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STAR-CCM+を用いたNASA CRMの空力特性予測 Aerodynamic Prediction of NASA CRM with STAR-CCM+

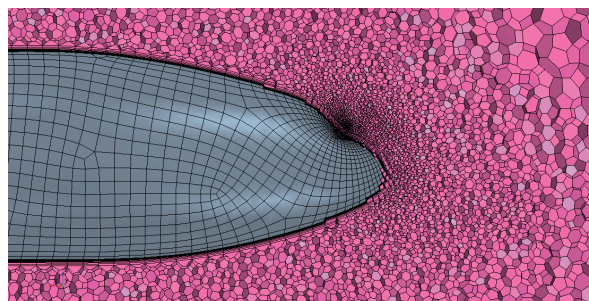
曾我匡統、鈴木竜太、大関昌平、山西伸宏
シーメンスPLMソフトウェア(旧：株式会社CD-adapco)

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Mesh / Solver information

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- Case 1
- Solver : STAR-CCM+
 - Mesh type : Polyhedral Mesh
 - Finite Volume Method : Cell centered
 - Inviscid flux : 2nd-order
 - Viscous flux : 2nd-order
 - Turbulence Model : SST $k-\omega$



Solver setting

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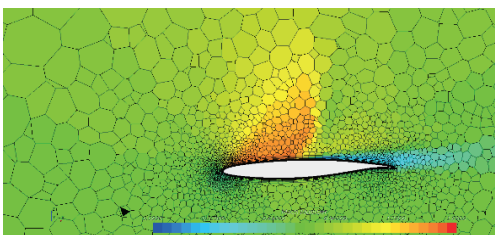
- CFL : 50
- Grid sequencing initialization technique
 - Maximum grid levels : 5
 - Maximum iterations per level : 250
 - Convergence tolerance per level : 1.0e-4
- Continuity convergence accelerator technique to improve mass conservation
 - Convergence accelerator update frequency : 1
 - Under-relaxation factor : 0.05
- $k-\omega$ Turbulence
 - Under-relaxation factor : 0.8

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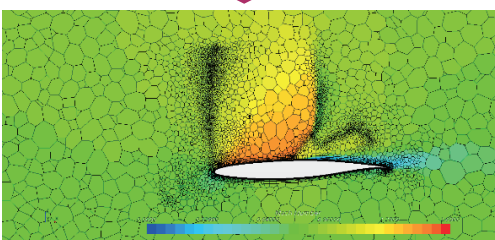
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Adaptive mesh refinement with polyhedral mesh

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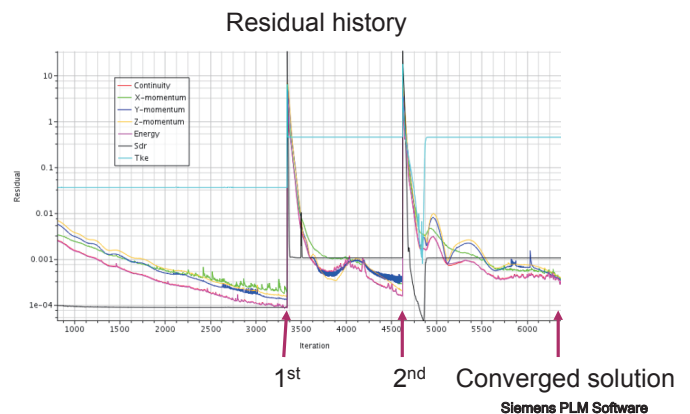


Refinement



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Table-based mesh refinement implemented in STAR-CCM+ is used for AMR. We carried out the refinement twice to obtain the convergent solutions.



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Adaptive mesh refinement with polyhedral mesh

Variables used for mesh refinement criteria in a custom field function are:

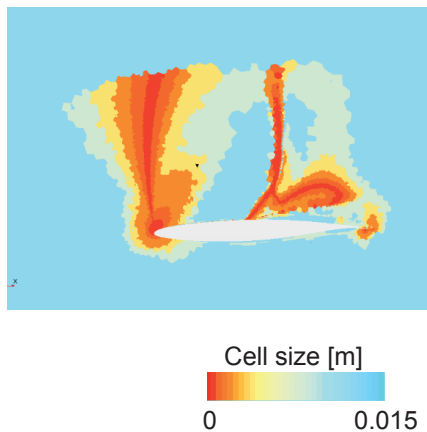
- Gradient of pressure coefficient
- Range of Mach number

Defined field function

```

If {WD} > 0.2 then    x = 2.5/14*{WD} + c0
Else if |grad(Cp)| > 100 or (M > 0.99 and M < 1.01) and {WD} < 0.1 then    x = c1
Else if |grad(Cp)| > 50 or (M > 0.97 and M < 1.03) and {WD} < 0.1 then    x = c2
Else if |grad(Cp)| > 20 or (M > 0.95 and M < 1.05) and {WD} < 0.1 then    x = c3
Else if |grad(Cp)| > 15 or (M > 0.93 and M < 1.1) and {WD} < 0.1 then    x = c4
Else if |grad(Cp)| > 10 or (M > 0.91 and M < 1.2) and {WD} < 0.1 then    x = c5
x: Cell size, Cp: Pressure coefficient, WD: Wall distance
c0 = 0.012, c1 = 5.0e-4, c2 = 0.001, c3 = 0.002, c4 = 0.004, c5 = 0.008
    
```

