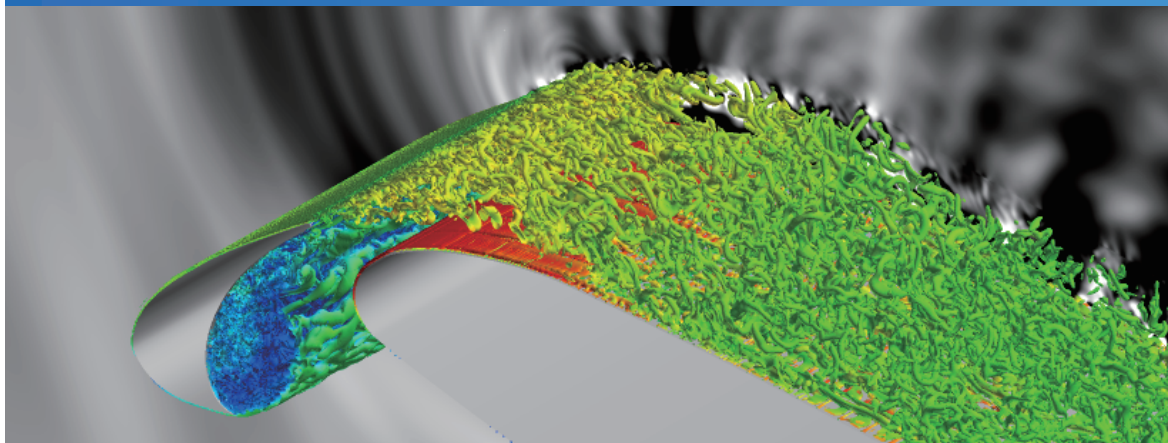


APC4@36<sup>th</sup> ANSS

# Unsteady Flow Simulation around 30P30N by Cascaded LBM



Takashi ISHIDA

Numerical Simulation Research Unit  
Japan Aerospace Exploration Agency

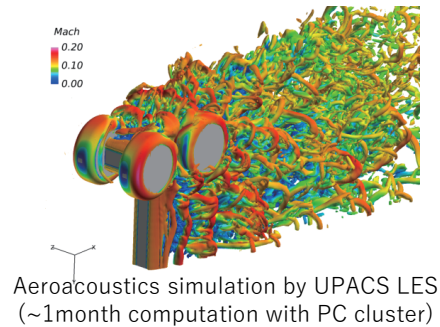
## Outline

- Numerical Method
  - Lattice Boltzmann Method
    - Cascaded LBM
  - Boundary condition
    - Wall boundary
    - Outer boundary
  - Building-Cube Method
  
- Numerical Results
  - Problem category 1-1 (2D)
  - Problem category 1-3 (3D)
  - Problem category 3-1 (3D)
  
- Conclusions

# Background

- CFD use :
  - understanding the flow physics
  - engineering design (especially in steady state)

- Problems in current CFD
  - Cost for unsteady flow simulation
    - High resolution/High order schemes
    - Restriction for  $\Delta t$
    - Inner iteration of implicit time integration
    - Handling of massive output data
  - Model dependency
    - DES, DDES, IDDES, Zonal DES, ...
    - RANS/LES switching parameter



- It is difficult to directly apply unsteady flow simulation for engineering design.
- Lattice Boltzmann Method has capability to overcome current CFD problem (?)

# Algorithms of LBM

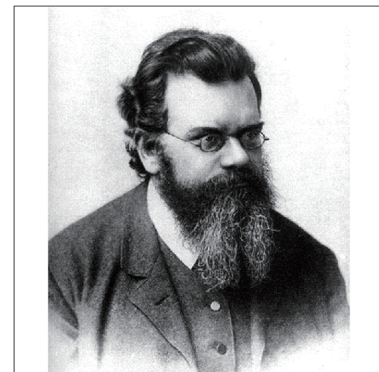
- Governing equation: Boltzmann transport equation

$$\frac{\partial f_i}{\partial t} + \mathbf{e}_i \cdot \nabla f_i = \Omega_i \quad (i = 1, \dots, b)$$

