CflowによるCRM-HLの検証解析 - 格子解像度の影響・安田 英将, 澤木 悠太, 山内 優果, 浅野 宏佳 (川崎重工)

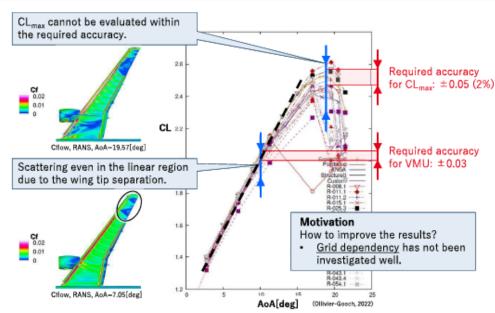


Motivation Computational Setups

Case5 (RANS, AoA=7.05[deg])

Case3 (DDES, AoA=19.57[deg]) Summary

Motivation



Lift curve of CRM-HL, M=0.2, RANS @ AIAA HLPW-4(2022)

Motivation

Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary

Computational cases

Grid dependencies are focused on.

- 1. Case 5: Required grid resolution for RANS simulation is investigated.
- 2. Case 3: Grid resolution effects in DDES are evaluated.

Because DDES requires grid resolution of at least enough for RANS to resolve the flow field, the required grid resolution is investigated in the Case 5.

Computational cases

Grid(*1)	HLPW-4 No. (*2)	Туре	Case 5		Case 3	
Griu.			7.05[deg]		17.05[deg]	19.57[deg]
Cflow-C1	140.C	Hex	0	Λ		
Cflow-C2	N/A	Hex	0	11		
Cflow-C3	N/A	Hex	0	Ш	0	0 🚓
Cflow-C6	N/A	Hex	0	1	0	0
ANSA-C	101.C	Hex	0	ľ		
PW-A	1.3.A	Tet+Prism	0	Ш		
PW-C	1.3.C	Tet+Prism	0	Į,		
JAXA-C	240.C	Tet+Prism	0	V		

- (*1) "-A" or "-C" represent grid levels defined in the HLPW-4 gridding guidelines.
 (*2) Provided in the HLPW-4 web site: https://hillittpw.larc.nasa.gov/Workshop4/grids_downloads.html

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Vation Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary Numerical methods

Numerical methods used in Cflow are summarized in the table below.

- RANS simulation was started from uniform flow condition (cold start).
- DDES was started from RANS results at the same flow condition (warm start).

Numerical methods

	Case 5 (RANS)	Case 3 (DDES)			
Governing equations	Compressible Reynolds-averaged Navier-Stokes equations				
Spatial discretization	Cell-centered finite volume method				
Flux reconstruction	2nd-order accurate reconstruction based on MUSCL				
Gradient	Green-Gauss				
Inviscid flux	Simple low-dissipation AUSM scheme (SLAU)				
Slope limiter	minmod				
Viscous flux	2nd-order accurate central difference				
Turbulence modeling	SA-neg	SA-neg-based Delayed Detached Eddy Simulation (DDES)			
Time integration	Matrix-free Gauss Seidel (MFGS) implicit method				
	local time-stepping method	1st order, dt=0.01[-] (CFL≈1 around bracket wake region)			

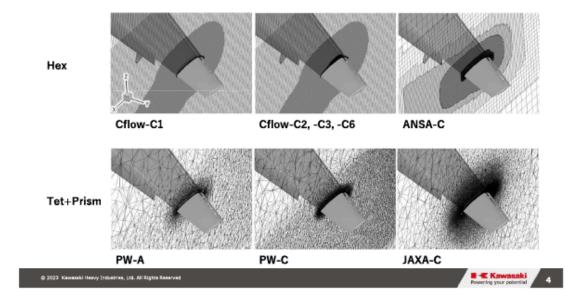
Motivation

Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary

Computational grids

Effects of both grid type and grid resolution are investigated.

