階層型直交格子流体ソルバUTCartによる風洞壁を含むCRM-HL周り流れの定常RANS解析・ 玉置 義治 (東北大), 横山 悠人, 今村 太郎 (東大)

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#### 1A04

## 階層型直交格子流体ソルバUTCartによる 風洞壁を含むCRM-HL周り流れの定常RANS解析

#### 東京大学大学院

○ 玉置義治 横山悠人 今村太郎



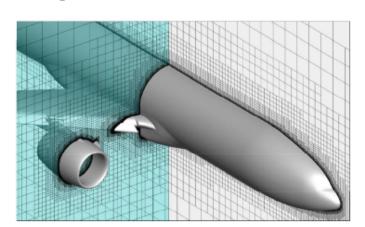
#### **UTCart**

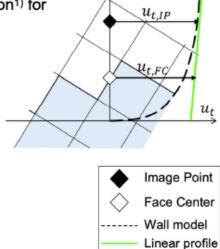




(The University of Tokyo Cartesian-grid-based automatic flow solver)

- Hierarchical Cartesian grid (cell-based refinement)
  - · Automatic and robust grid generation
  - · Orthogonality of the grid
  - Immersed boundary method with a wall function<sup>1)</sup> for high-Re flows





1) Tamaki, Harada, and Imamura, AIAA J., Vol 55, 2017.

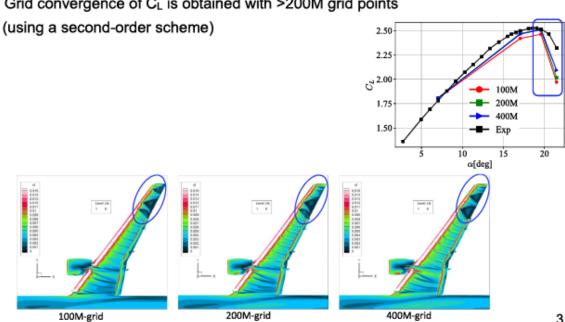
### **UTCart in APC-8**





(Funada, Imamura, & Sugaya)

- · Free-air cases were simulated with three different grid resolutions
- · Grid convergence of C<sub>L</sub> is obtained with >200M grid points

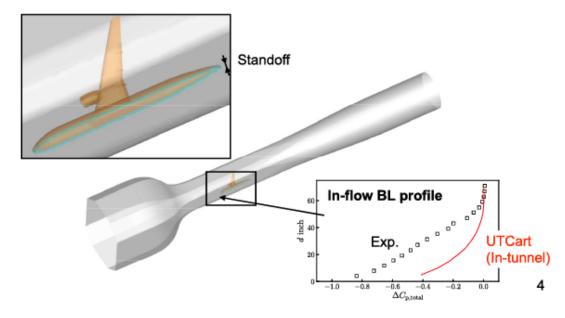


### Objective





- Demonstrate capability of UTCart for complex in-tunnel flow geometries
- · Evaluate effects of tunnel wall / floor boundary layer / standoff



### Numerical methods/ grids



Governing Equation	RANS	
Turbulence Model	SA-noft2	
Inviscid Flux	4 <sup>rd</sup> -order upwind biased <sup>3)</sup> + SLAU	
Viscous Flux	2 <sup>nd</sup> -order central difference	
Time Integration	MFGS (Local Time Stepping)	
Wall Boundary Condition	IB+SA wall model	
Distance between IP and wall	3∆x	

• Minimum cell size: 0.26 inch ( $C_{\rm ref}/1024$ )

· # of cells: 114~119 M

3) Tamaki and Imamura, Computers & Fluids, Vol 144, 2017.

