Fourth Aerodynamics Prediction Challenge (APC-IV) 4 July 2018



Investigation of Effect of Subgrid Length Scale in DDES through Unsteady Flow Simulation of 30P30N Airfoil (30P30N非定常解析を通した DDESサブグリッド長さスケールの影響調査)

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# **Computations in APC-IV**

### Computational grid

- Provided by JAXA: /apc/grids/3element\_highlift\_airfoil/30P30N\_modified\_slat\_configF/fastar/3D\_L3\_fine\_r1.fsgrid
- **73.6M** cells (**0.27M** cells in 2D x **270** cells in spanwise)
- Spanwise length: 2 inch
- Wall-normal cell spacing on the surface  $\Delta y^+ \sim 0.54$
- Nearly isotropic cells in the slat cove region

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	Computational	cases
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enlarged view of grid at slat cove region

		DI	DES by FaSTA L3 (fine)	R	
Airfoil/Re/Ma	AoA	$\Delta_{max}$	$\Delta_{vol}$	$\Delta_{SLA}$	
30P30N	5.5	1	1	1	課題1-3 課題3-1, 3-2
Re=1.7e6 Ma=0.17	9.5	11	-	-	課題1-3 課題3-1, 3-2
	14		-	-	課題3-1, 3-2

#### present topic: comparison of <u>subgrid length scales</u> in the context of DDES

Investigation of Effect of Subgrid Length Scale in DDES

## Background

#### Length scale definition in DDES

- $L_{DDES} = L_{RANS} f_d \max(0, L_{RANS} L_{LES})$ 
  - $L_{LES} = \Psi C_{DES} \Delta$  subgrid length scale

  - $\Delta = \max(\Delta x, \Delta y, \Delta z) \text{ [Spalart, 1997]}$
- Aeroacoustic simulation around a slat using DDES by UPACS [Murayama, 2015]
  - w/ original definition of  $\Delta$  (= max( $\Delta x, \Delta y, \Delta z$ ))
  - Shear layer development was delayed
  - Narrow band peaks were overestimated

#### New definitions of A have been proposed

- $\Delta_{\omega}$  for Axial jet [Chauvet, 2007]
- $\Delta_{SLA}$  for free shear layer [Shur, 2015]
- Few applications to a high-lift airfoil
- Few systematic comparisons among them

[Murayama, 2015]

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Investigation of Effect of Subgrid Length Scale in DDES

### Objective

To evaluate the effect of subgrid length scale in DDES for aerodynamic and aeroacoustic analysis of 30P30N airfoil

mainly on slat 



## Definitions of subgrid length scale in DDES

- Length scale definition in DDES
  - $L_{DDES} = L_{RANS} - f_d \max(0, L_{RANS} - L_{LES})$

$$L_{RANS} = d_w$$

- $L_{LES} = \Psi C_{DES} \triangle$  subgrid length scale
- $f_d$  : DDES shielding function
- $d_w$  : wall distance
- Ψ : correction parameter for low Reynolds number term [Shur, 2003] C<sub>DES</sub>: constant value

#### 1. Definition in original DES [Spalart, 1997]

 $\Delta = \Delta_{max} = \max(\Delta x, \Delta y, \Delta z)$  $\Delta x$ ,  $\Delta y$ ,  $\Delta z$ : cell spacing in each coordinate direction 

#### 2. Subgrid scale typically used in LES [Deardroff, 1970]

$$\Delta = \Delta_{vol} = (\Delta x \Delta y \Delta z)^{1/3}$$

#### 3. Vorticity-dependent maximum cell length [Shur, 2015]

 $\Delta = \Delta_{SLA} = \tilde{\Delta}_{\omega} F_{KH}^{lim}$   $\tilde{\Delta}_{\omega} = \frac{1}{\sqrt{3}} \max_{n,m=1,8} |(l_n - l_m)|$   $F_{KH}^{lim} = \begin{cases} 1 & if f_d < (1 - \varepsilon) \\ F_{KH} & if f_d \ge (1 - \varepsilon) \end{cases}$   $I_n = n_\omega \times r_n$   $n_\omega = (n_x, n_y, n_z) : \text{ unit vector <u>aligned with the vorticity vector</u>} r_n : \text{ position vector } (n \text{ is corresponding to cell vertices})$   $0.1 < F_{KH} < 1.0$   $F_{KH} < 1.0 \text{ facilitates K-H instability by making $\Delta$ small}$  $\varepsilon = 0.01$ 

 $F_{KH}^{lim}$  is modified  $F_{KH}$  for DDES [Shur, 2015] to prevent activation of  $F_{KH}$  inside attached boundary layer

## Visualization of subgrid length scales: slat



Investigation of Effect of Subgrid Length Scale in DDES

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## Numerical method

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6	n	
2	-	

### Near-field flow analysis: FaSTAR (Unstructured CFD code)

Governing equation	3D compressible Navier-Stokes equations	
Method	Cell-centered finite volume method	
Turbulence model	SA-noft2-R DDES	
Discretization of inviscid term	SLAU ( <u>S</u> imple <u>L</u> ow-dissipation <u>AU</u> SM) <sup>[1]</sup>	
Reconstruction method	2 <sup>nd</sup> order Unstructured MUSCL	
Limiter	Limiter Hishida limiter <sup>[2]</sup>	
Gradient calculation	GLSQ (Green-Gauss/Weighted-Least-Square hybrid) [3]	
Time integration	LU-SGS with dual-time stepping method	
#inner iterations	5 (fixed)	

#### Far-field sound pressure evaluation: UPACS-Acoustics

Governing equation	Ffowcs Williams-Hawkings equation
FW-H surface	Solid wall surface of the airfoil [4]

[1] Shima et al., AIAA Journal 49 (8) pp. 1693-1709, 2011.

[2] Hishida et al., JAXA-SP-10-012. (in Japanese)

[3] Shima et al., AIAA Journal 51 (11) pp. 2740-2747, 2013.

[4] Terracol et al., AIAA Paper 2015-3132, 2015.

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## **2D TKE distributions**





## **2D TKE profiles**



- Δ<sub>vol</sub> and Δ<sub>SLA</sub> show similar trend to UPACS
  Δ<sub>SLA</sub> shows steep decrease at L7
- Adverse trend to UPACS at  $\Delta_{max}$

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Investigation of Effect of Subgrid Length Scale in DDES

## Summary

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- Comparsion of subgrid length scales at DDES for 30P30N airfoil
  Δ<sub>max</sub>/Δ<sub>vol</sub>/Δ<sub>SLA</sub>
- Small effect on time-averaged Cp
- $\Delta_{vol}$  and  $\Delta_{SLA}$  facilitates mixing of shear layer from the slat cusp, compared with  $\Delta_{max}$ 
  - rapid mixing in Q-criterion isosurface at the slat cusp
  - trend of decreasing peak magnitudes in 2DTKE profile
  - reduced peak values in NPBs in surface/farfield pressure spectra
- Observations for  $\Delta_{SLA}$ 
  - steep decrease in 2DTKE
  - submerged NBPs in surface/farfield pressure spectra
  - expected activation of  $F_{KH}$  at the slat cusp; unexpected activation on the flap
- Future work
  - <sup>D</sup> to investigate effect of subgrid length scale on the main element and the flap