

The 49th Fluid Dynamics Conference/ The 35th Aerospace Numerical Simulation Symposium
28 June 2017, National Olympics Memorial Youth Center, Tokyo, Japan



Summary of Third Aerodynamics Prediction Challenge (APC-III)

Atsushi Hashimoto (JAXA)
APC committee

Contents



-
- Participants
 - Test case 1
 - Test case 2
 - Test case 3
 - Summary

Statistics of submitted data



- Organizations and number of submitted data(total 53 data)
 - National research institutes: JAXA(29)
 - Universities: Tohoku Univ., Tohoku Univ./KIT(1), Univ. of Tokyo(1), Toyama Univ.(3), Hokkaido Univ.(2)
 - Aerospace industries: KHI
 - Commercial software: Exa(1), CD-adapco(1), Cradle(2), NUMECA(12), AdvanceSoft(1)

- Grids for test case 1
 - HexaGrid: 14
 - MEGG3D: 16
 - UPACS: 10
 - Custom: 11

} Provided by committee

- Turbulence models
 - Test case 1: SA(9), SST(23), EARSM(15), K-ε(2), BSL(1), SS/SST-2003 Hybrid(1)
 - Test case 3: DES(2), VLES(1)

3

Participants of case 1



ID	Name	Organization	Code	Grid	Turbulence Model
A ●	橋本 敦	JAXA	FaSTAR	HexaGrid	SA-noft2-R-QCR2000
					SST-2003
					SST-2003-sust
					SST-2003-sust-QCR2000
					EARSM
					EARSM(w/o nonlinear)
					EARSM-QCR2000 (w/o nonlinear)
				MEGG3D	SA-noft2-R-QCR2000
					SST-2003
					SST-2003-sust
					SST-2003-sust-QCR2000
					EARSM
					EARSM(w/o nonlinear)
					EARSM-QCR2000 (w/o nonlinear)

4

Participants of case 1



ID	Name	Organization	Code	Grid	Turbulence Model
A ●	橋本 敦	JAXA	FaSTAR	UPACS	SA-noft2-R-QCR2000
					SST-2003
					SST-2003-sust
					SST-2003-sust-QCR2000
					EARSM
					EARSM(w/o nonlinear)
					EARSM-QCR2000 (w/o nonlinear)
				Custom (Cartesian based)	SA-noft2-R-QCR2000
					SST-2003
					SST-2003-sust
					SST-2003-sust-QCR2000
					EARSM
					EARSM(w/o nonlinear)
					EARSM-QCR2000 (w/o nonlinear)

5

Participants of case 1



ID	Name	Organization	Code	Grid	Turbulence Model
C ●	佐々木 大輔	金沢工業大学	BCM-TAS カップリング	Custom (MEGG3D+BCM)	SA
D ●	玉置 義治	東京大学	UTCart	Custom (Octree Cartesian)	SA-noft2-R-QCR2000
E ●	松島 紀佐	富山大学	FaSTAR	HexaGrid	SST-2003
F ●	寺島 洋史	北海道大学	RG-FaSTAR	HexaGrid	SST-2003
					SS/SST-2003 Hybrid
I ●	曾我 匡統	CD-adapco	STAR-CCM+	Custom (polyhedra)	SST
J ●	中島 吉隆	ソフトウェアクレイドル	scFLOW	HexaGrid	SST
				Custom (polyhedra)	

6

Participants of case 1



ID	Name	Organization	Code	Grid	Turbulence Model
K ●	岡 新一	NUMECA	FINE/Open	UPACS	SA-fv3(Cmat)
					SST-2003(Cmat)
					SSC-EARSM(Cmat)
				MEGG3D	SA-fv3(Cscal)
					SA-fv3(Cmat)
					SST-2003(Cscal)
					SST-2003(Cmat)
					SSC-EARSM(Cscal)
					SSC-EARSM(Cmat)
					KE-YS-1993(Cscal)
					KE-YS-1993(Cmat)
S-BSL-EARSM(Cscal)					
L ●	大西 陽一	アドバンスソフト	Advance/FrontFlow/red	HexaGrid	SST

7

Participants of case 1



ID	Name	Organization	Code	Grid	Turbulence Model
A1 ●	橋本 敦	JAXA	FaSTAR	Custom (HexaGrid)	SA-Zonal DES (Spanwise polynomialx1)
A2 ●	橋本 敦	JAXA	FaSTAR	Custom (HexaGrid)	SA-Zonal DES (Spanwise polynomialx6)
H ●	甲斐 寿 Ehab Fares	Exa Japan Exa Corp.	PowerFLOW	Custom (Cartesian LBM)	VLES

8

Issues of APC-I and APC-II



- The variation of CFD is large for high angles of attack
 - **Test case 1:** Investigation of grids and turbulence models for high angle-of-attack flows
 - The committee recommends turbulence models other than SA

- The slight difference remains between CFD and experiment
 - **Test case 2:** Discussion on the difference based on follow-up computations under arbitrary conditions

- Improvement of buffet prediction accuracy
 - **Test case 3:** Comparison with unsteady pressure frequency spectra, unsteady PSP
 - Unsteady pressure data and flow field data are submitted.

9

Case 1: Alpha-sweep



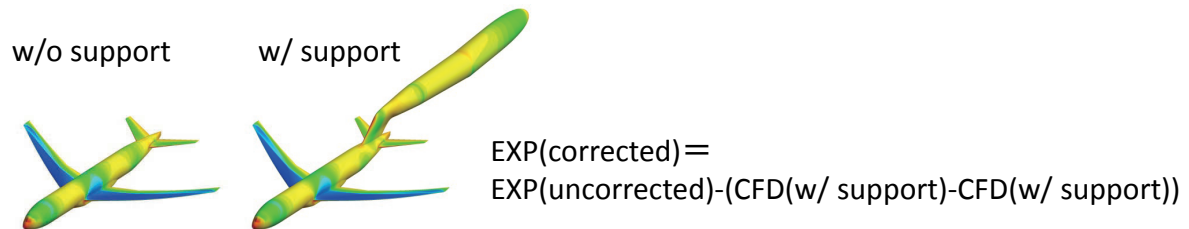
- Model: NASA-CRM($i_H=0\text{deg}$) without support device
- Grid: Medium($\sim 10\text{M}$)
- Conditions: $M = 0.847$, $Re_c = 2.26 \times 10^6$, $T_{ref} = 284\text{K}$
- Angles: -1.79deg , -0.62deg , 0.32deg , 1.39deg , 2.47deg , 2.94deg , 3.55deg , 4.65deg , 5.72deg
- Data to be submitted:
 - Aerodynamic coefficients(C_D, C_L, C_m)
 - Decompose them into pressure and friction
 - Decompose them into parts (main wing, fuselage, tail)
 - Surface C_p distributions
 - Main wing
- Recommendations:
 - Usage of turbulence models other than SA
 - Discussion on high-angle-of-attack flows

10



Support correction

- We added experimental data corrected by support interferences.
- The results of HexaGrid and FaSTAR are used for the correction.



AoA	CD (w support)	CD (wo support)	Δ CD	CL (w support)	CL (wo support)	Δ CL	Cm (w support)	Cm (wo support)	Δ Cm
-1.79	0.0202	0.0221	-0.0019	-0.128	-0.117	-0.011	0.218	0.192	0.026
-0.62	0.0182	0.0202	-0.0020	0.031	0.045	-0.014	0.157	0.128	0.029
0.32	0.0187	0.0209	-0.0022	0.147	0.162	-0.015	0.121	0.091	0.030
1.39	0.0207	0.0231	-0.0024	0.277	0.294	-0.017	0.080	0.047	0.032
2.47	0.0248	0.0277	-0.0029	0.414	0.434	-0.020	0.048	0.014	0.034
2.94	0.0279	0.0311	-0.0033	0.478	0.499	-0.020	0.032	-0.003	0.035
3.55	0.0339	0.0377	-0.0038	0.551	0.568	-0.017	0.022	-0.011	0.033
4.65	0.0503	0.0549	-0.0045	0.628	0.643	-0.015	0.039	0.008	0.031
5.72	0.0692	0.0741	-0.0048	0.663	0.683	-0.020	0.078	0.047	0.030

11

Case 1: List of data



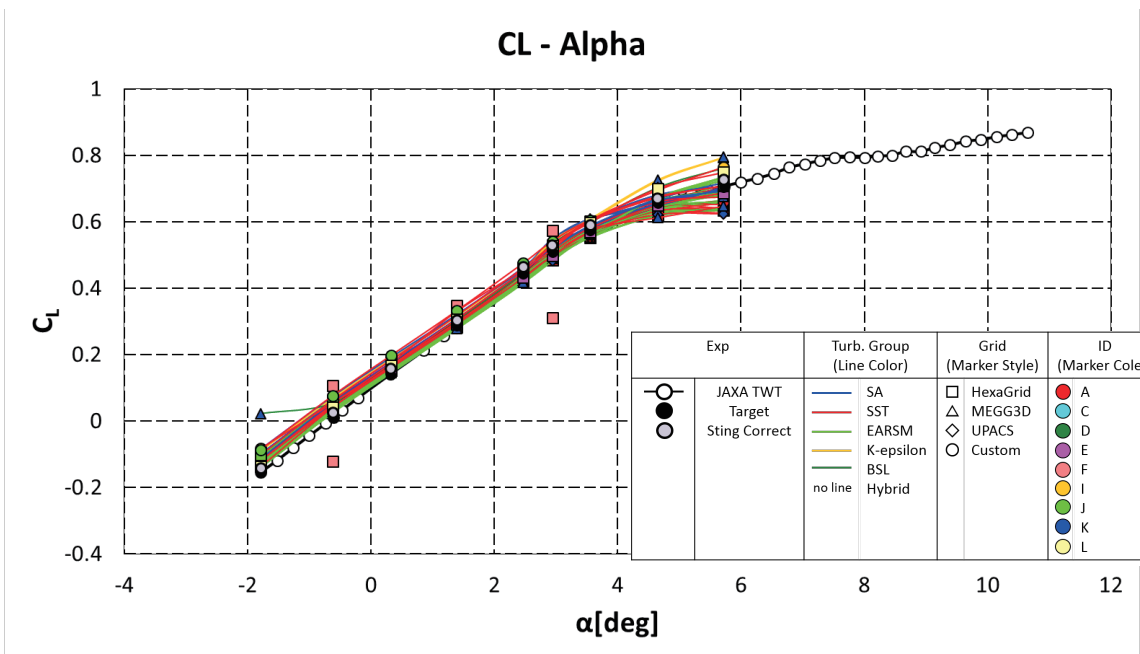
- Alpha sweep (CL- α , CL-CD, Cm- α)
 - Comparison with APC-I and APC-II
 - Comparison between grids(HexaGrid, MEGG3D, UPACS, Custom)
 - Comparison between turbulence models(SA, SST, EARSM)
- Cruise condition ($\alpha=2.94$ deg)
 - Aerodynamics coefficients(CD, CL, Cm, CDi)
 - Cp distributions (Section A-I)
- High angle of attack ($\alpha=5.72$ deg)
 - Cp distributions (Section A-I)
 - Comparison between the results with and without SOB separation
 - Comparison between grids (HexaGrid, MEGG3D, UPACS, Custom)