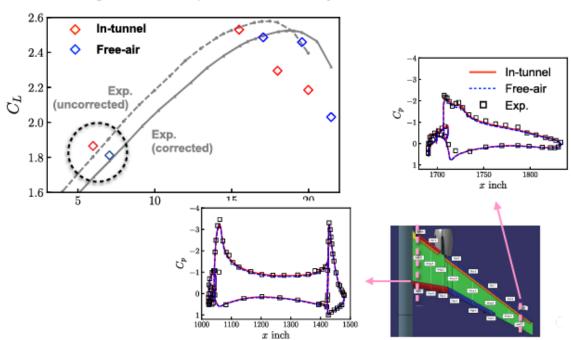
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### Results at low-AoA





· Lift at low angle of attack is predicted accurately



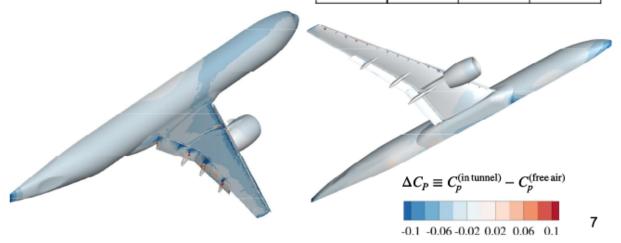
#### Tunnel effects at low AoA





$\alpha_{ m uncorrected}$ =	= 5.98°
$\alpha_{\text{corrected}} =$	

	$\Delta C_D$	$\Delta C_L$	$\Delta C_M$
CFD	-0.032	0.045	-0.001
Exp.	-0.033	0.025	-0.005

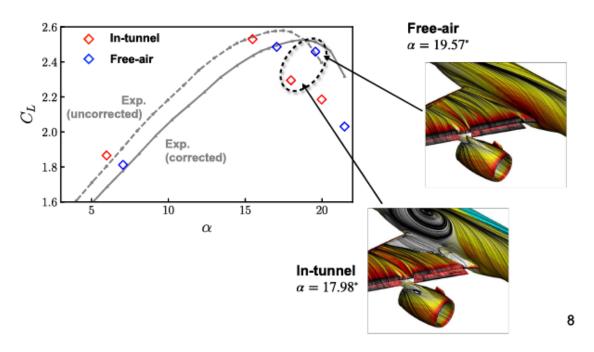


# Stall prediction





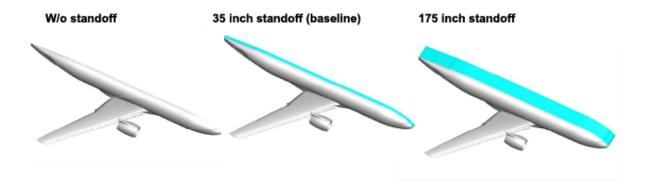
Stall AoA differs between the free-air/in-tunnel simulations



#### Floor BL / standoff height



- Several additional cases are conducted at  $\alpha_{\rm uncorrected}=17.98^{\circ}$  to clarify the causes of the different stall behaviors
- . Simulations are conducted with/without the floor BL

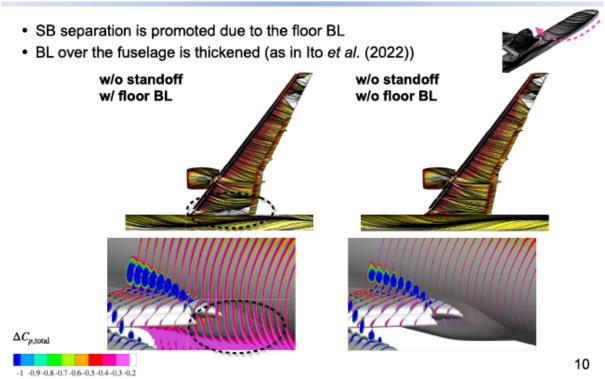


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#### Effects of floor BL



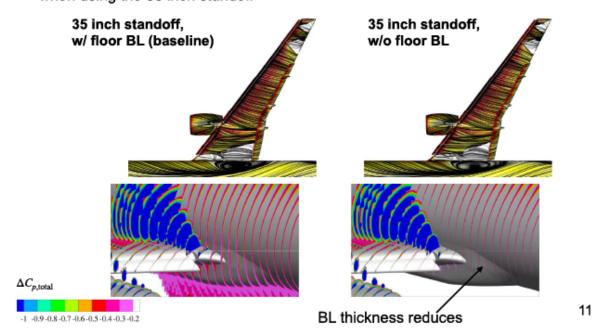




#### Effects of floor BL



 Contrary to expectations, the floor BL does not make almost any difference when using the 35 inch standoff