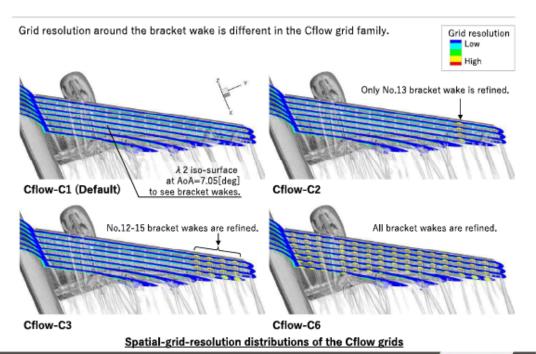
- Hex-dominant: 5 types, Tet+Prism: 3 types
 - Cflow-C2, -C3, and -C6 have finer grid around bracket wake than Cflow-C1. (→Next slide.)
- Spatial grid resolution is different even in the same grid level C.

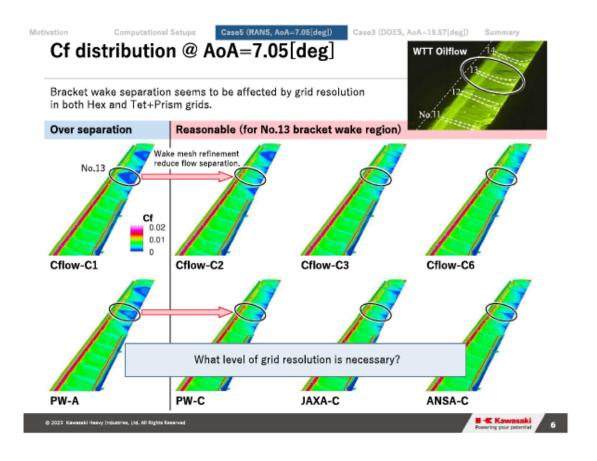


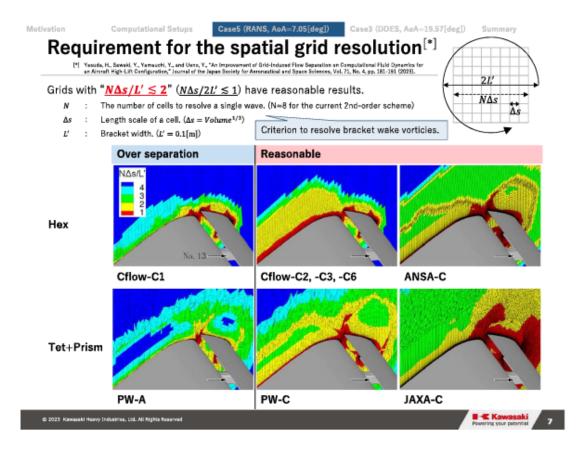
Computational grids — Cflow-grid family

Case (RANS, AoA=7.05[deg]) Case (DDES, AoA=19.57[deg]) Summary

Computational grids — Cflow-grid family



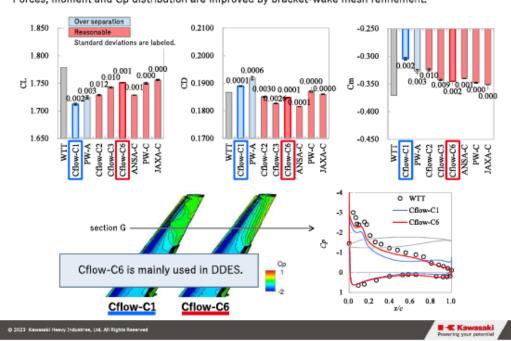




Motivation Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary

Forces, Moment, Cp distribution

Forces, moment and Cp distribution are improved by bracket-wake mesh refinement.



Motivation Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary

DDES at AoA=19.57[deg]