12

Case 1: Alpha sweep



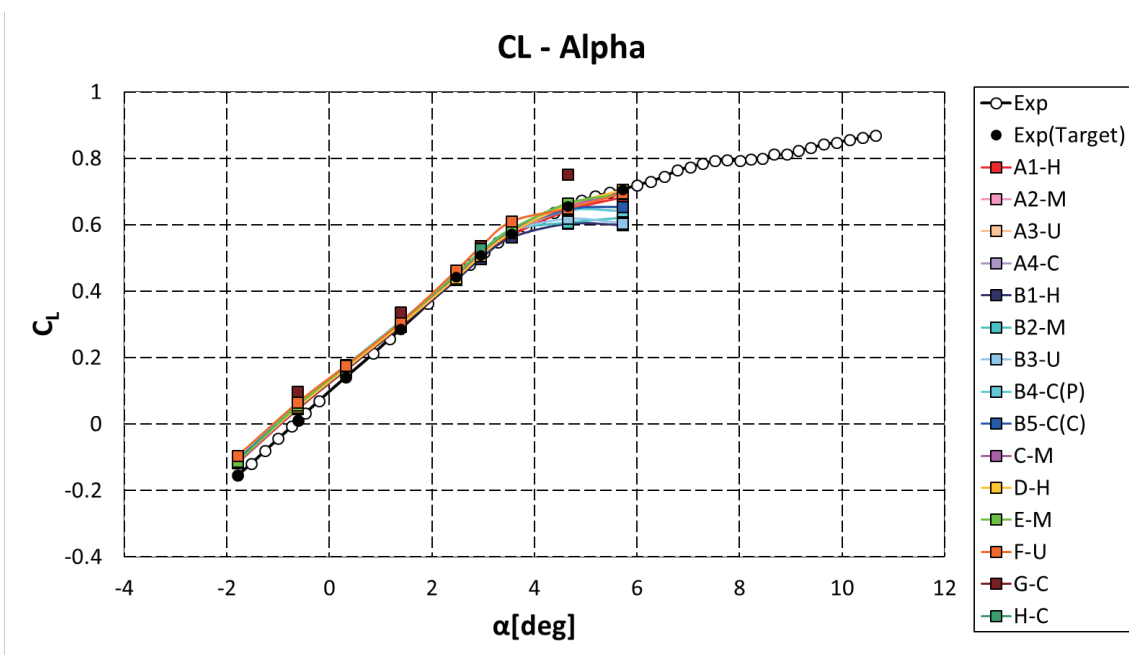
Comparison with the previous results of APC-I and APC-II



The variation is larger than that of APC-I and APC-II especially for high angles of attack. But the slope is almost same between turbulence models.

13

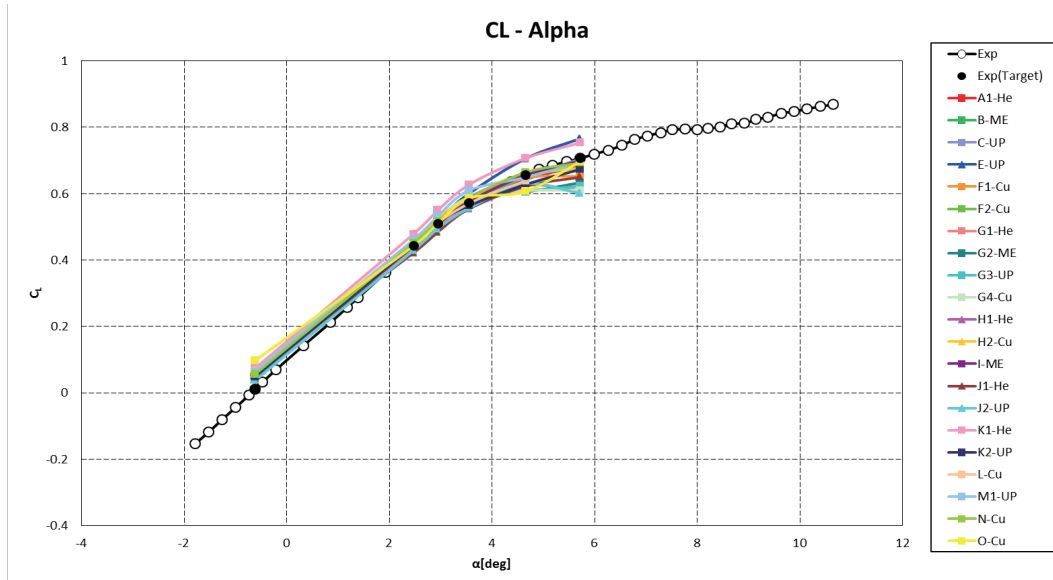
Alpha sweep of APC-II



14



Alpha sweep of APC-I

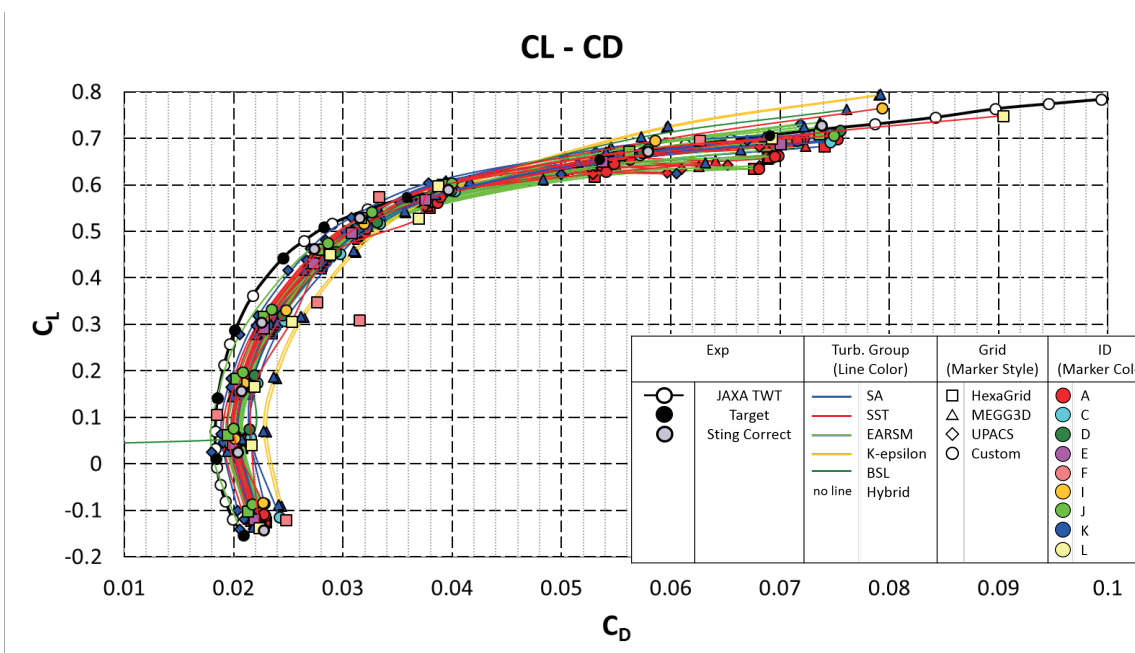


15

Case 1: Alpha sweep



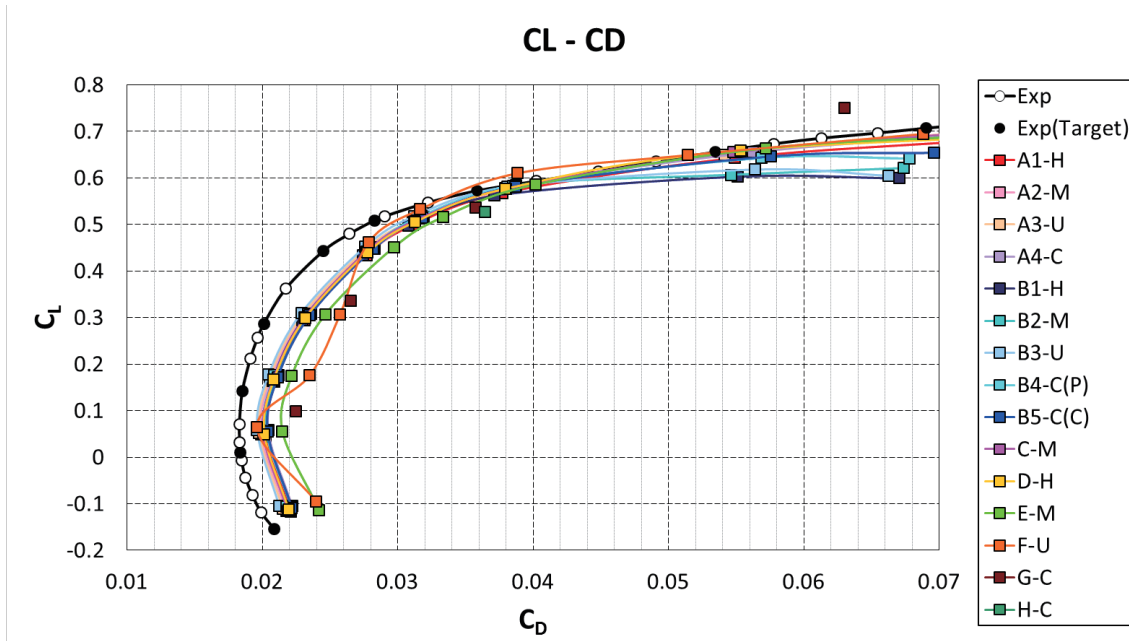
Comparison with the previous results of APC-I and APC-II



The variation is larger than that of APC-I and APC-II.
But the trend is almost same between turbulence models.