- $f$  : probability distribution function
- $\mathbf{e}$  : discrete set of velocities
- $\Omega$  : collision operator

- Discretization on lattice:

$$f_i(\mathbf{r} + \mathbf{e}_i dt, t + dt) = f_i(\mathbf{r}, t) + dt \times \Omega_i(f_1, \dots, f_b) \quad (i = 1, \dots, b)$$



Ludwig Eduard Boltzmann  
(1844–1906)

- Lattice model used in this research: D2Q9, D3Q27

# Algorithms of LBM

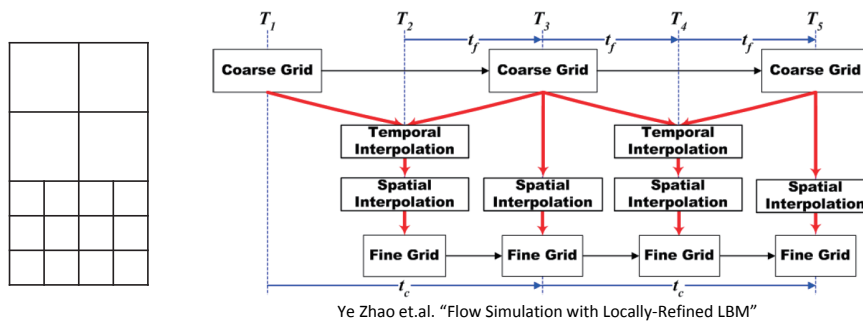
- Relaxation parameter  $\tau$  depends on the local grid size  $\Delta x$ .

- $\frac{\Delta x_{coarse}}{\Delta x_{fine}} = n$  leads  $\frac{\Delta t_{coarse}}{\Delta t_{fine}} = n$

- Temporal/spatial interpolation are necessary among difference size cells.

- Usually, non-equilibrium part of  $f$  is rescaled.

$$f_i^{fine} = \hat{f}_i^{eq,coarse} + (\hat{f}_i^{coarse} - \hat{f}_i^{eq,coarse}) \frac{\Delta x_{fine} \tau_{fine}}{\Delta x_{coarse} \tau_{coarse}}$$



Ye Zhao et.al. "Flow Simulation with Locally-Refined LBM"



# Algorithms of LBM

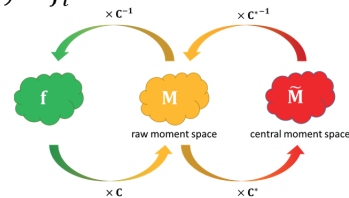
- Cascaded LBM is used for collision operator.

- Satisfy Galilean invariance and has better accuracy/stability
  - Compute central moment defined by moving coordinate:

$$\tilde{M}_{p,q,r} = \sum_i (e_{ix} - u_x)^p \cdot (e_{iy} - u_y)^q \cdot (e_{iz} - u_z)^r \cdot f_i$$

- Relation between Raw moment/Central moment

$$\tilde{M} = C^* M$$



- 27 Central moments used in this research:

$$M_\rho, M_x, M_y, M_z, K_{xy}, K_{xz}, K_{yz}, K_{xx-yy}, K_{xx-zz}, K_{xx+yy+zz}, K_{xyy+zz}, K_{xxy+zz}, K_{xxz+yyz}, K_{xyy-zzz}, K_{yzz-xyy}, K_{xxx-yyy}, K_{xyz}, K_{xxyy+xxzz+yyzz}, K_{xxyy+xxzz-yyzz}, K_{xxyy-xxzz}, K_{xxyz}, K_{xyyz}, K_{xyzz}, K_{xyyzz}, K_{xxyzz}, K_{xxyyzz},$$

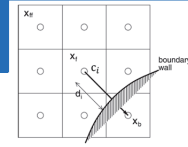
and  $K_{xxyyzz}$ .

- $\tau = 1$  is used for the above moments to enhance stability.
  - Our approach is **Implicit LES**.

