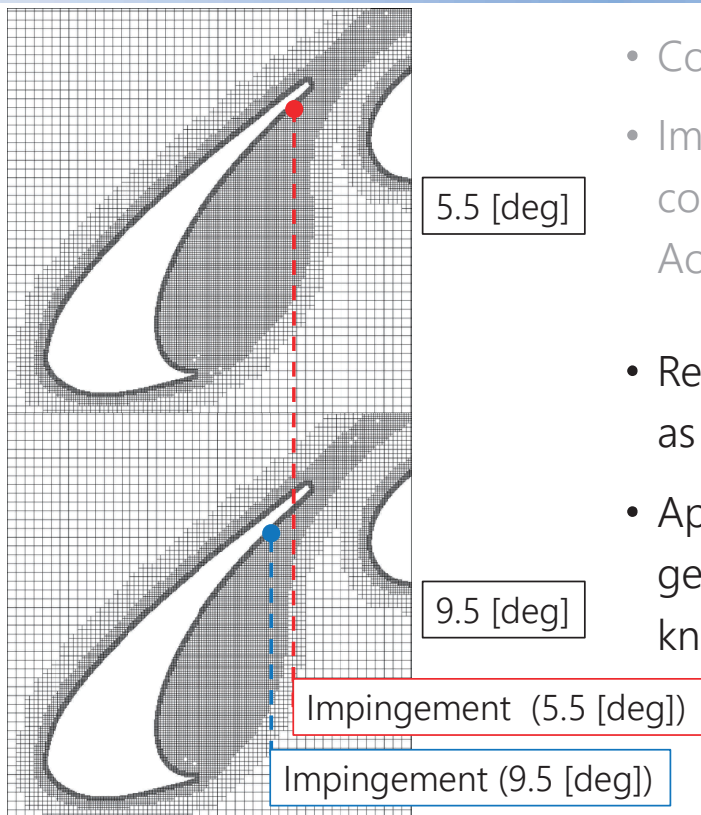
- Contours of span-wise vorticity.
- Impingement point in the slat cove moves upstream when AoA increases.
- Refined cells also move as well as impingement point.
- Appropriately refined grids are generated without empirical knowledge.

12





# Instantaneous flow : Vorticity

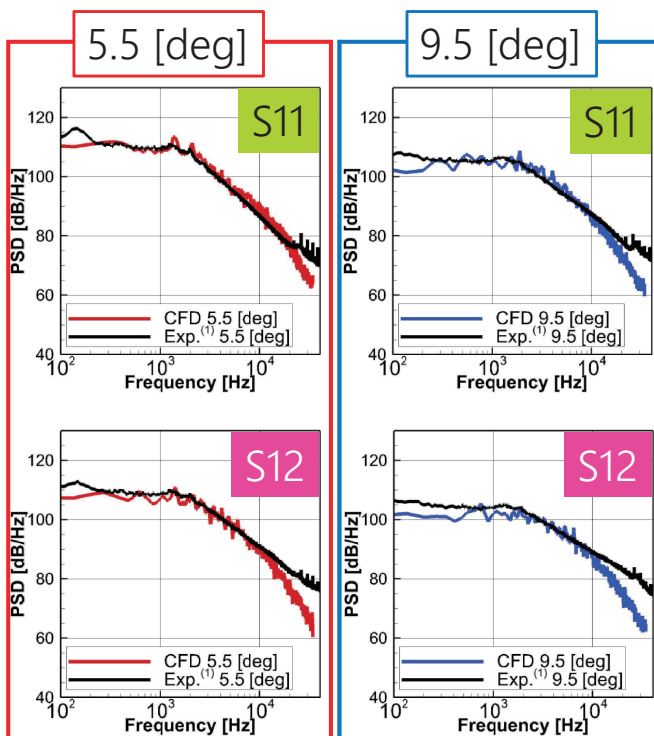


- Contours of span-wise vorticity.
- Impingement point in the slat cove moves upstream when AoA increases.
- Refined cells also move as well as impingement point.
- Appropriately refined grids are generated without empirical knowledge.

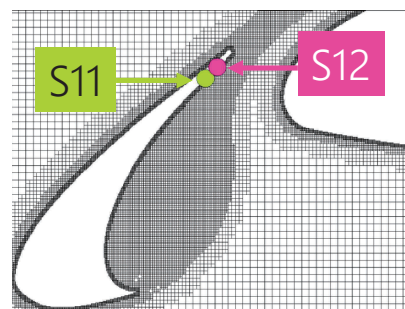
13



# PSD of surface pressure : S11 and S12



- **Good agreement with experimental results.**
- PSD levels of 9.5 [deg] are lower than those of 5.5 [deg].
- Impingement point moves upstream.