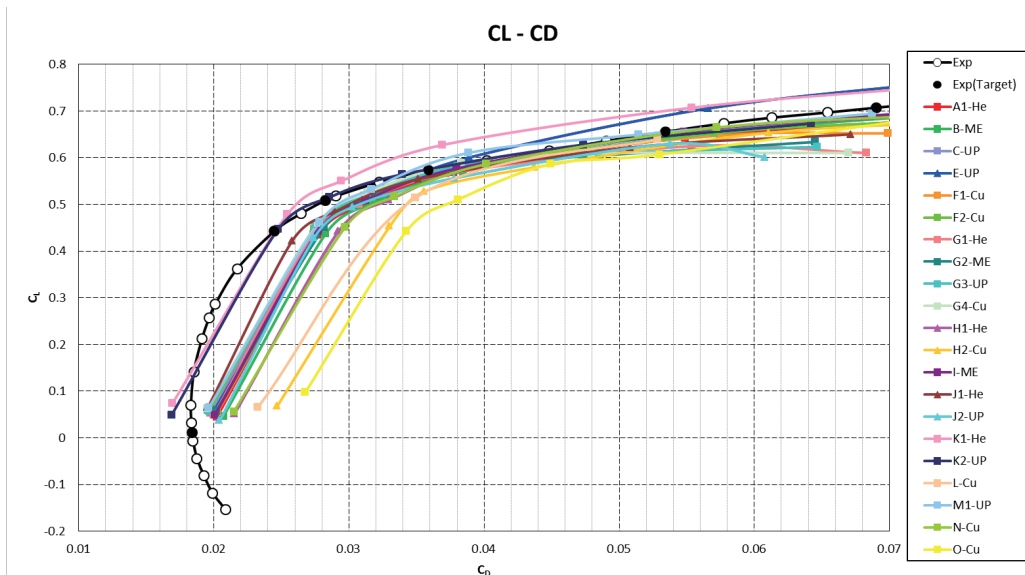
16

Alpha sweep of APC-II



17

Alpha sweep of APC-I

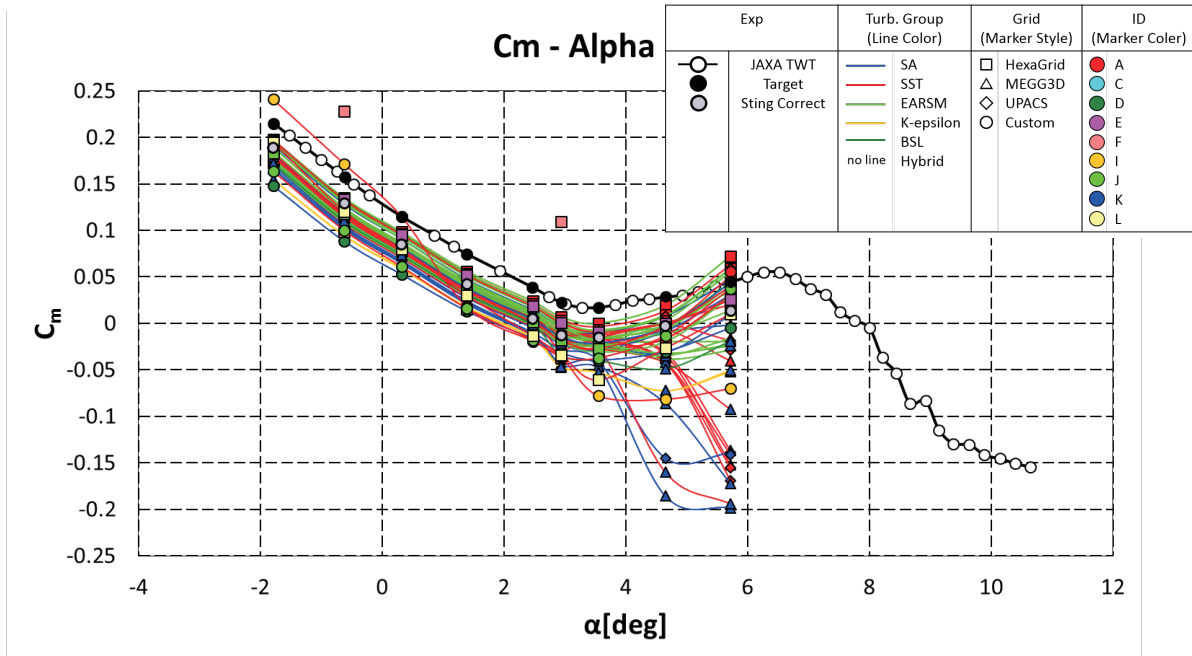


18



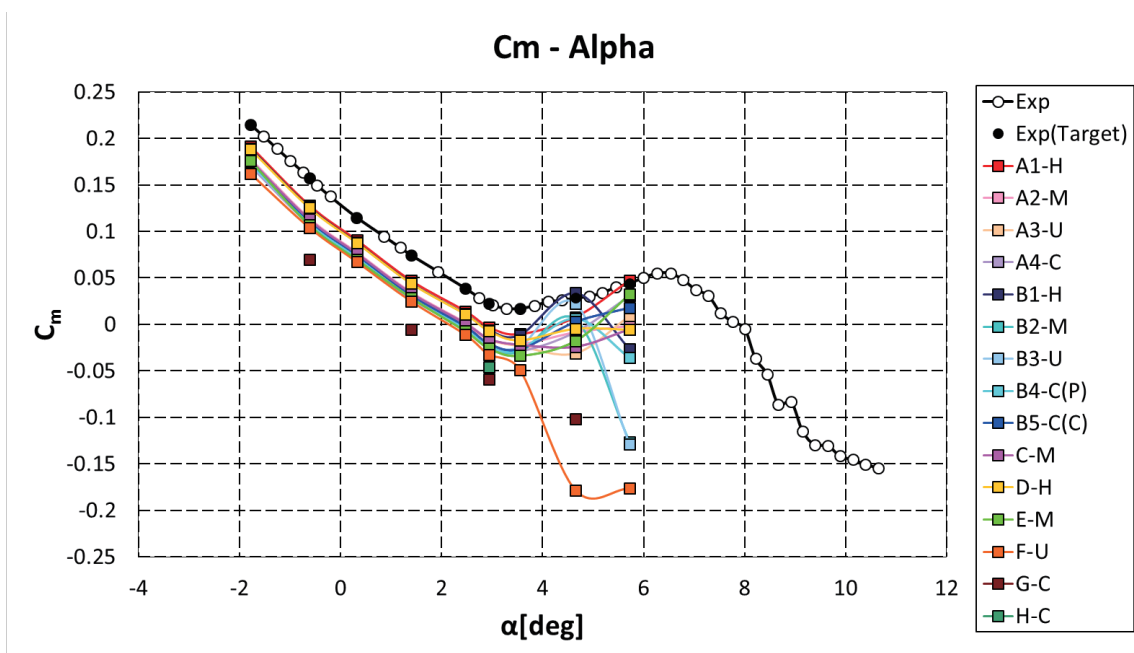
Case 1: Alpha sweep

Comparison with the previous results of APC-I and APC-II

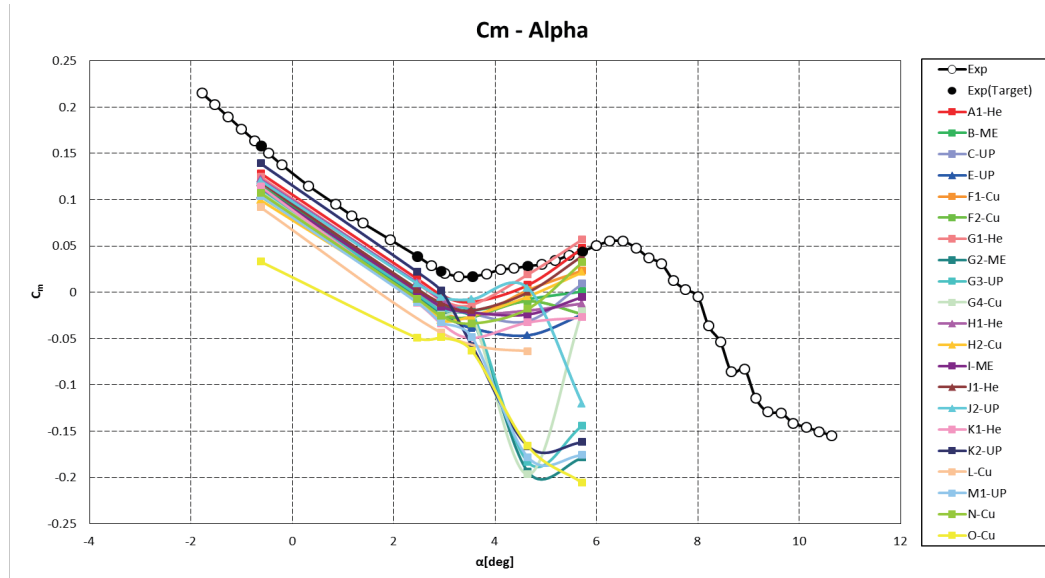


The variation is larger than that of APC-I and APC-II especially for high angles of attack. But the slope is almost same between turbulence models.