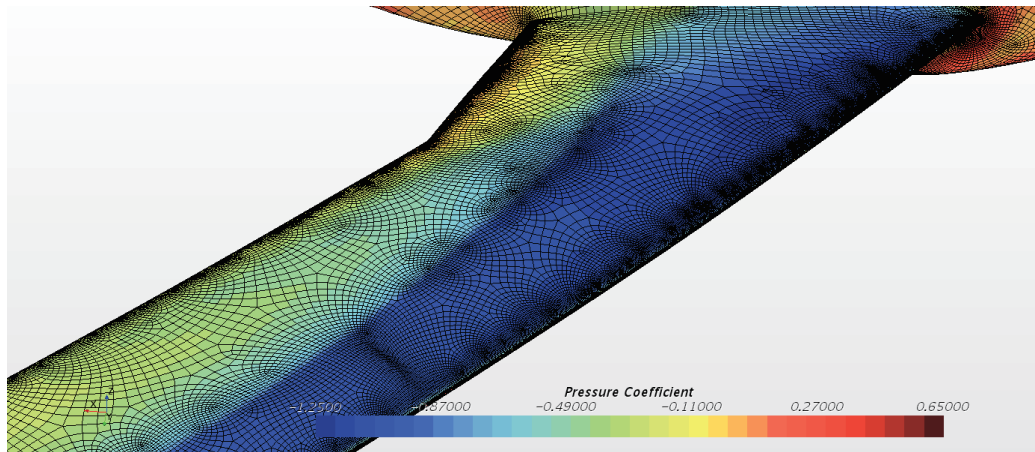
Cell size distribution at Section E



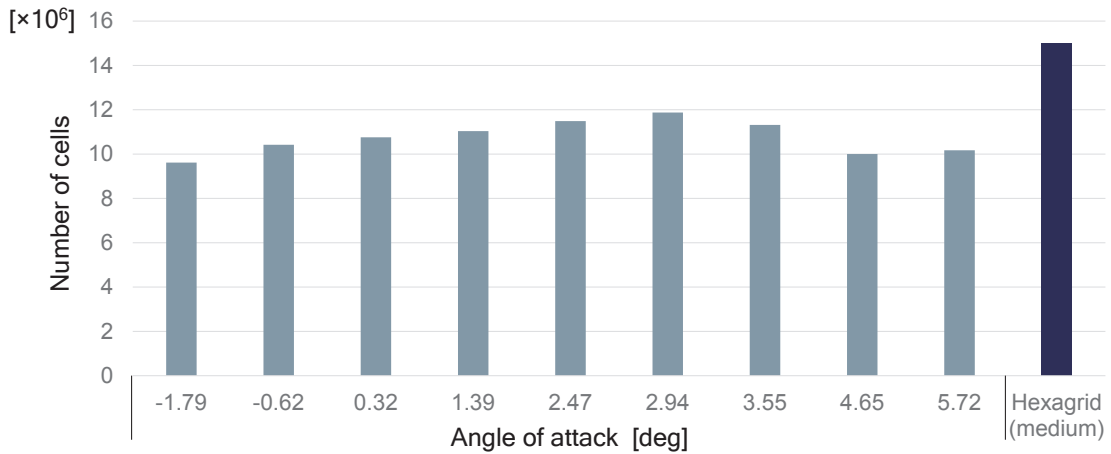
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Surface mesh adequately resolved to capture shock

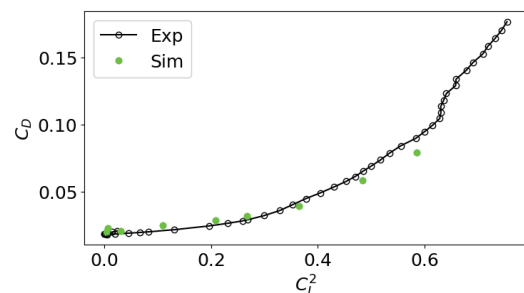
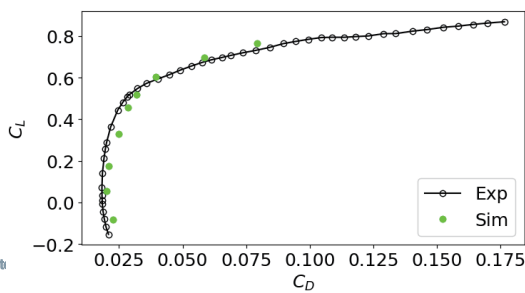
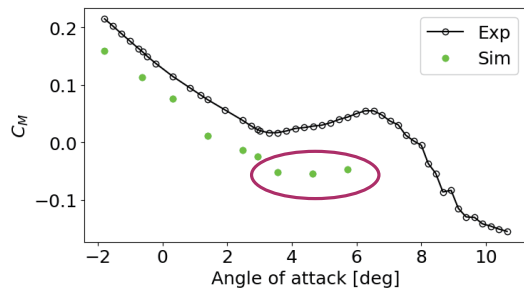
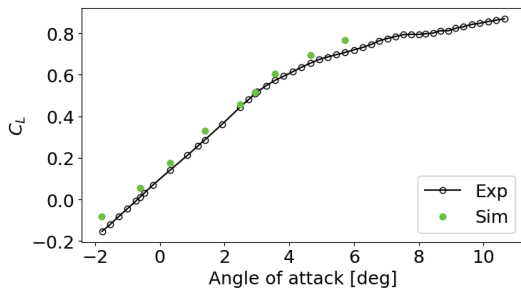
C_p distribution and mesh on the wing