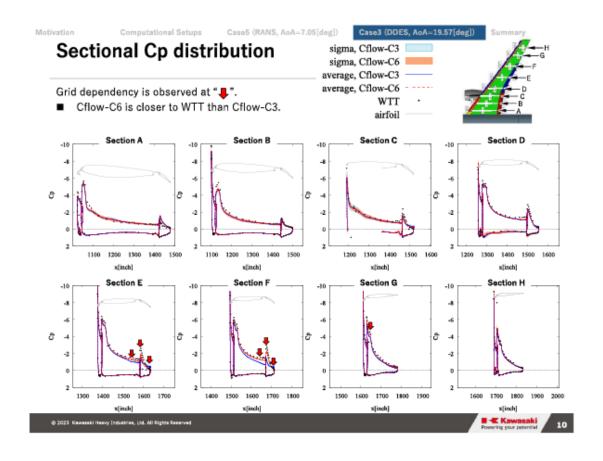
CL, CD, and Cm of Cflow-C3/-C6 are compared to WTT results. ■ Cflow-C3 underestimates CL_{max} by approximately 4%. Cflow-C6 has closer results than Cflow-C3. CL improves to the level of the required accuracy (2%). CD and Cm also improve. → The bracket wake's grid resolution is important for CL_{max} estimation. 2.70 2.70 2.70 Required accuracy ±0.05 (±2%) for CL 2.60 2.60 2.50 2.50 2.50 **2.40** 당 2.40 당 2.40 2.30 2.30 2.30 -EXP(corrected) 2.20 Cflow-C3 2.20 2.20 Cflow-C6 2.10 2.10 2.10 -0.4 -0.35 -0.3 -0.25 -0.2 -0.15 -0.1 10 12 14 16 18 20 22 24 0.2 0.25 0.3 0.35 0.4 0.45 0.5 AoA, deg CD Cm AoA=17.05[deg] is also shown for Cflow-C3 as a reference.

CL, CD, and Cm are averaged in 10000step (flow through approximately 2.8*MAC).
 Each CFD result is plotted with standard deviation.

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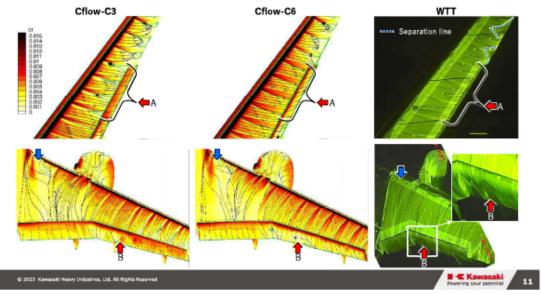


Vation Computational Setups Case5 (RANS, AoA=7.05[deg]) Case3 (DDES, AoA=19.57[deg]) Summary

Mean surface flow at AoA=19.57[deg]

Mean Cf and surface stream line are compared to WTT oilflow.

- Wake refined grid (Cflow-C6) captures flow separation more precisely. (♣ A, B)
 - Cflow-C3 overestimate flow separation around bracket wakes (A) and underestimate around flap (B).
- Surface flow at LE of wing root does not match WTT. (



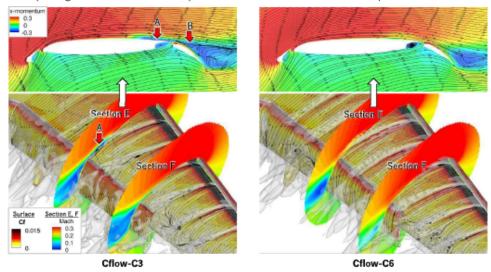
Motivation

Case5 (RANS, AoA=7.05[deg])

Case3 (DDES, AoA=19.57[deg]) Summary

Flow fields around section E, F

- Wake refined grid (Cflow-C6) captures bracket wakes well.
- Bracket wake separation (A) affect flow field over the flap (B).
- Capturing bracket wake is also important for the flow field around the flap.



Surface Cf, streamline, Section Mach (E, F), & 2 iso-surface

Motivation

Computational Setups

Case5 (RANS, AoA=7.05[deg])

Case3 (DDES, AoA=19.57[deg]) Summary

Summary

Case 5: Required grid resolution in RANS at AoA=7.05[deg]

- Flow field could be well captured by bracket wake refinement.
- Grids satisfying a criterion " $N\Delta s/L' \lesssim 2$ " ($N\Delta s/2L' \lesssim 1$) showed reasonable agreement with the WTT flow fields around the wing tip.

The number on cells to resolve a single wave. $(N \approx 8 \text{ for the current 2nd-order scheme})$ Length scale of a cell. ($\Delta s = Volume^{1/3}$) Δs

Bracket width. (L' = 0.1[m])

Case 3: Grid resolution effects in DDES at AoA=19.57[deg]

- Bracket wake refined grid showed better results for both the aerodynamic coefficients and flow fields.
- The grid resolution criterion seems to be effective for DDES.

Enough grid resolution to capture bracket wakes is important for both RANS and DDES to improve the simulation accuracy.