Alpha sweep of APC-II



Alpha sweep of APC-I



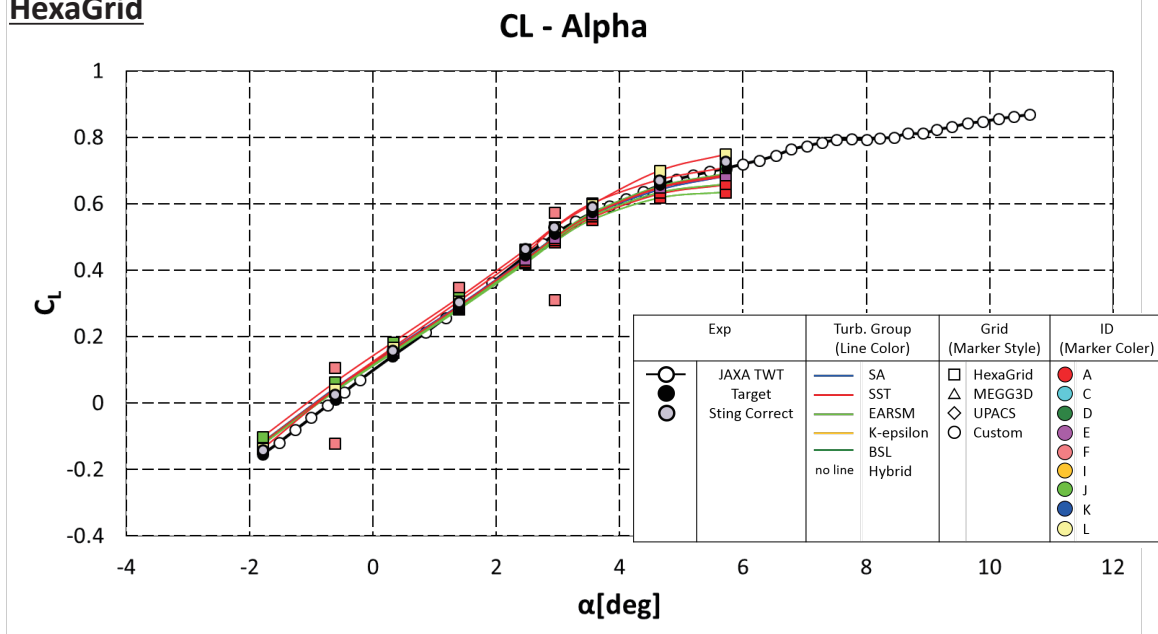
21

Case 1: Alpha sweep



Comparison between grids

HexaGrid



The high AoA behaviors of SST and EARSM are affected by the grid

22

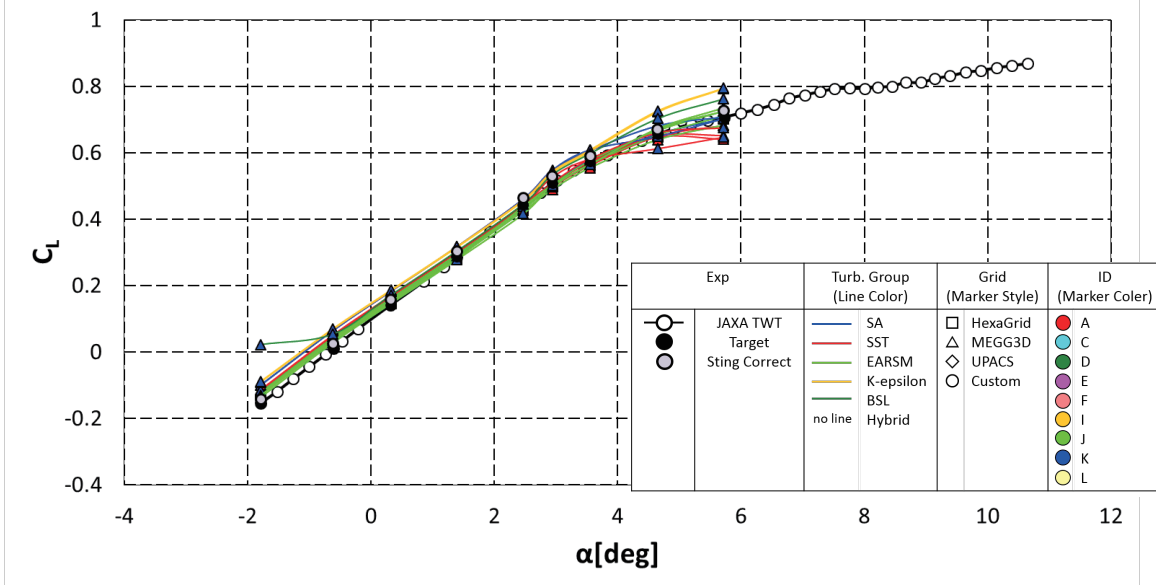


Case 1: Alpha sweep

Comparison between grids

MEGG3D

CL - Alpha



The high AoA behaviors of SST and EARSM are affected by the grid

23

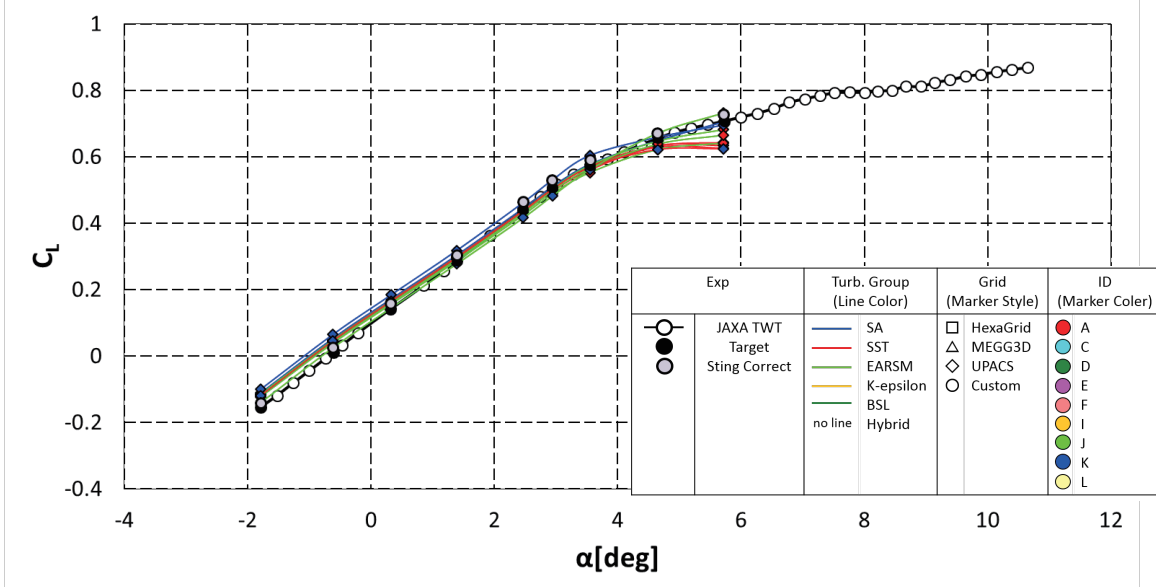
Case 1: Alpha sweep



Comparison between grids

UPACS

CL - Alpha



The high AoA behaviors of SST and EARSM are affected by the grid

24

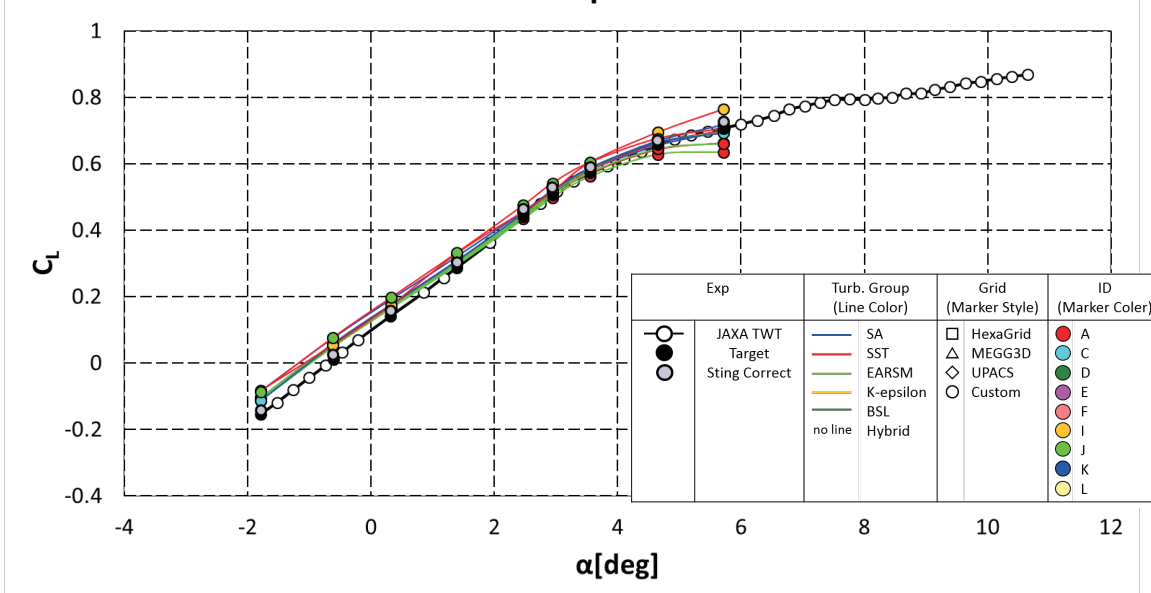


Case 1: Alpha sweep

Comparison between grids

Custom(Cartesian & Polyhedra)

CL - Alpha



The high AoA behaviors of SST and EARSM are affected by the grid

25

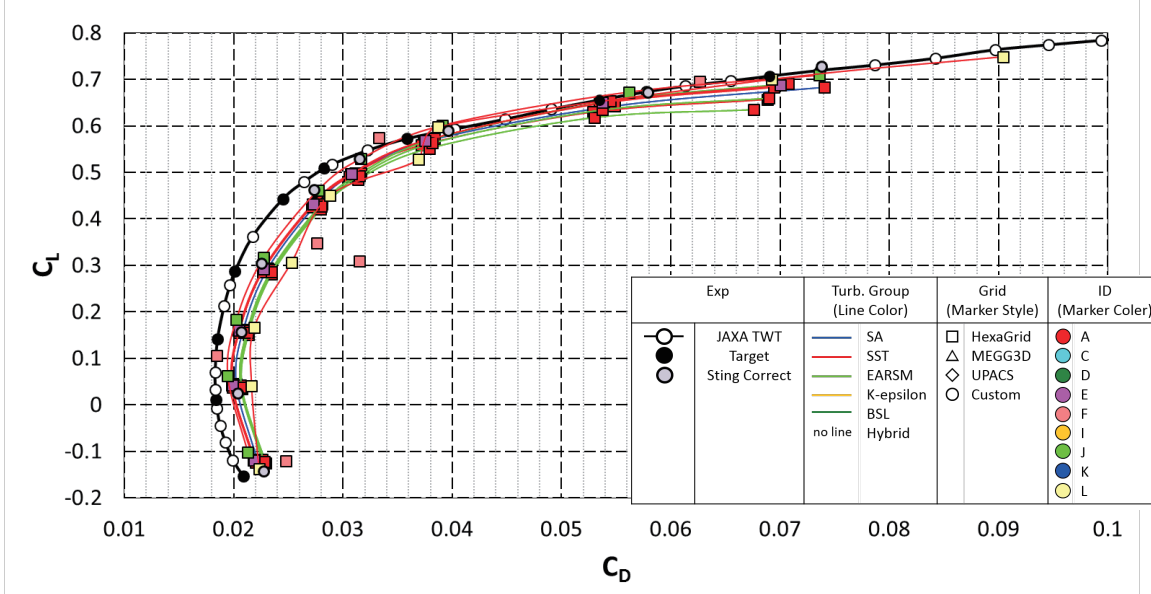


Case 1: Alpha sweep

Comparison between grids

HexaGrid

CL - CD



CD predicted with UPACS grid is smaller than the others
(This may be caused by the turbulence models used with UPACS grid)

26

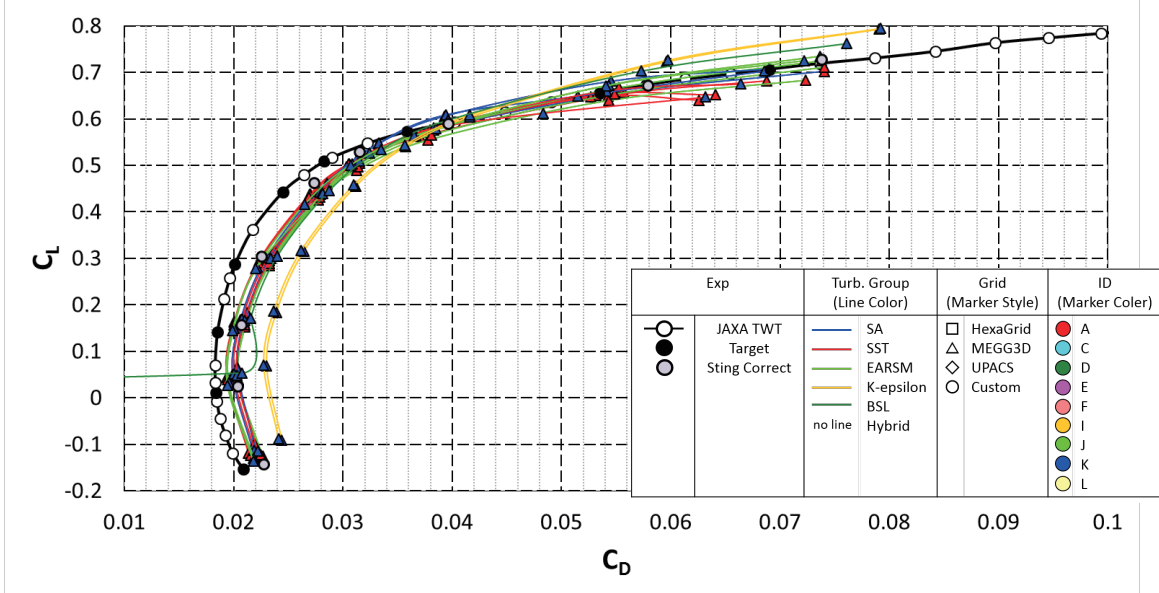


Case 1: Alpha sweep

Comparison between grids

MEGG3D

CL - CD



CD predicted with UPACS grid is smaller than the others
(This may be caused by the turbulence models used with UPACS grid)

27

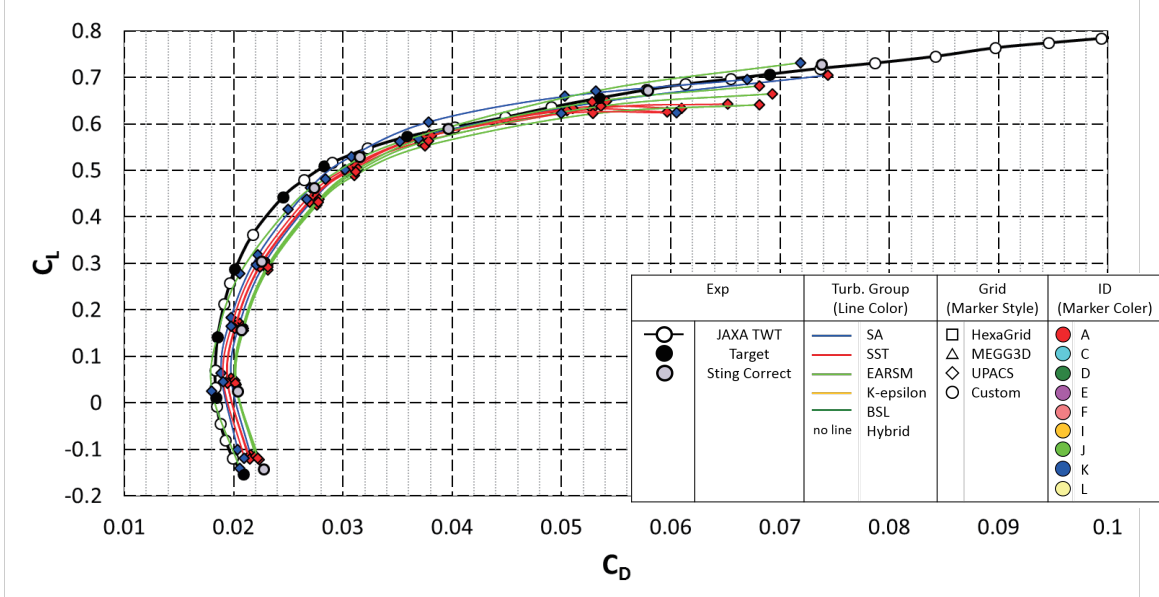
Case 1: Alpha sweep



Comparison between grids

UPACS

CL - CD



CD predicted with UPACS grid is smaller than the others
(This may be caused by the turbulence models used with UPACS grid)