Martin Geier, et. al., "Cascaded digital lattice Boltzmann automata for high Reynolds number flow"



# Wall/Outer boundary



- Interpolated Bounce-Back (IBB) Scheme (1<sup>st</sup> order)

$$f_{-i}(\mathbf{x}, t + \Delta t) = 2q\tilde{f}_i(\mathbf{x}, t) + (1 - 2q)\tilde{f}_i(\mathbf{x} - \mathbf{c}_i\Delta t, t) - 2w_i\rho(\mathbf{x}, t)\frac{\mathbf{e}_i \cdot \mathbf{u}_w}{c_s^2} \quad \left(q_i < \frac{1}{2}\right)$$

$$f_{-i}(\mathbf{x}, t + \Delta t) = \frac{1}{2q}\tilde{f}_i(\mathbf{x}, t) + \frac{2q - 1}{2q}\tilde{f}_{-i}(\mathbf{x}, t) - \frac{1}{q}w_i\rho(\mathbf{x}, t)\frac{\mathbf{e}_i \cdot \mathbf{u}_w}{c_s^2} \quad \left(q_i \geq \frac{1}{2}\right)$$

where  $q_i = \frac{d_i}{|\mathbf{c}_i|\Delta t}$ , non-dimensional distance

※No wall function is used.

G. Eitel-Amor et.al. "A lattice-Boltzmann method with hierarchically refined meshes"

- Damping function is used for the outer boundary condition.

$$f^{outer} = f - \alpha * (f - f_{eq}^{target})$$

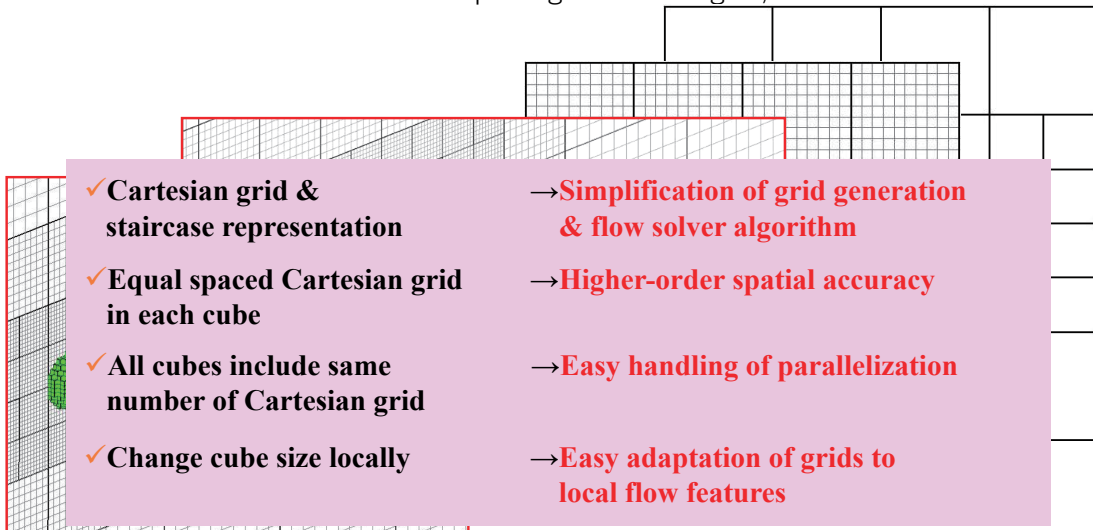
$$\alpha = 0.5 \times \left(\frac{d - r}{R - r}\right)^2$$

where  $r/R$  are inner/outer radius of damping region,  
 $d$  is distance from inner radius  $r$



# Building-Cube Method

- BCM is a block-structured Cartesian grid approach proposed by prof. Nakahashi.
  - Computational domain is divided into "Cubes".
  - Each cube has a uniform-spacing Cartesian grid, "Cells".