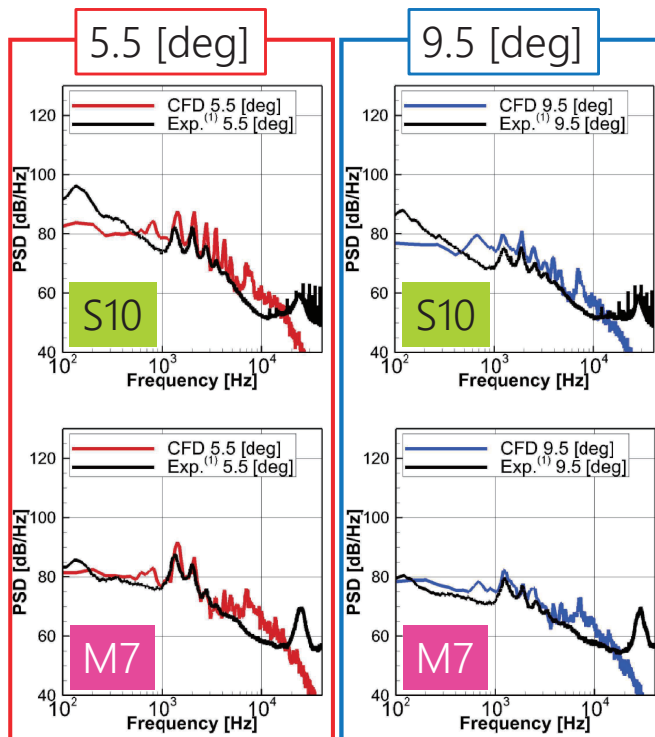


1) Murayama *et al.*, AIAA 2018-3460, 2018

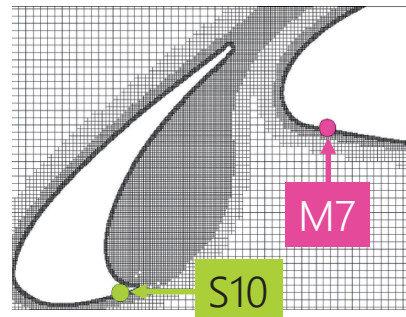
14



## PSD of surface pressure : S10 and M7



- CFD overestimates NBPs level (1kHz~10kHz).
  - The size of the grid is equivalent to L2 provided grid.
- Peaks around 7kHz are calculated.



1) Murayama *et al.*, AIAA 2018-3460, 2018

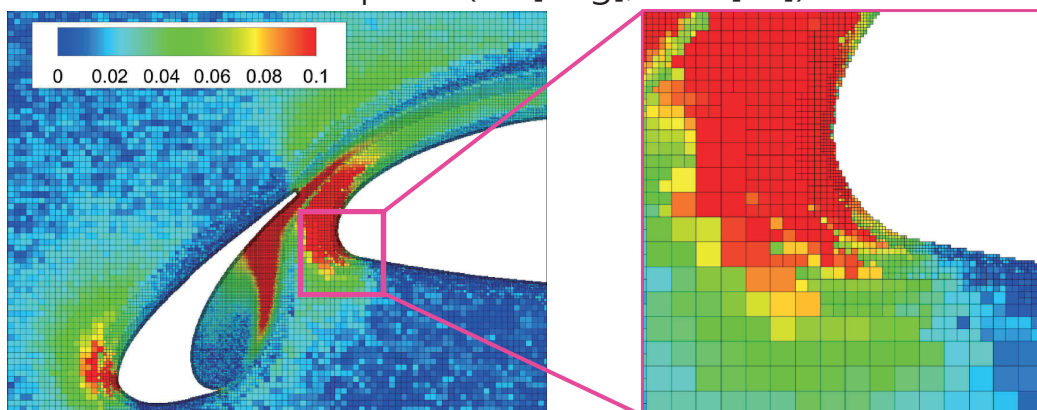
15

## RMS of $C_p$



- $C_p$  RMS is not smooth around hanging-node.
  - Fourth order accuracy in uniform region and 2nd order on hanging-node.
  - Negatively affect the PSDs prediction?
- Should be compared with the results of uniformly refined grids.

$C_{prms}$  (9.5[deg], Z=1 [in.])



16





## Conclusions

---

- Unsteady flow simulation was conducted by using UTCart.
  - 2D steady, AMR + 2.5D unsteady flow simulation.
  - Spatial resolution can be controlled automatically.
- Time averaged flow is well simulated.
  - $C_p$  distributions agree with the experimental data.
  - $CL$  values agree with APC-IV results.
- Necessary to compare with the results of uniformly refined grids.
  - PSDs in slat cove agree with experimental results.
  - Peaks around 7kHz are calculated at slat cusp and main wing .