28

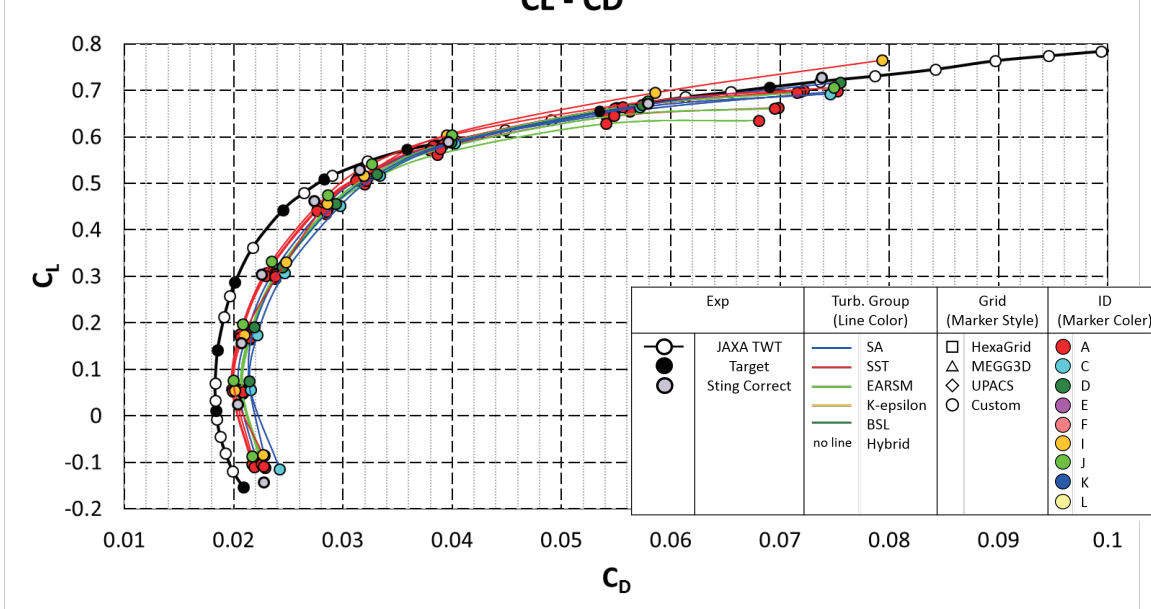
Case 1: Alpha sweep



Comparison between grids

Custom(Cartesian & Polyhedra)

CL - CD



CD predicted with UPACS grid is smaller than the others
 (This may be caused by the turbulence models used with UPACS grid)

29

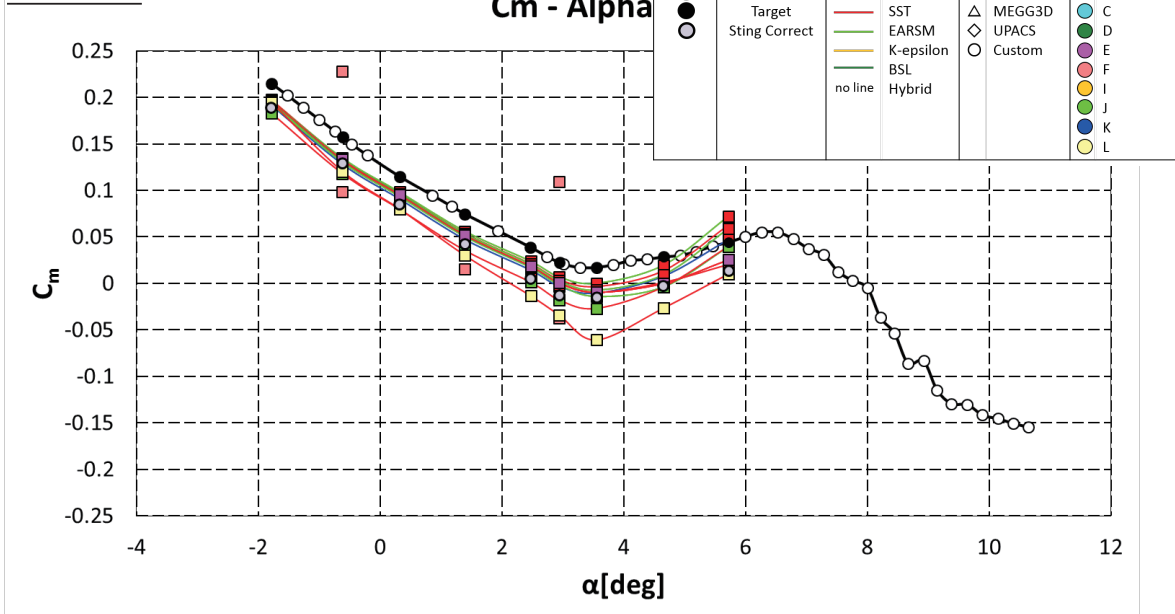
Case 1: Alpha sweep



Comparison between grids

HexaGrid

Cm - Alpha



Cm predicted with HexaGrid is higher than the others
 All data show the pitch-up characteristics for HexaGrid and Custom.

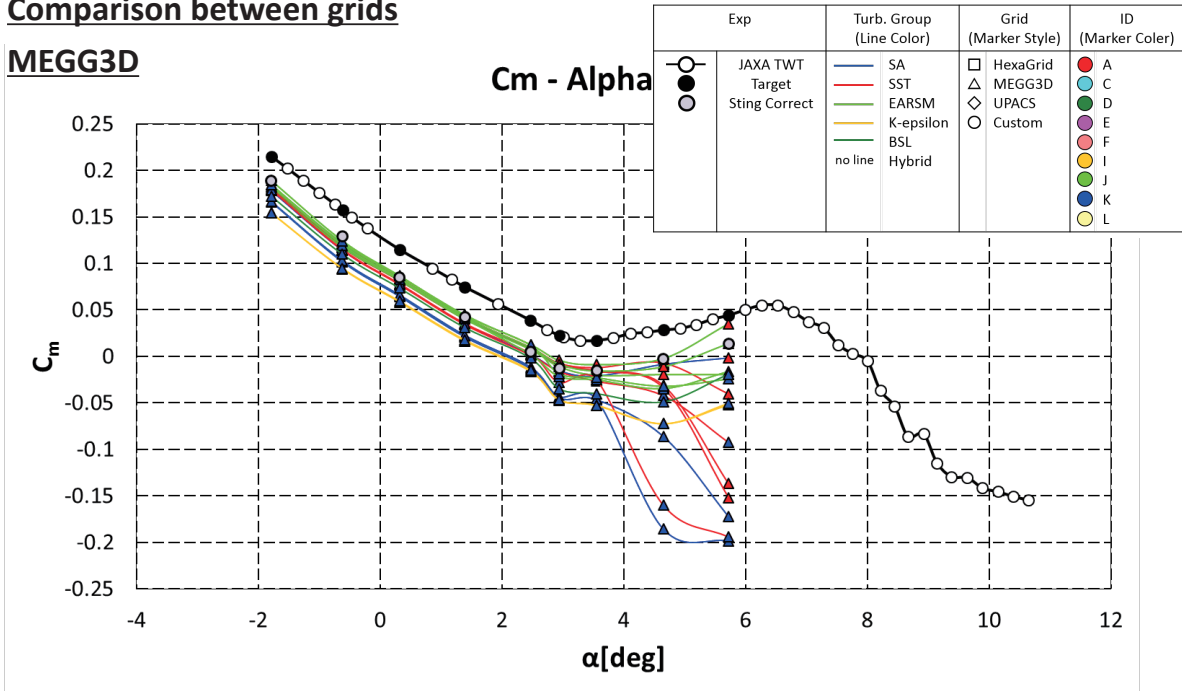
30



Case 1: Alpha sweep

Comparison between grids

MEGG3D



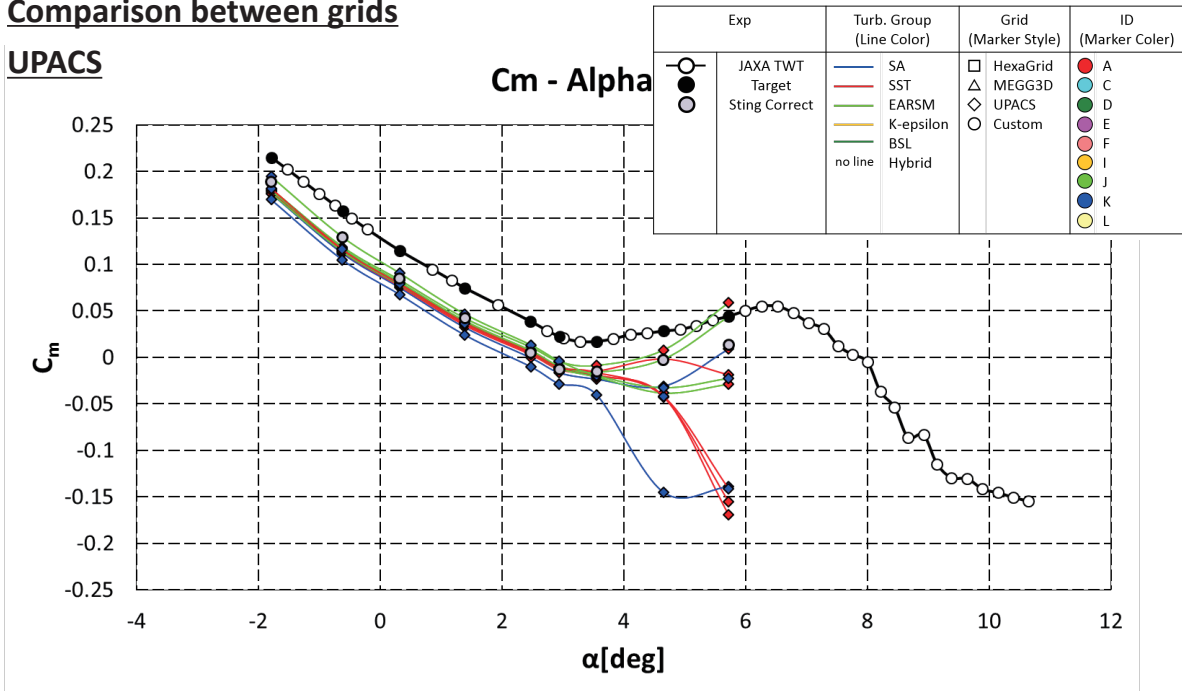
Cm predicted with HexaGrid is higher than the others
 All data show the pitch-up characteristics for HexaGrid and Custom.