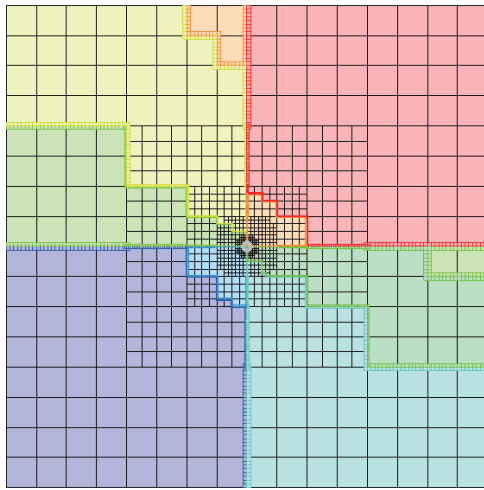


- ✓ Cartesian grid & staircase representation → Simplification of grid generation & flow solver algorithm
- ✓ Equal spaced Cartesian grid in each cube → Higher-order spatial accuracy
- ✓ All cubes include same number of Cartesian grid → Easy handling of parallelization
- ✓ Change cube size locally → Easy adaptation of grids to local flow features

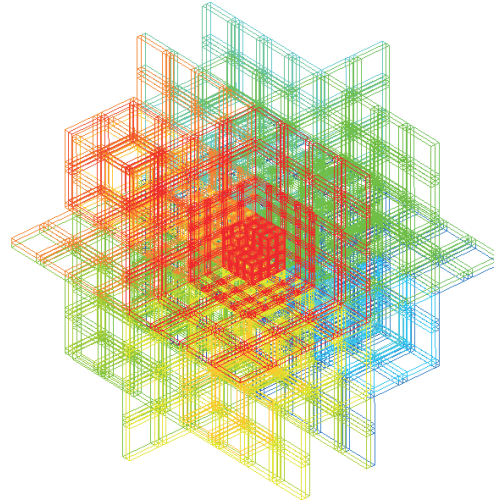


# Domain Partition

- BCM framework use both OpenMP/MPI parallelization.
- Z-ordering is used for MPI parallelization.



2D



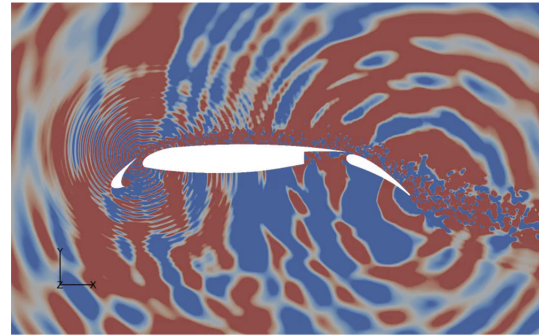
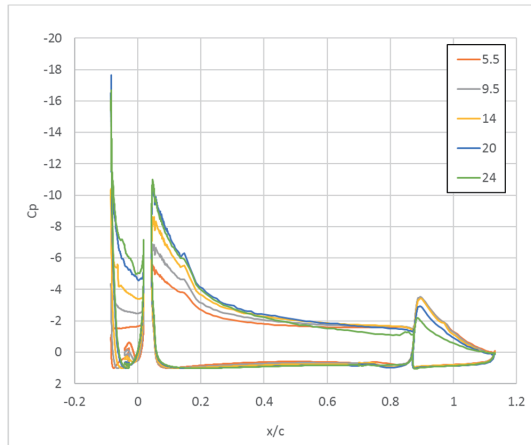
3D

# Grid information

<i>dimension</i>	Details	
	2D	3D
<i>Re</i>	$1.71 \times 10^6$	
<i>M<sub>∞</sub></i>	0.17	
<i>α</i>	5.5	
<i>Domain</i>	$32L_{\infty} \times 32L_{\infty}$	$16L_{\infty} \times 16L_{\infty} \times 0.125L_{\infty}$
<i>Cube</i>	6535	77326
<i>Cell</i>	$32^2$	$4^3, 8^3, 16^3, 32^3$
<i>Total cells</i>	6.7M	4.9M, 40M, 317M, 2.5B
<i>Δx<sub>min</sub></i>	$1.22 \times 10^{-4}L_{\infty}$	$2.44 \times 10^{-4}L_{\infty}$

Periodic boundary condition is applied in spanwise direction.