The numbers of cells used for calculation are approximately 10 million

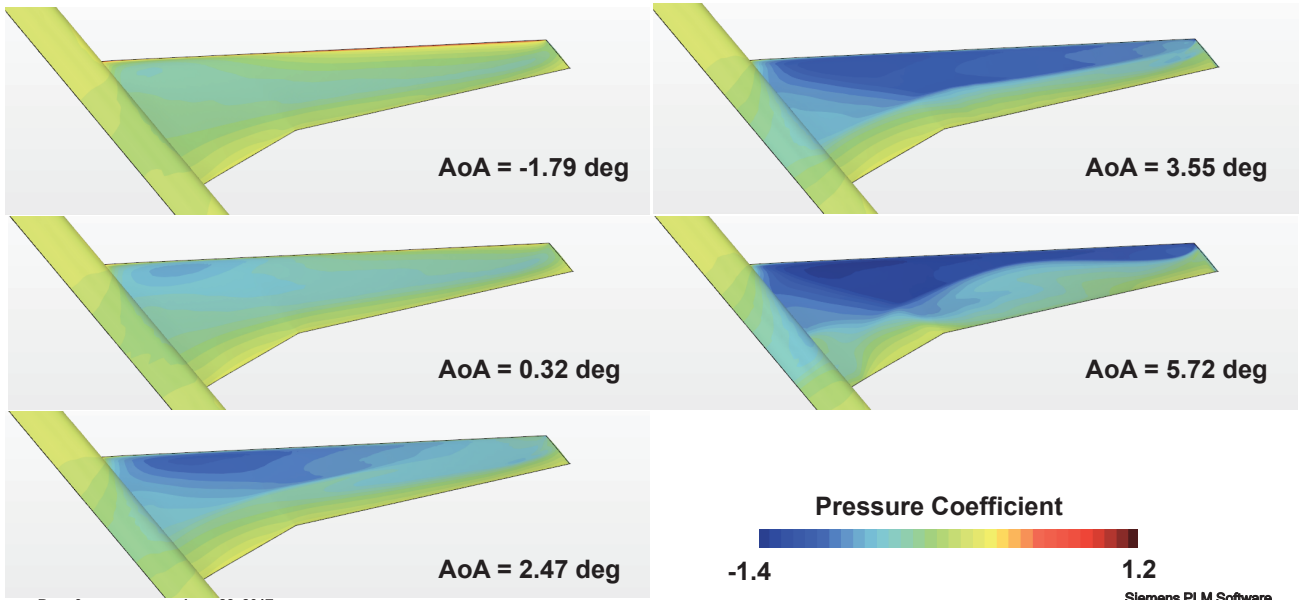


AoA sweeps
 C_M prediction deviates at high angle of attack



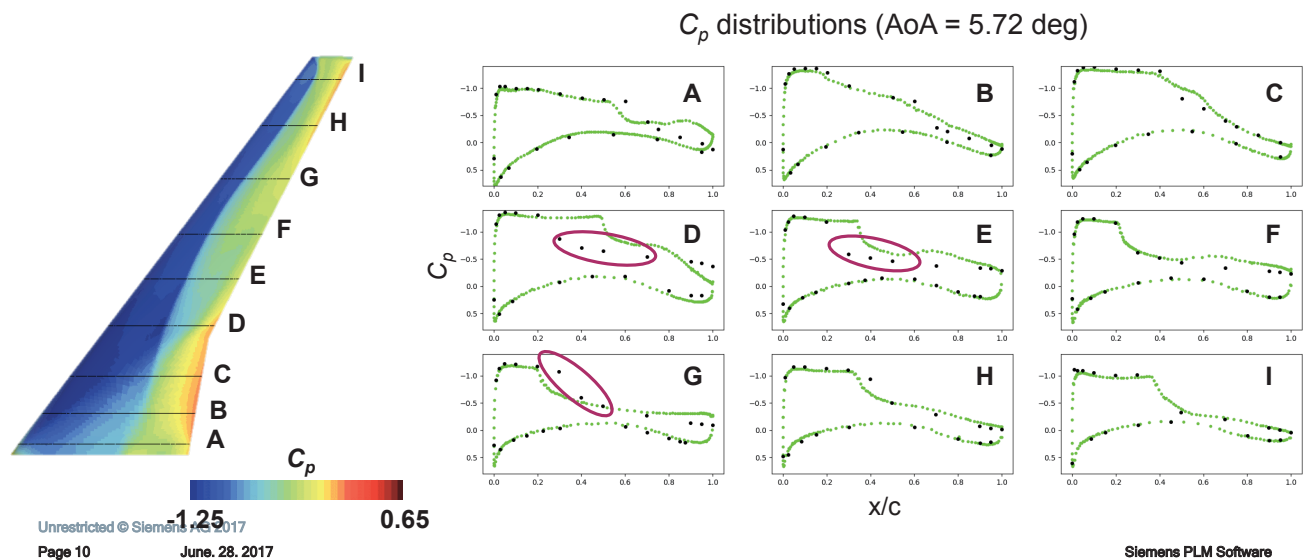
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Pressure coefficient distributions on the wings



The location of the shock wave does not match with the experiment at Section D, E, and G

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Points of improvement **SIEMENS**

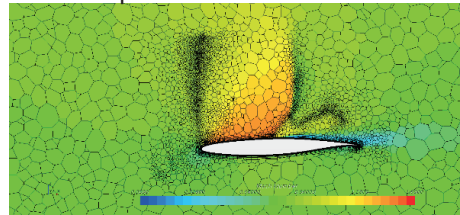
- Modify the mesh refinement criterion
- Refine the leading edge
- Switch from polyhedral mesh to trimmed mesh

Reduction of number of cells by modifying the mesh refinement criterion **SIEMENS**

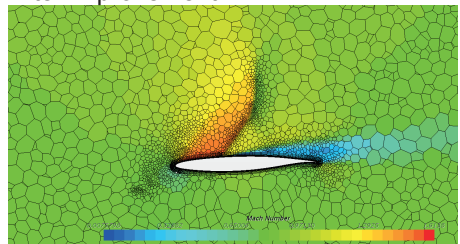
The variables for the refinement has been changed to

- Gradient of pressure coefficient
- **Gradient of Mach number**

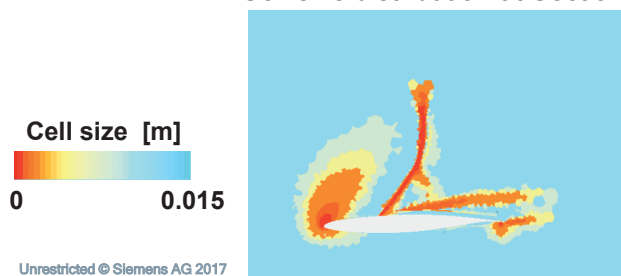
Before improvement



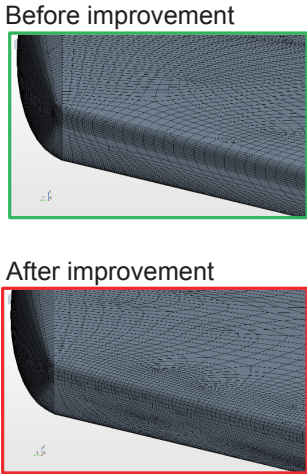
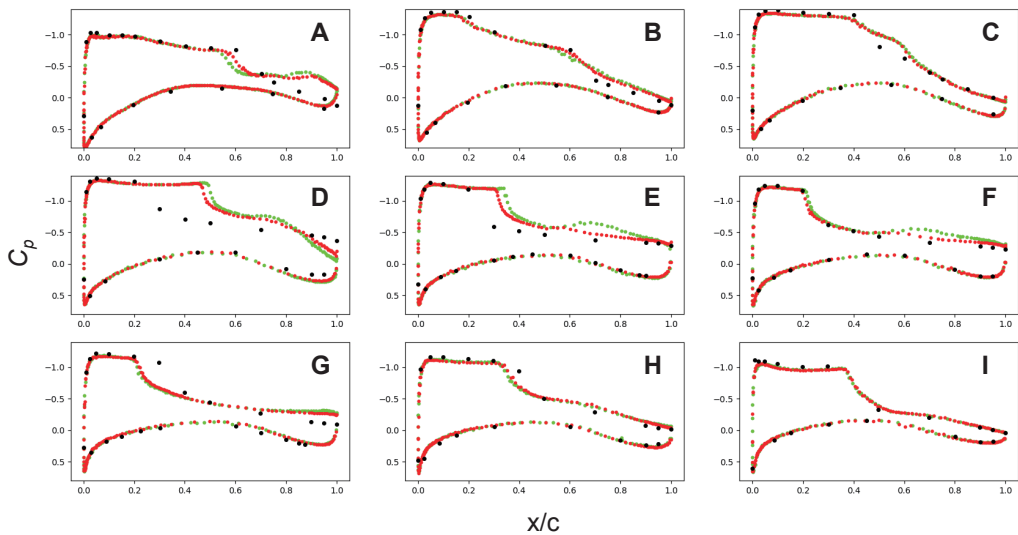
After improvement



Cell size distribution at Section E



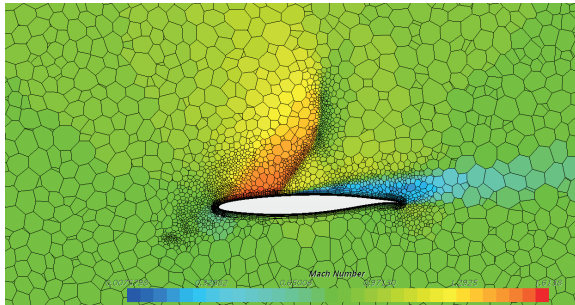
C_p distribution improved by refining the leading edge (AoA = 5.72 deg)