Case 1: Alpha sweep



Comparison between grids

UPACS



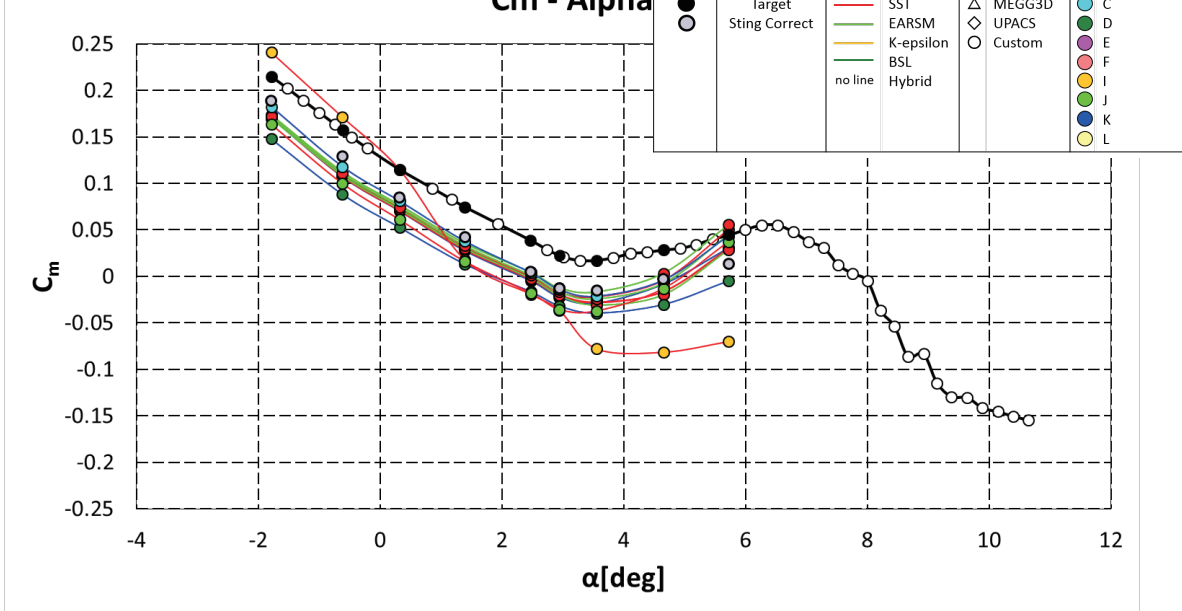
Cm predicted with HexaGrid is higher than the others
 All data show the pitch-up characteristics for HexaGrid and Custom.

Case 1: Alpha sweep



Comparison between grids

Custom(Cartesian & Polyhedra)



Cm predicted with HexaGrid is higher than the others
All data show the pitch-up characteristics for HexaGrid and Custom.

33

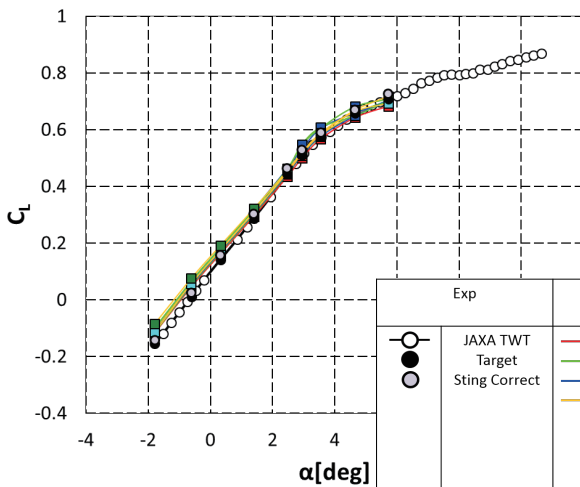
Case 1: Alpha sweep



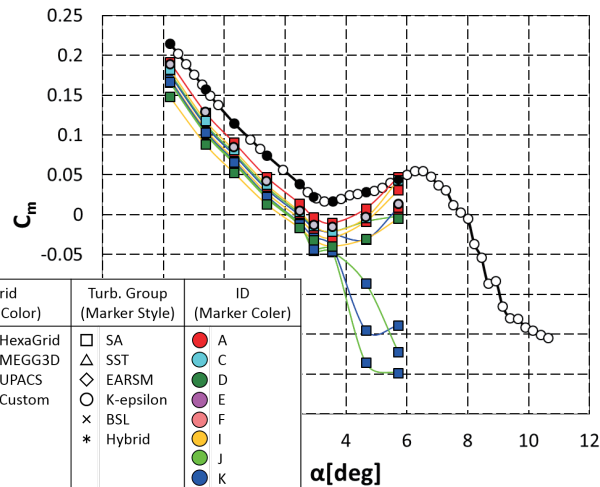
Comparison between turbulence models

SA

CL - Alpha



Cm - Alpha



Exp	Grid (Line Color)	Turb. Group (Marker Style)	ID (Marker Color)
JAXA TWT	HexaGrid	SA	A
Target	MEGG3D	SST	C
Sting Correct	UPACS	EARSM	D
	Custom	K-epsilon	E
		BSL	F
		Hybrid	I
			J
			K
			L

CL: SA > SST > EARSM
Cm: SA < SST < EARSM
EARSM shows pitch-up for high AoA



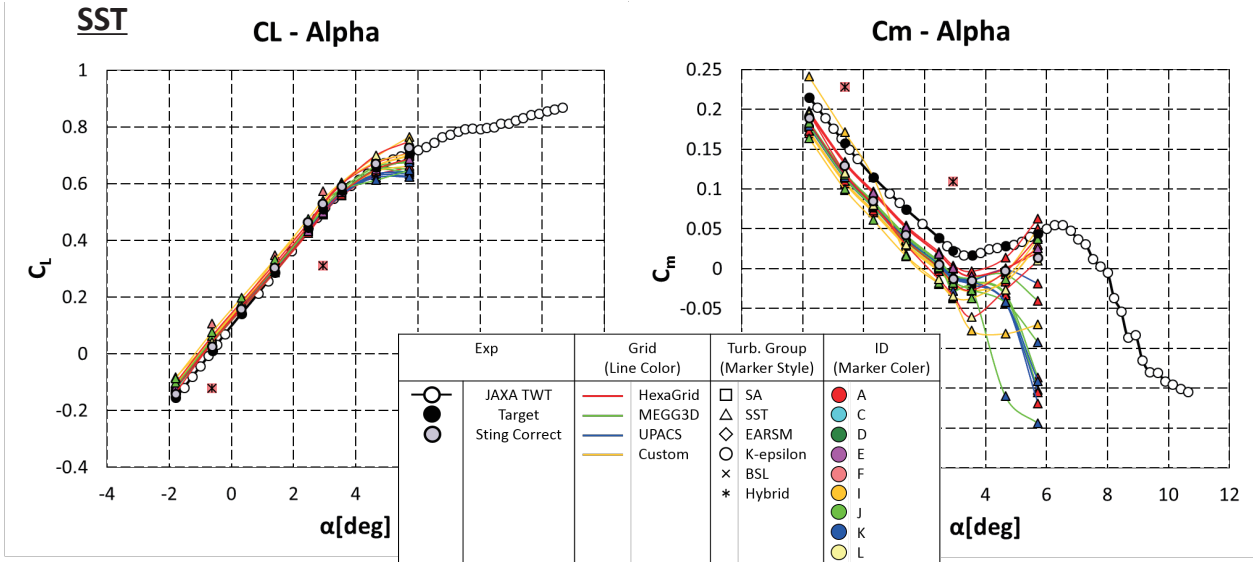
The shock moves forward for EARSM, backward for SA

34



Case 1: Alpha sweep

Comparison between turbulence models



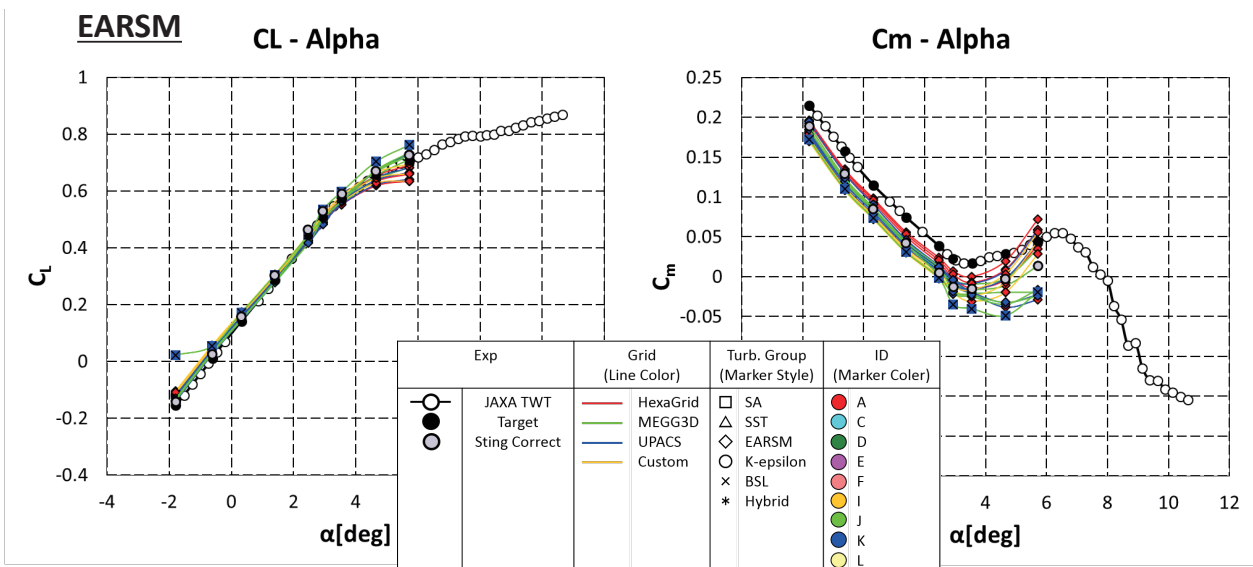
CL: SA > SST > EARSM
 Cm: SA < SST < EARSM
 EARSM shows pitch-up for high AoA

➔ The shock moves forward for EARSM, backward for SA

Case 1: Alpha sweep



Comparison between turbulence models



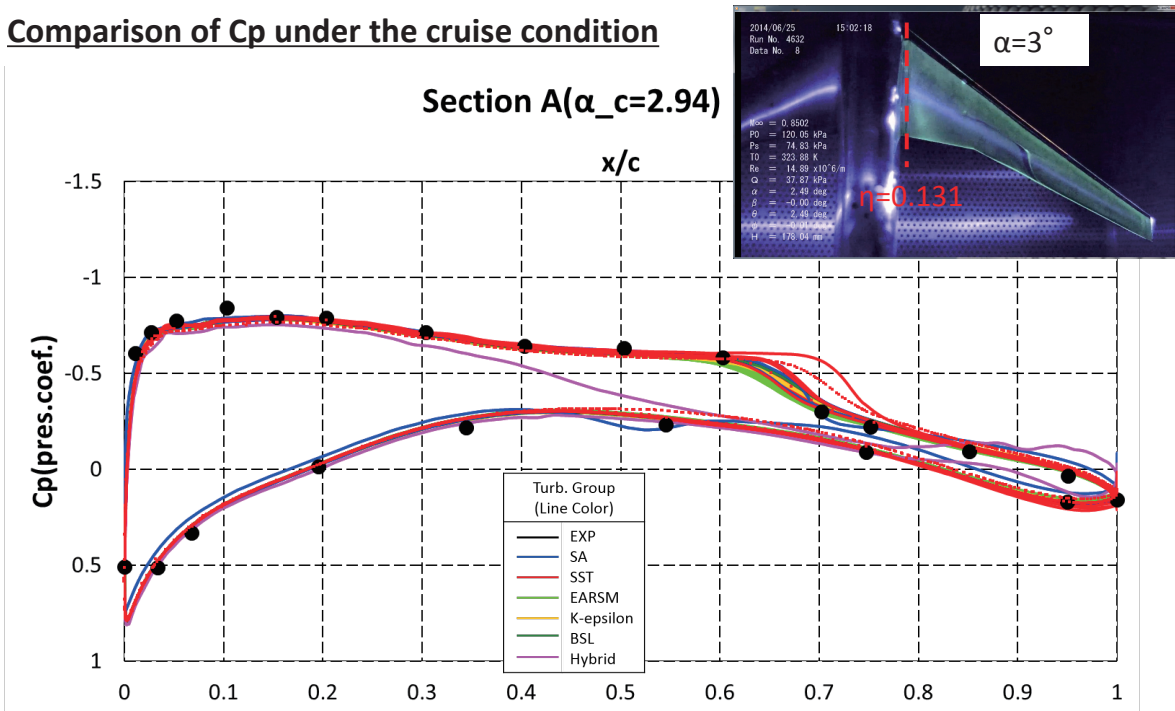
CL: SA > SST > EARSM
 Cm: SA < SST < EARSM
 EARSM shows pitch-up for high AoA