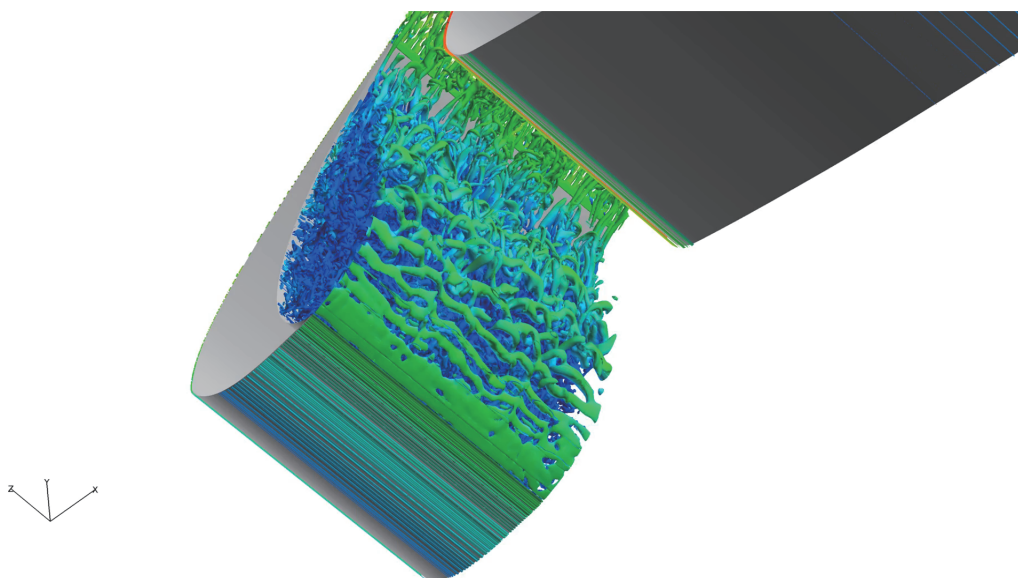
## 2D results



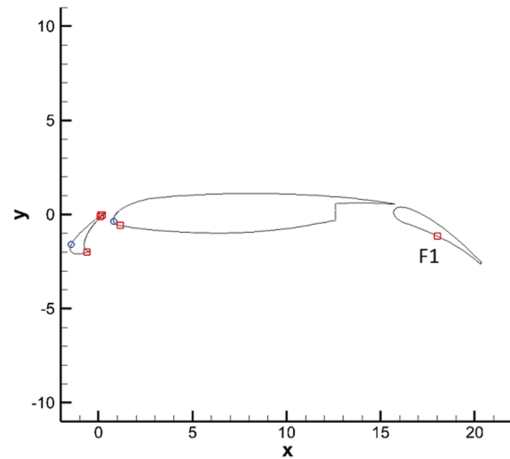
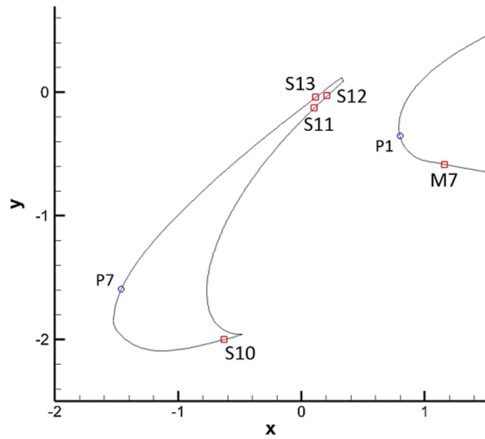
$dp$  field@AoA=5.5

- Flow separation is different at slat-cove compared to NS(RANS) results.  
⇒ due to 2D computation with ILES.
- LBM overestimated  $C_p$  compared to NS(RANS) results.