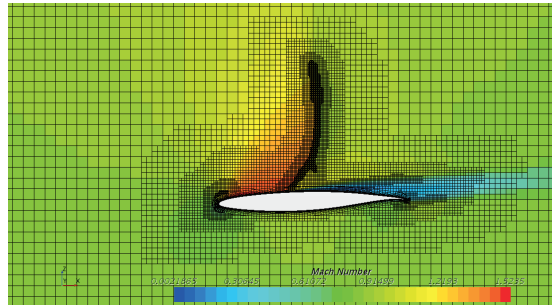
Trimmed mesh with AMR



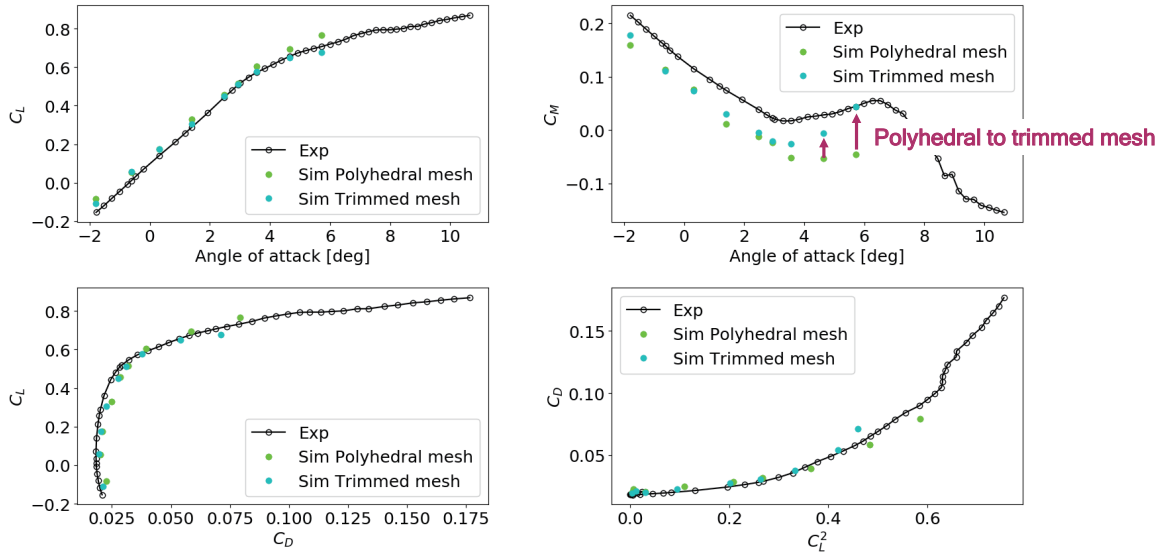
Polyhedral mesh with AMR



Trimmed mesh with AMR



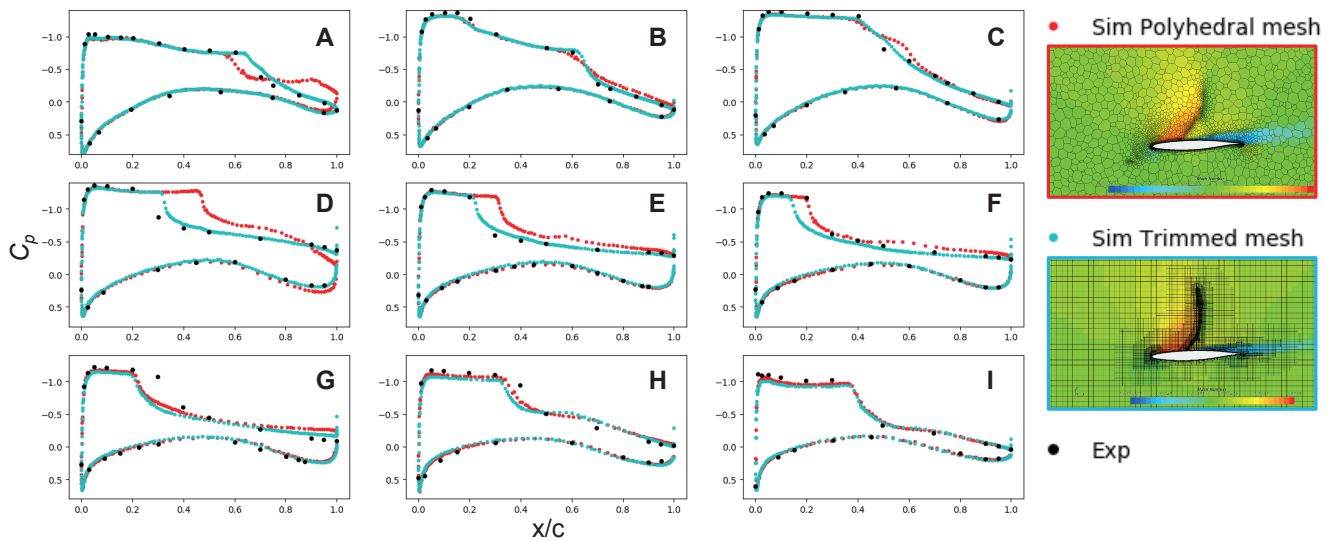
AoA sweep improved by using trimmed mesh



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Significantly improved predictions of C_p profiles on trimmed mesh (AoA = 5.72 deg)

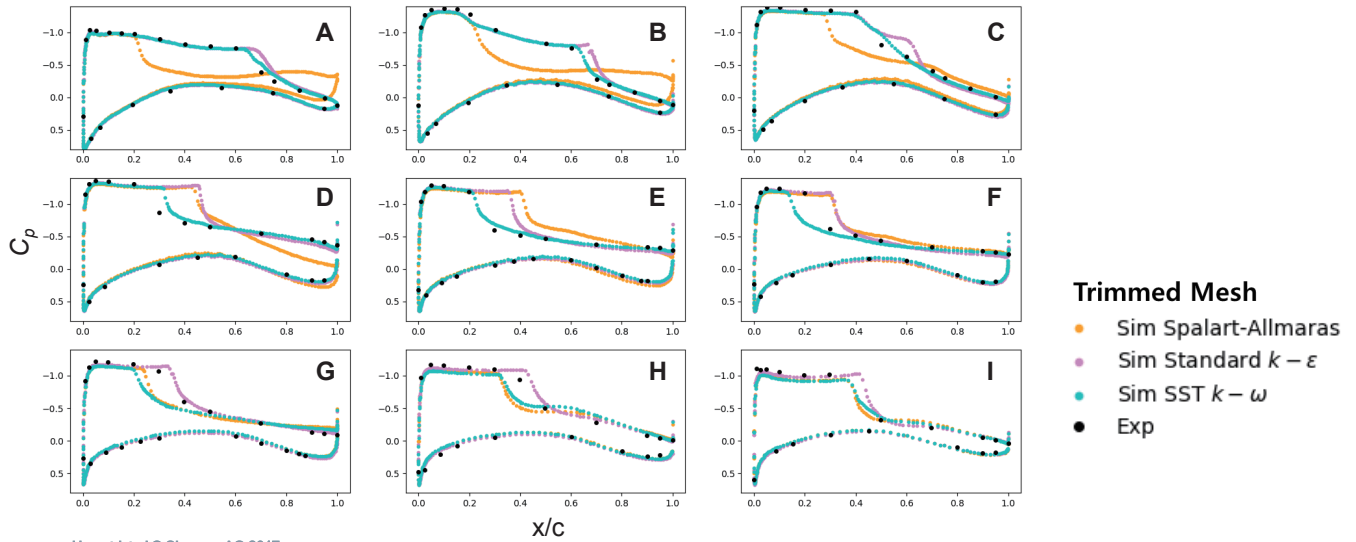


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Comparison of turbulence models (AoA = 5.72deg)
Good agreement of SST $k-\omega$ result with the experiment