➔ The shock moves forward for EARSM, backward for SA

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

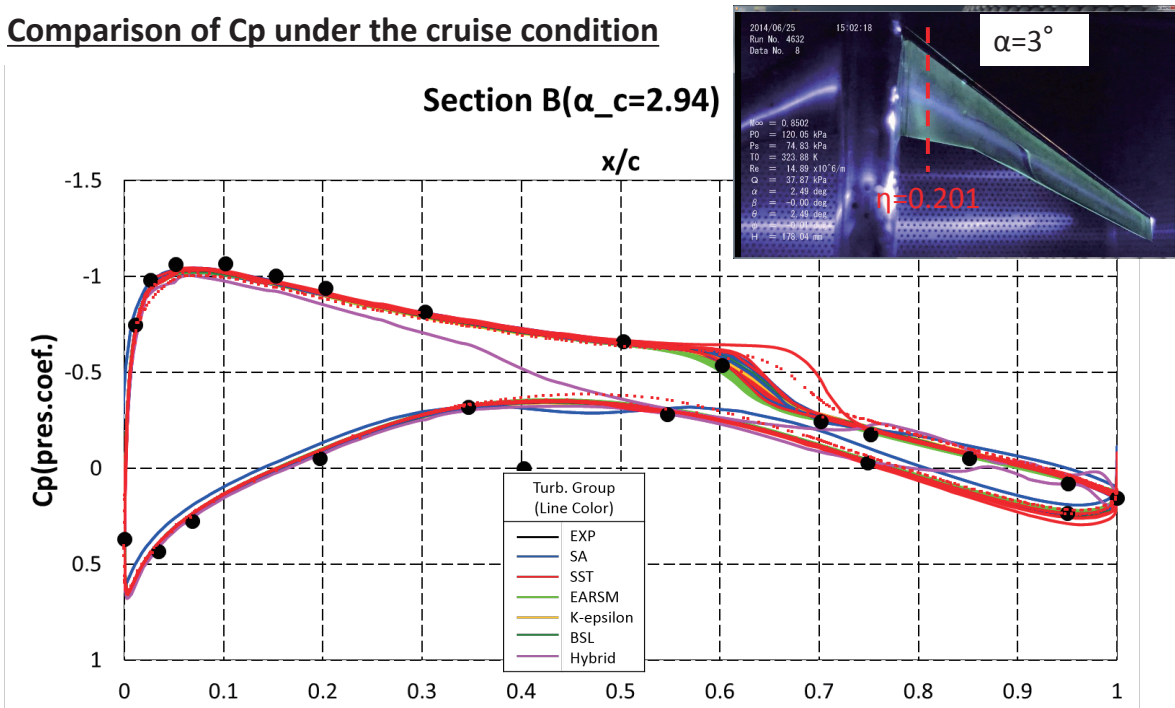


37

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

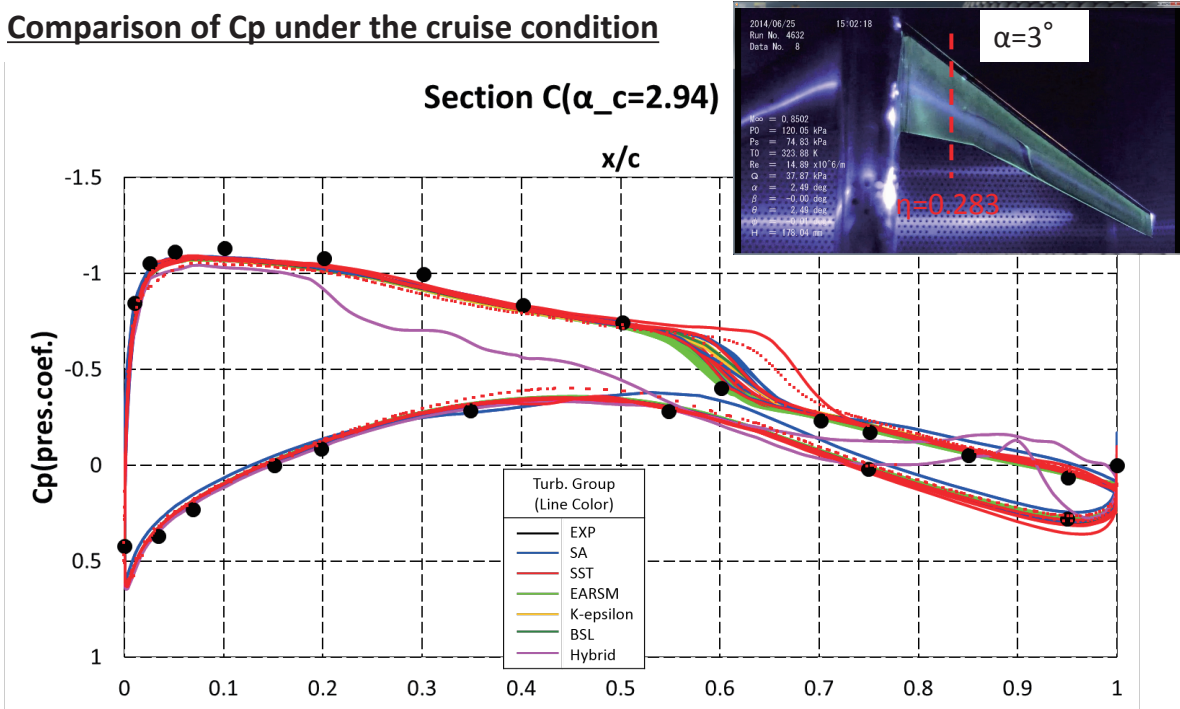


38



Case 1: Cp at cruise

Comparison of Cp under the cruise condition

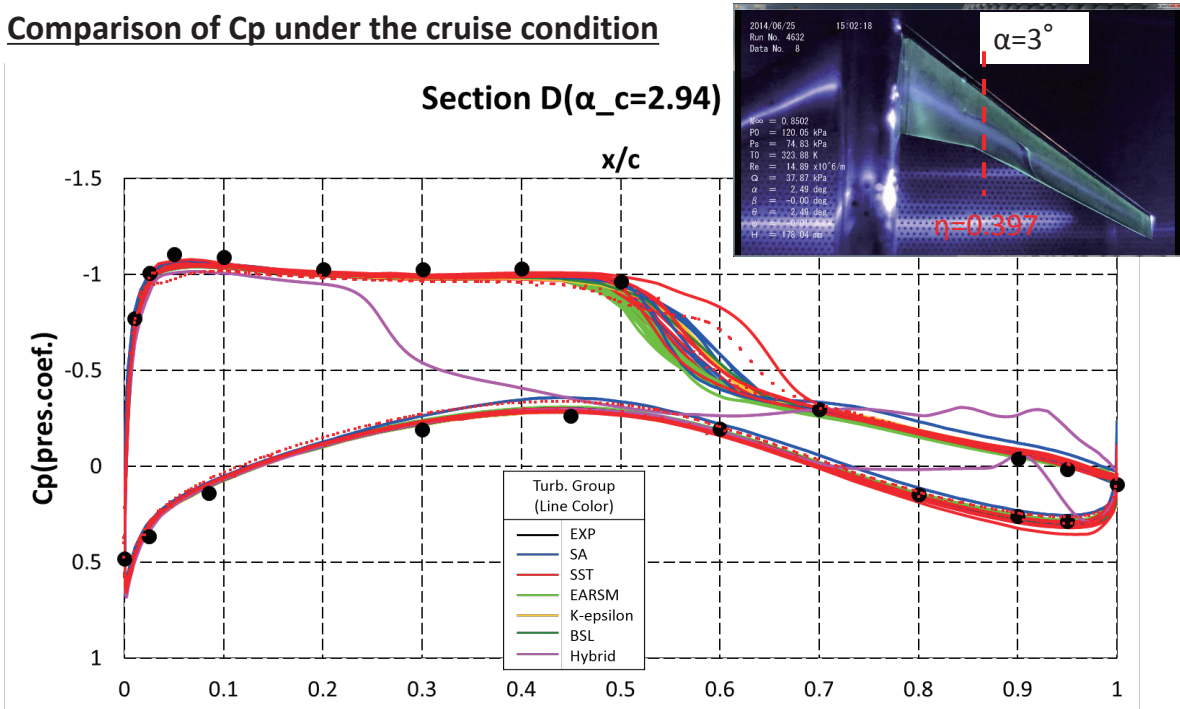


39

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

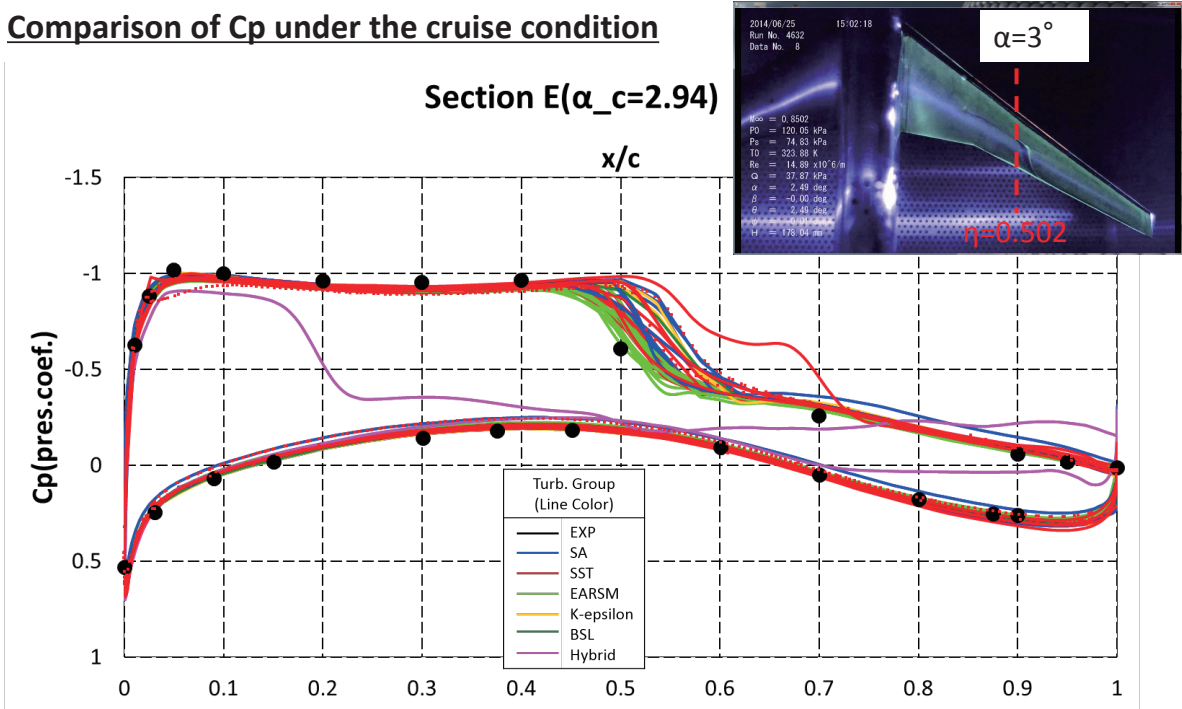