## 3D results



# PSD data position

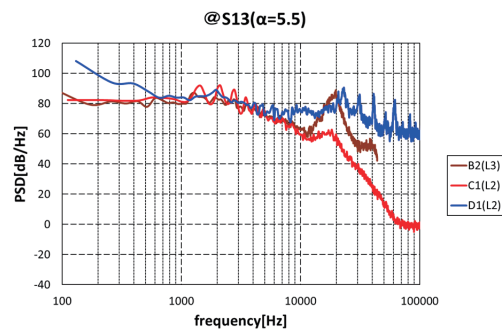
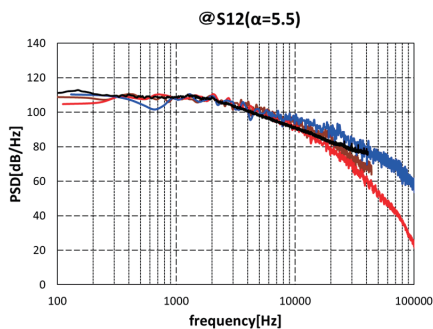
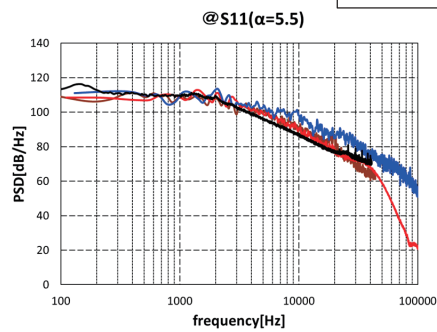
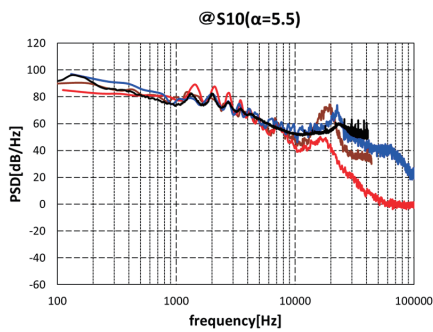