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- We carried out the calculations with polyhedral mesh and AMR
- C_D and C_L predictions agreed with the experimental results
- C_M prediction deviates at high angle of attack
- Resolving the leading edges provided better results
- Prediction significantly improved with trimmed mesh
- SST $k-\omega$ turbulence model provided better results than other models

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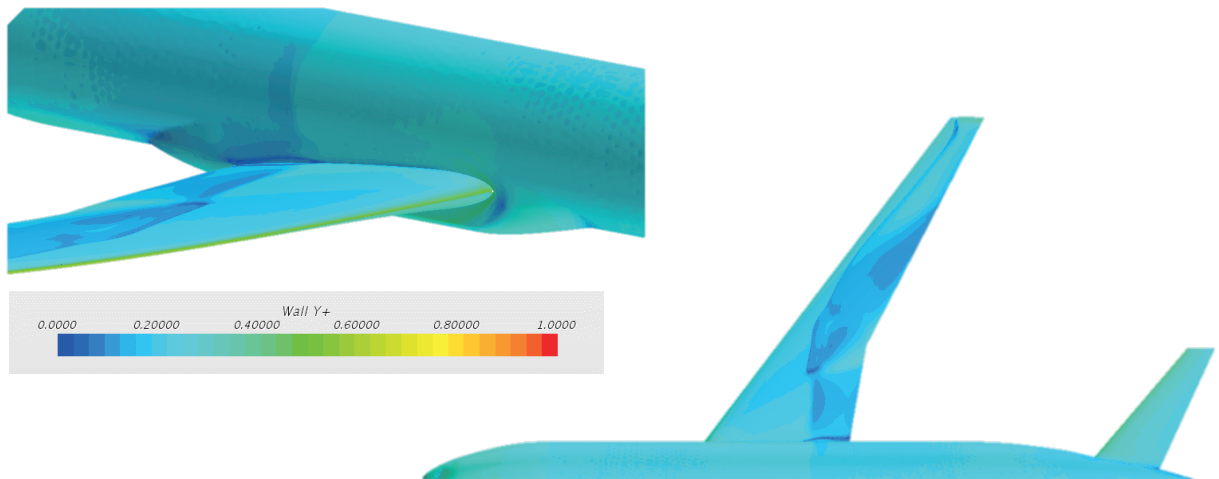
Appendix

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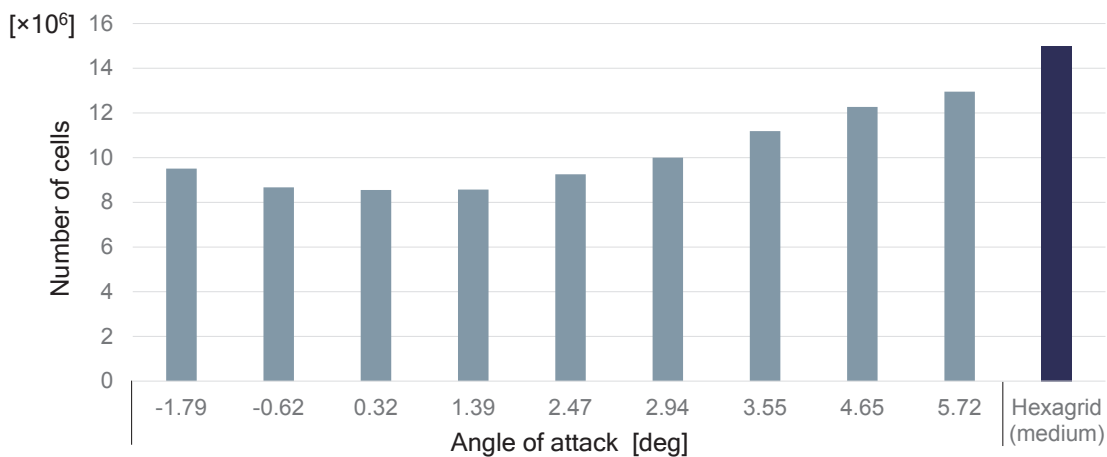

Realize innovation.

Wall Y⁺ distribution calculated with trimmed mesh (AoA = 5.72 deg)

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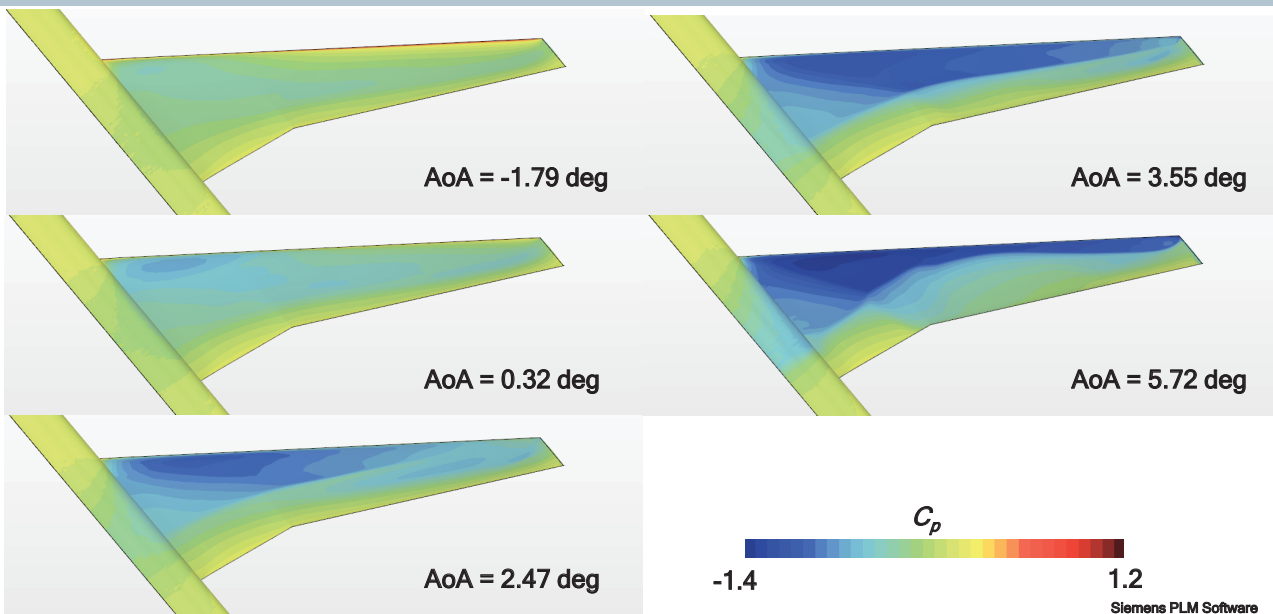