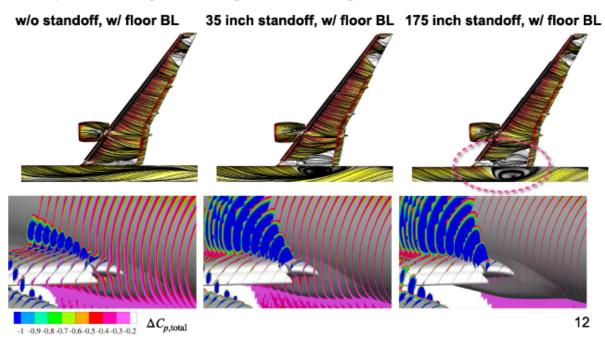


## Effects of standoff height





· Separation enlarges with a higher standoff height

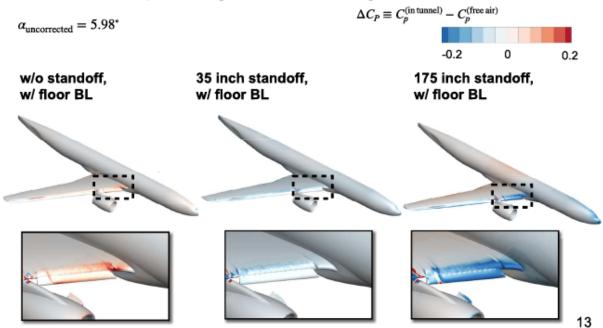


## Effects of standoff height





· Inboard suction peak strengthens as standoff height increases



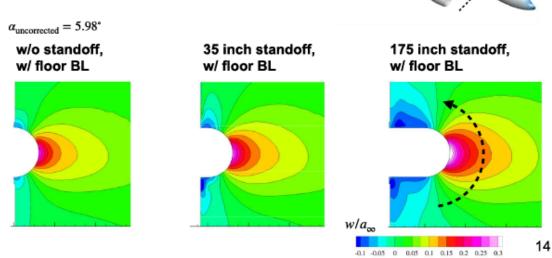
# Effects of standoff height





- · Effective AoA increases due to the fuselage
- → Separation in the inboard region is promoted

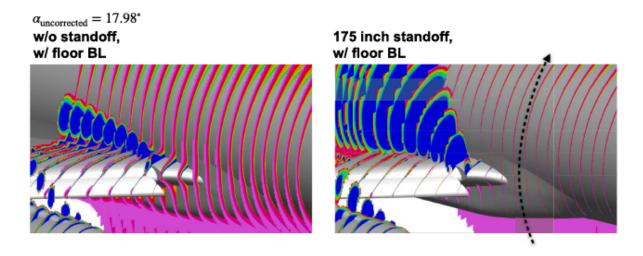




### Effects of standoff height



- · Effective AoA increases due to the fuselage
- → Separation in the inboard region is promoted



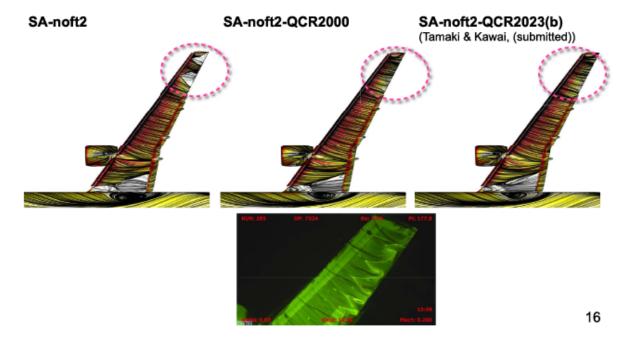
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## Sensitivity to turbulence model 🔧 東京大学





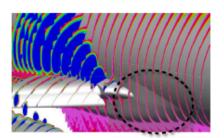
Turbulence model has certain influences on the separation pattern

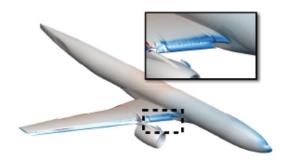


#### Conclusions



- UTCart has been successfully applied to the in-tunnel flow simulations
- Except for the stall conditions, the CFD simulations well predict the aerodynamics including tunnel effects
- · Half-span model experiment introduces twofold effects on the stall
  - Floor BL thickens the BL over the fuselage
  - Standoff increases the effective AoA in the inboard region
- Turbulence model should be improved further for accurate stall prediction





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