Takashi ISHIDA

13

# PSD comparison

- B2:FaSTAR(L3)
- C1:FaSTAR(L2)
- D1:Present

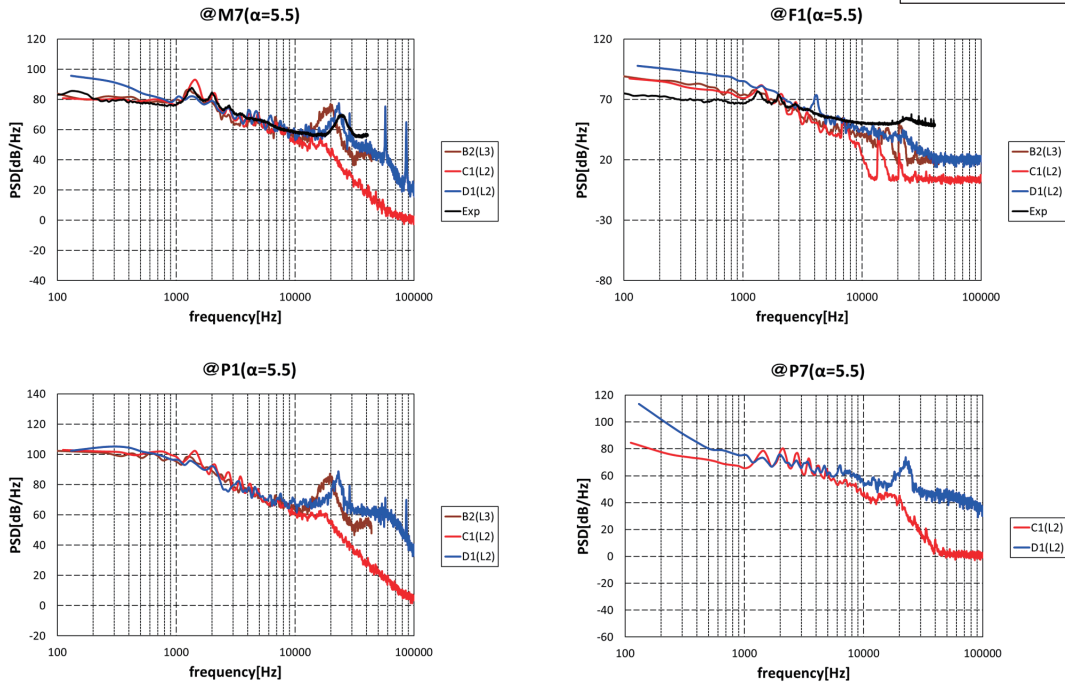


Takashi ISHIDA

14

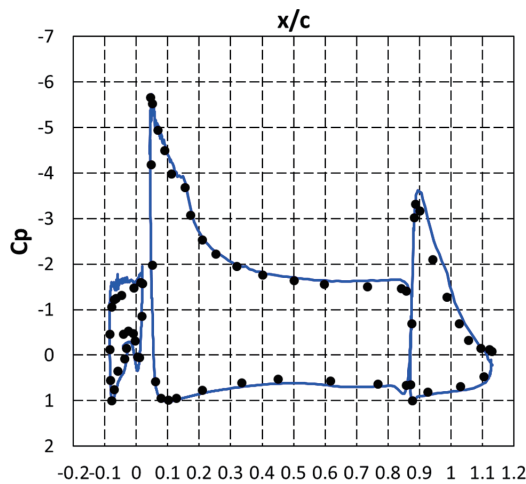
# PSD comparison

— B2:FaSTAR(L3)  
 — C1:FaSTAR(L2)  
 — D1:Present



# Time-averaged Cp

30P30N(α=5.5)

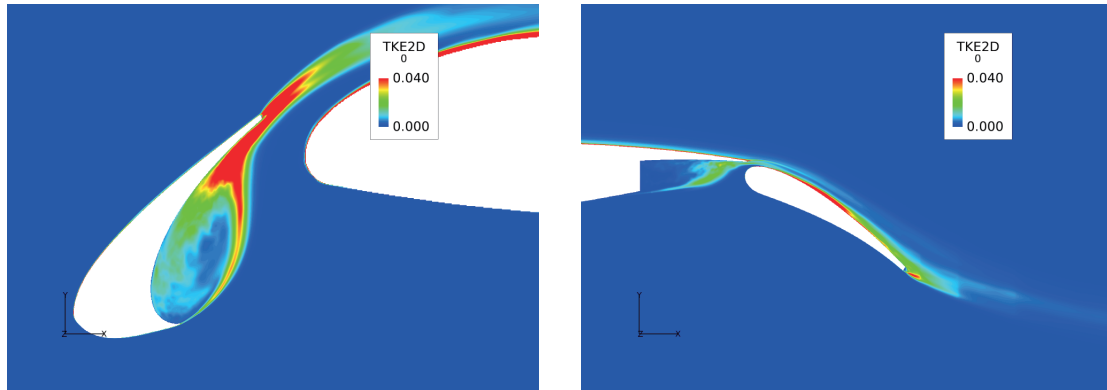


- LBM overestimated Cp at slat and flap ⇒ due to the outer domain size?
- BL thickness at slat-TE may be changed slightly compared other CFD results due to the flow acceleration at flap suction.





# TKE2D

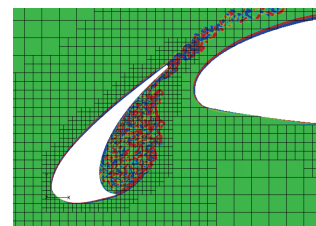


Takashi ISHIDA

17


## Conclusions

- NBPs were well captured by present approach.
- The peak from slat-TE was slightly shifted to higher region compared to NS results, but reasonable agreement was obtained with experimental data.
- Future works
  - Grid convergence
  - Effect of local mesh refinement based on flow field



Takashi ISHIDA

18



Thank you for your kind attention.