Number of cells generated with trimmed mesh and AMR Cell counts increases as the angle of attack gets higher



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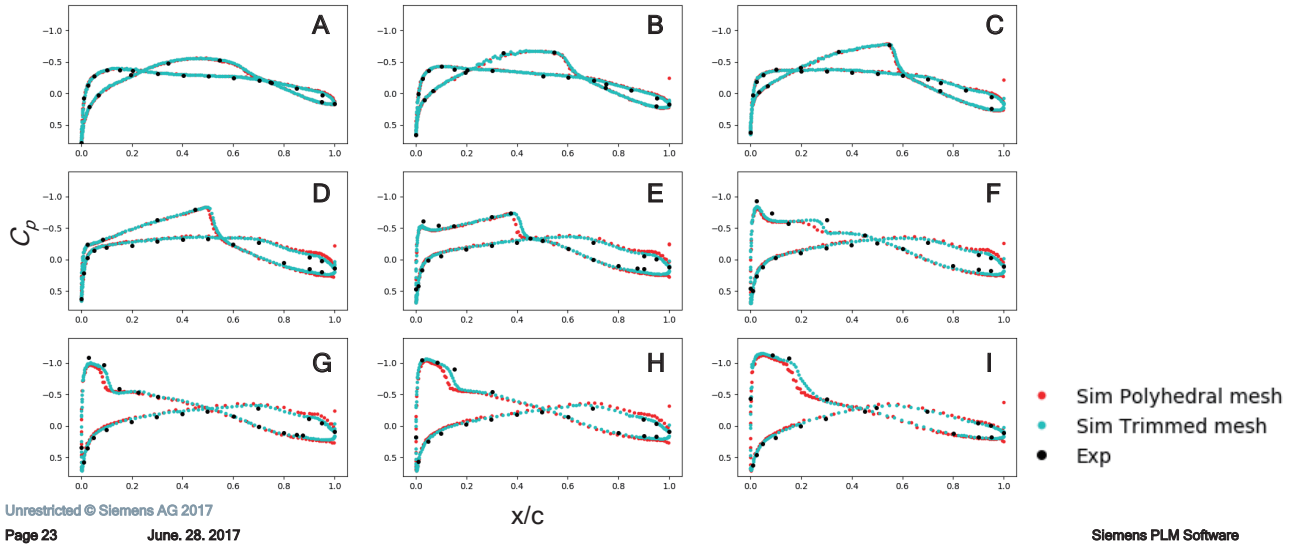
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Pressure coefficient distributions on the wings trimmed mesh

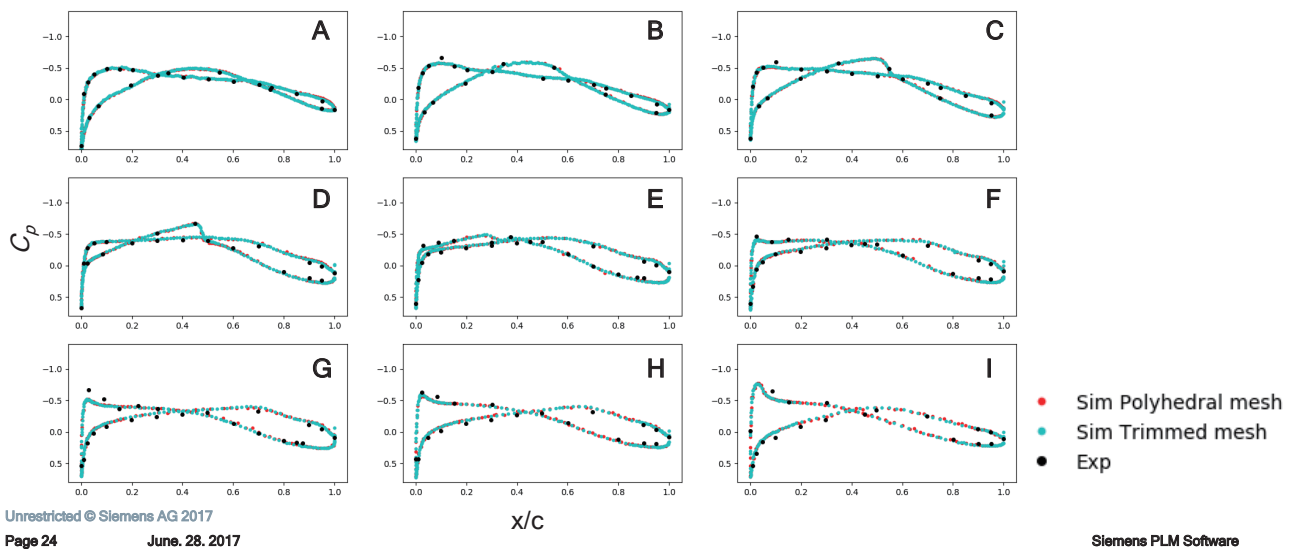




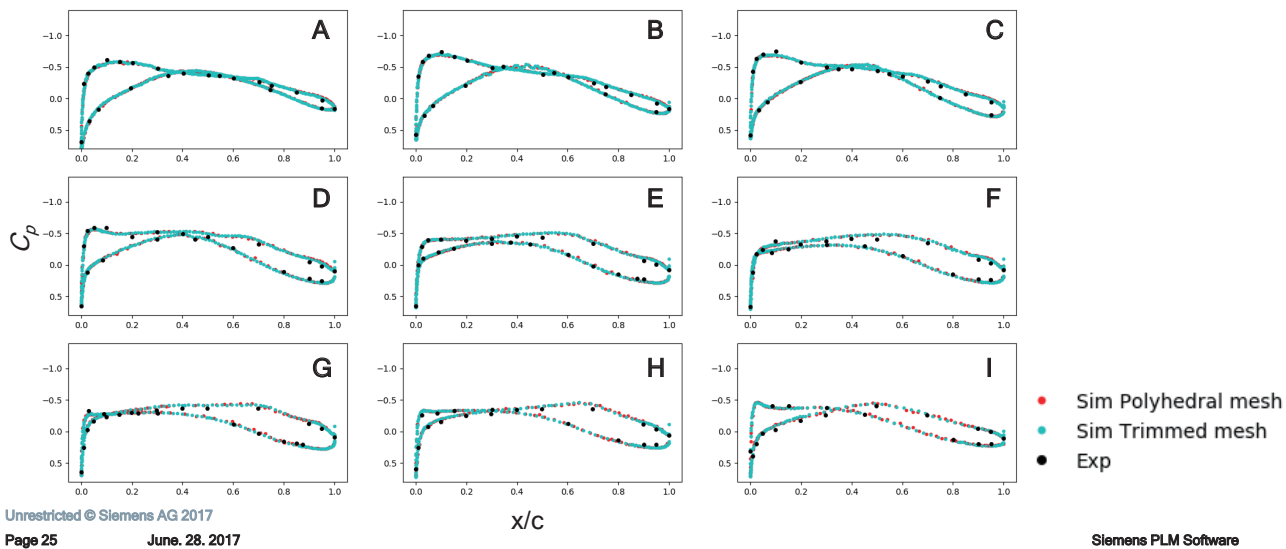
Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = -1.79 deg)



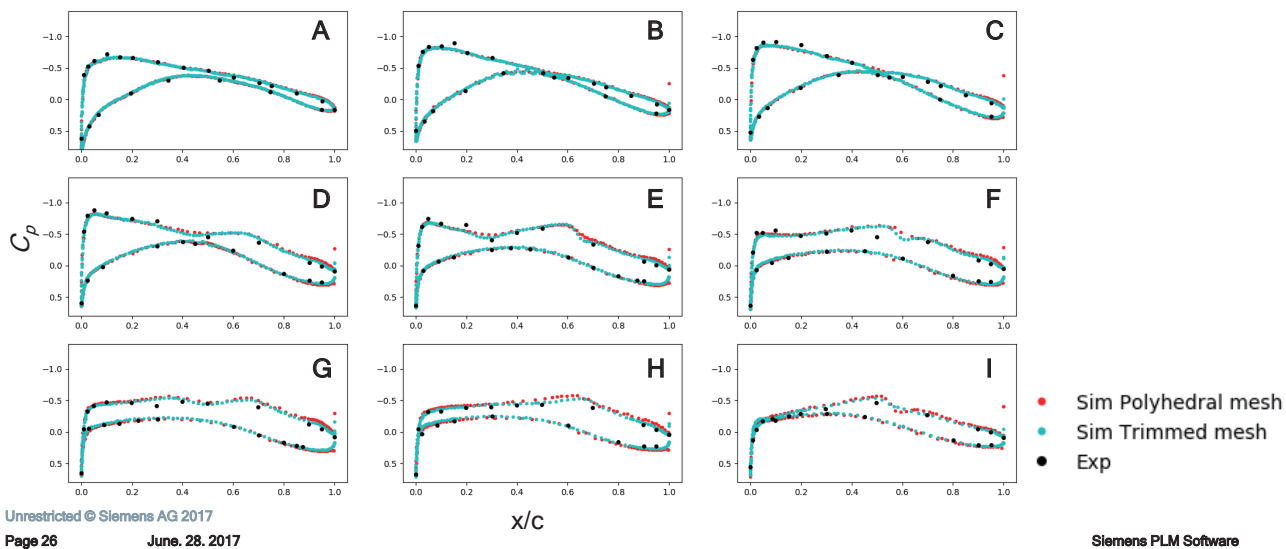
Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = -0.62 deg)



Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 0.32 deg)

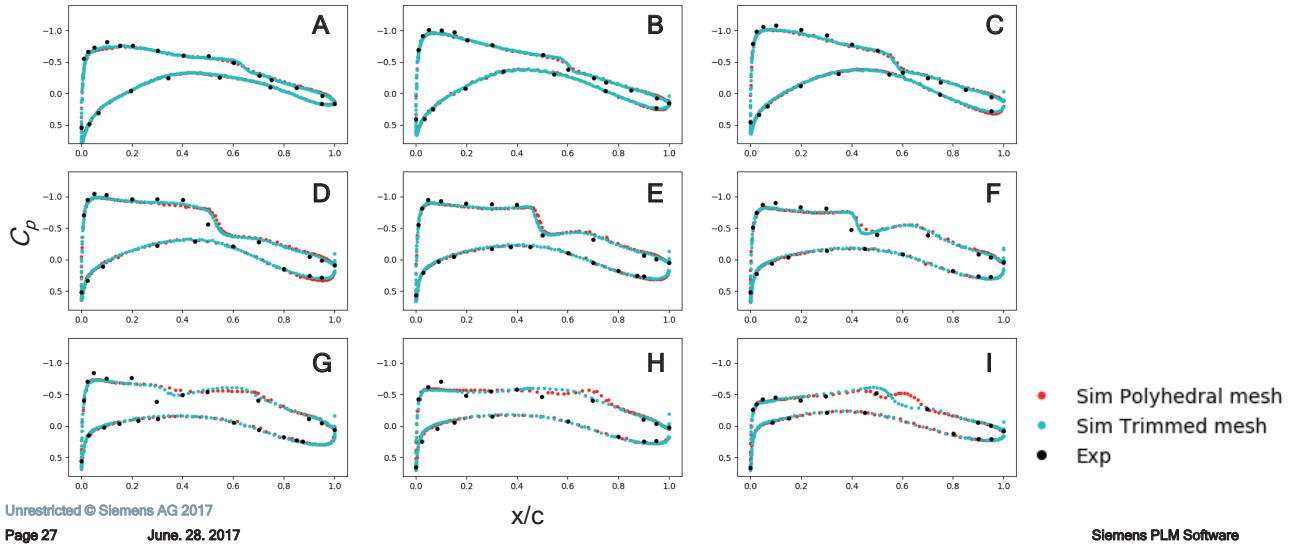


Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 1.39 deg)

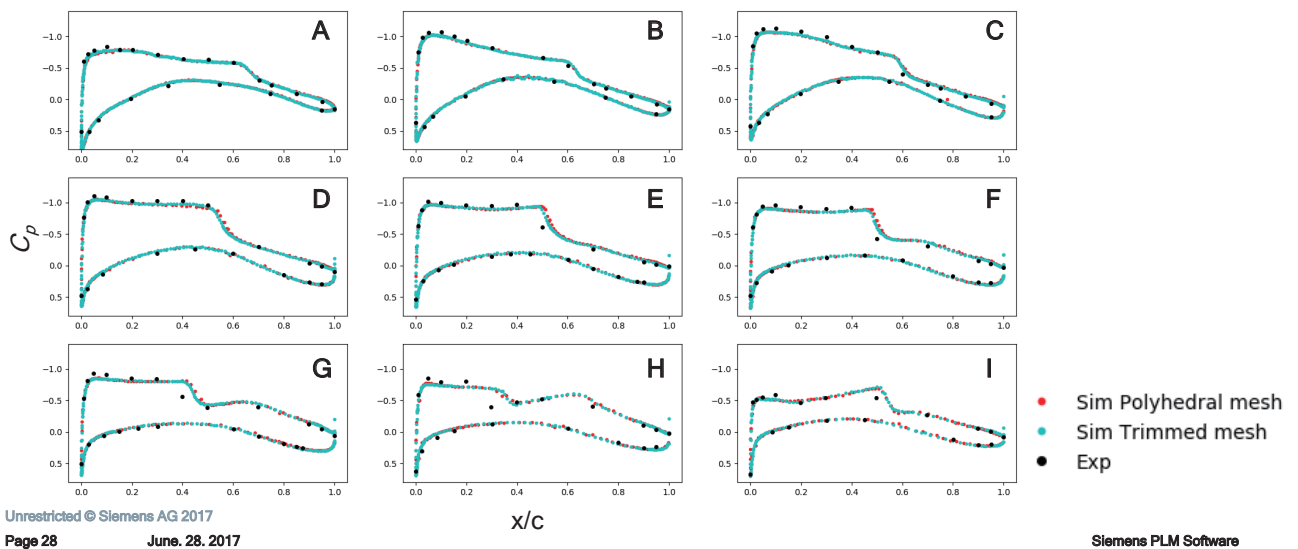




Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 2.47 deg)

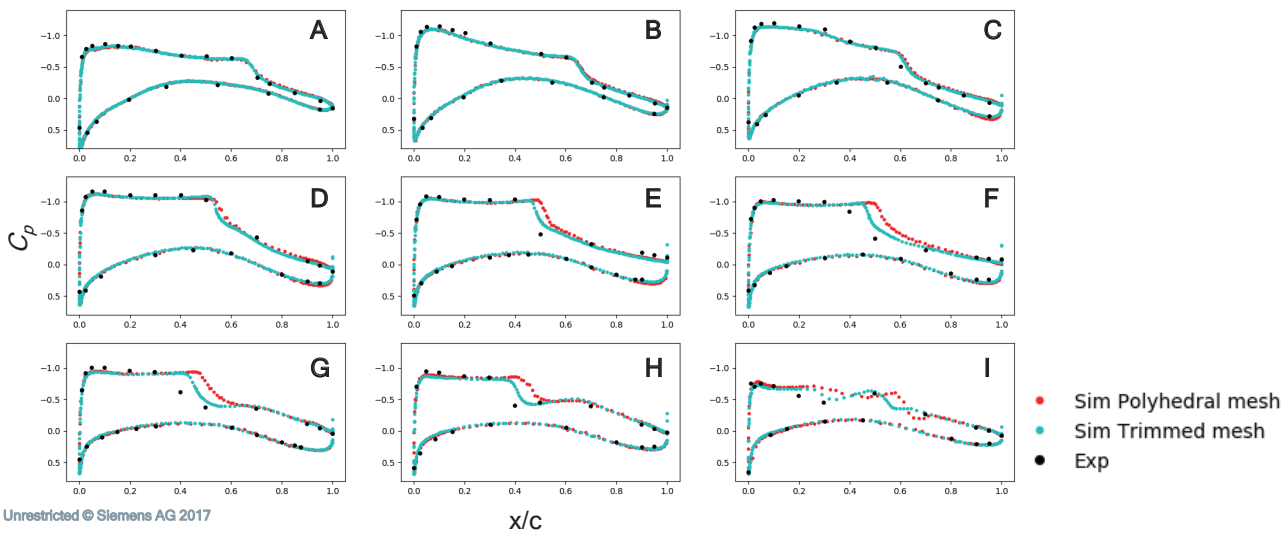


Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 2.94 deg)



Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 3.55 deg)

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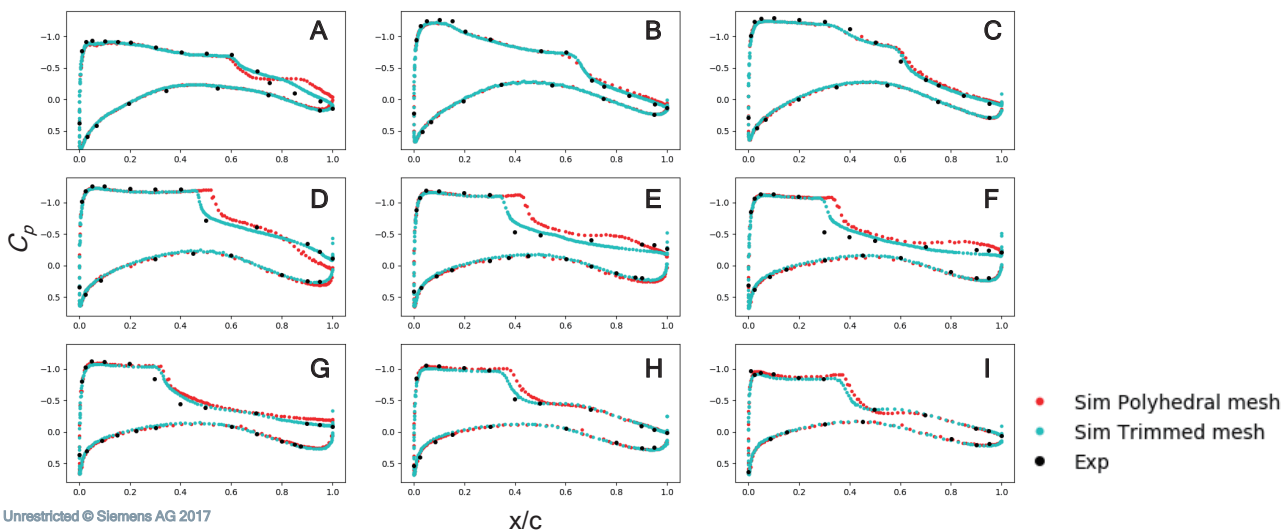


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Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 4.65 deg)

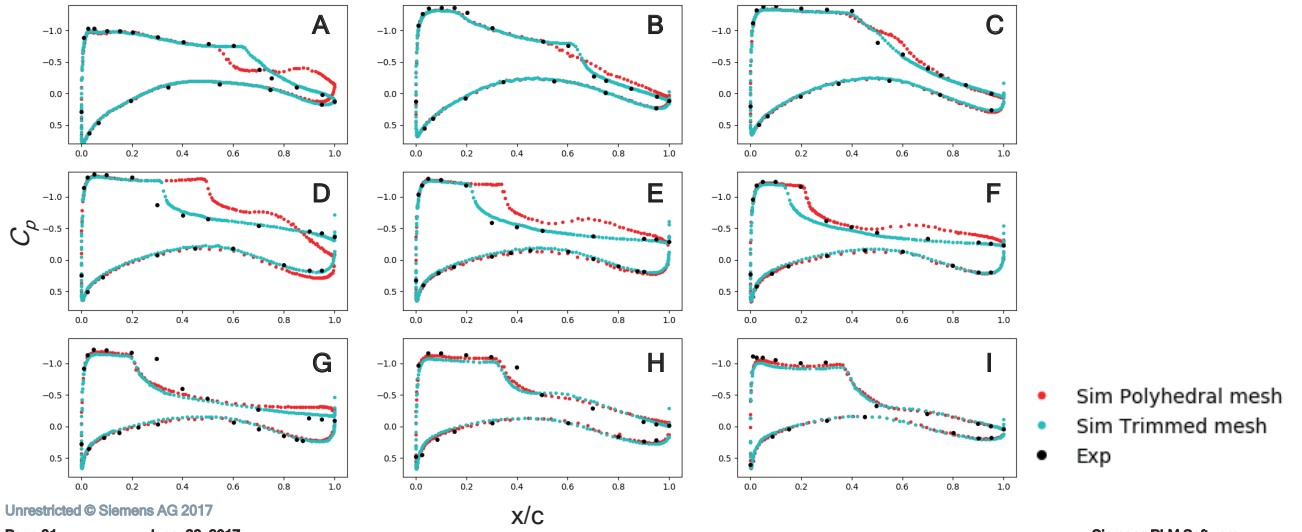
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Comparison of C_p calculated with polyhedral / trimmed mesh at each section (AoA = 5.72 deg)



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