40

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

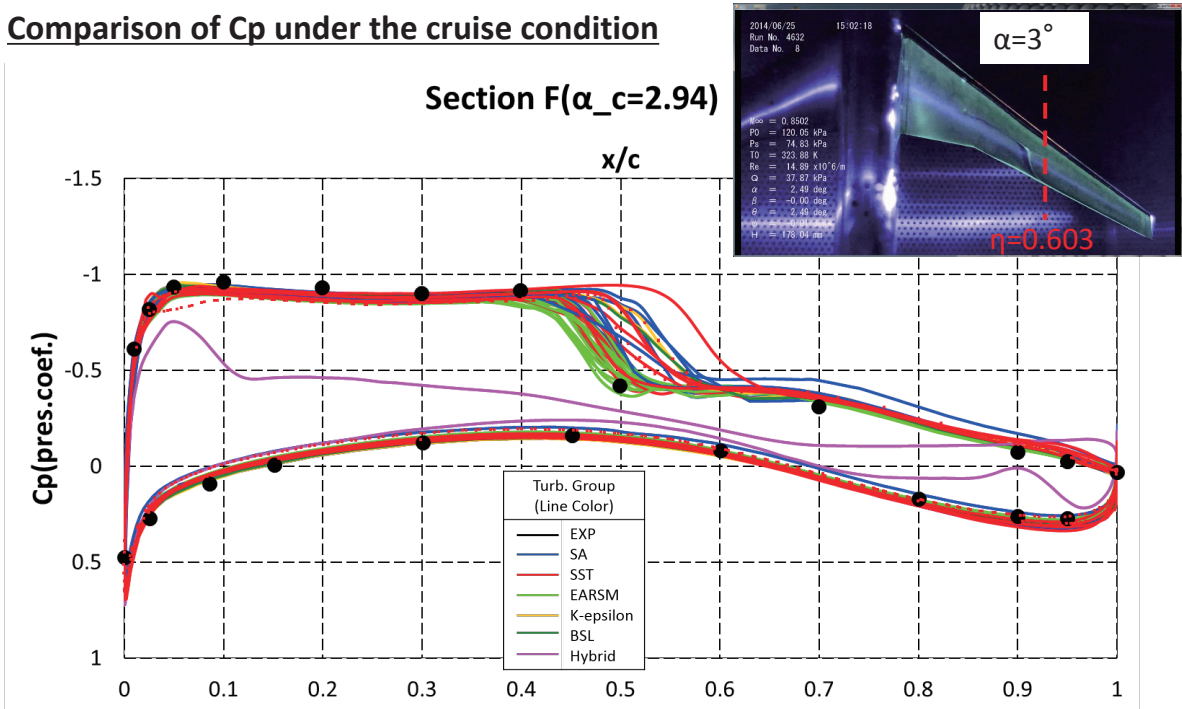


41

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

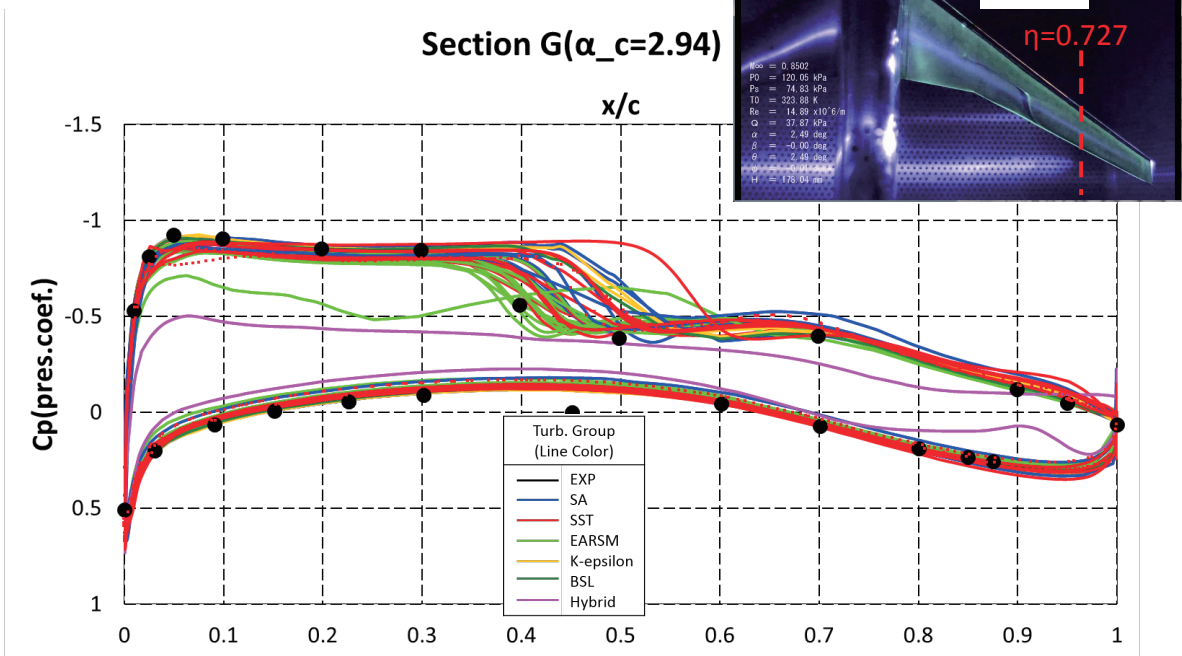


42



Case 1: Cp at cruise

Comparison of Cp under the cruise condition

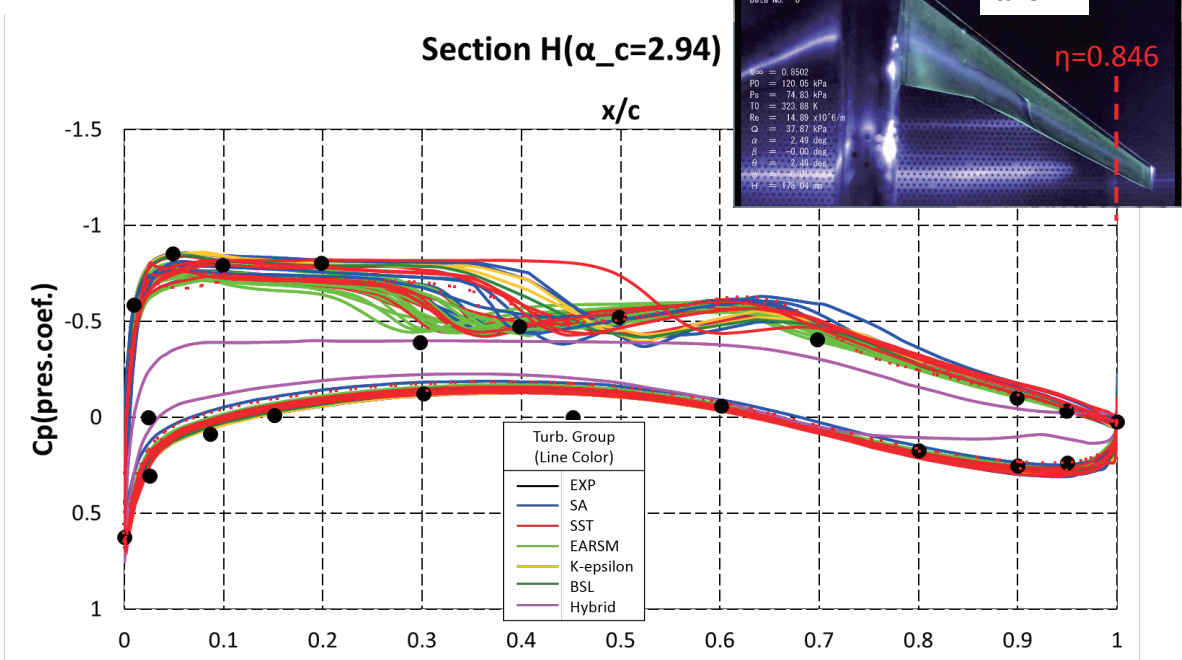


43

Case 1: Cp at cruise



Comparison of Cp under the cruise condition

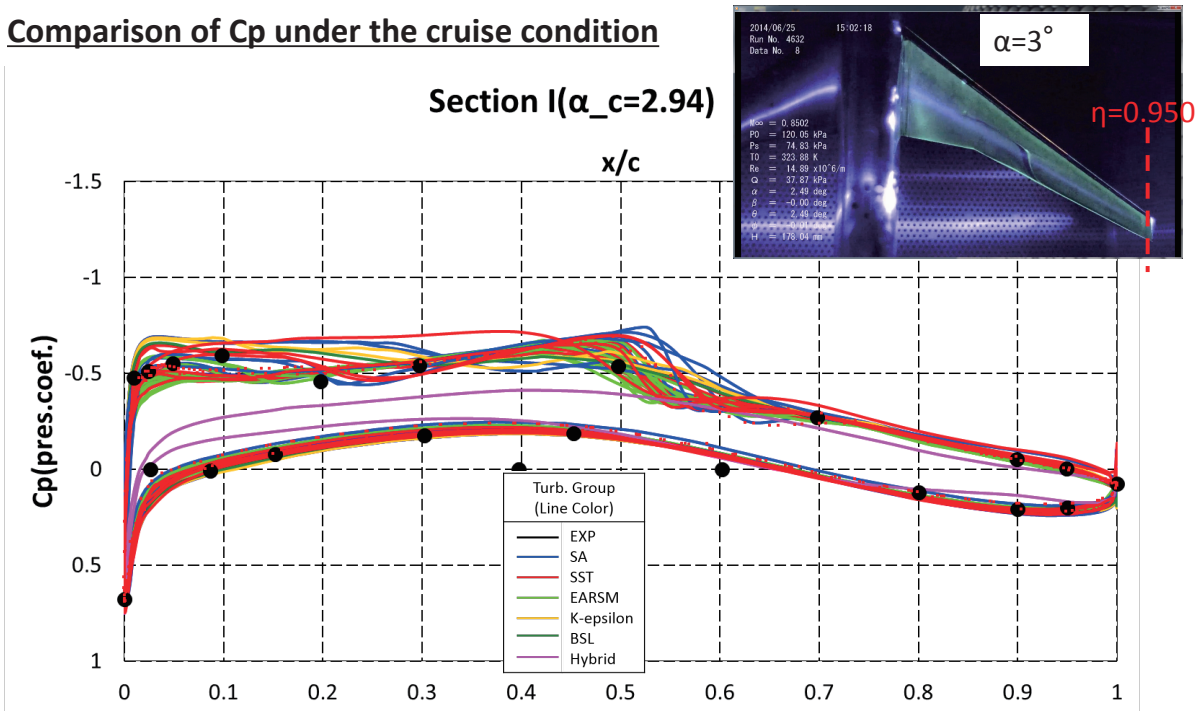


44

Case 1: Cp at cruise



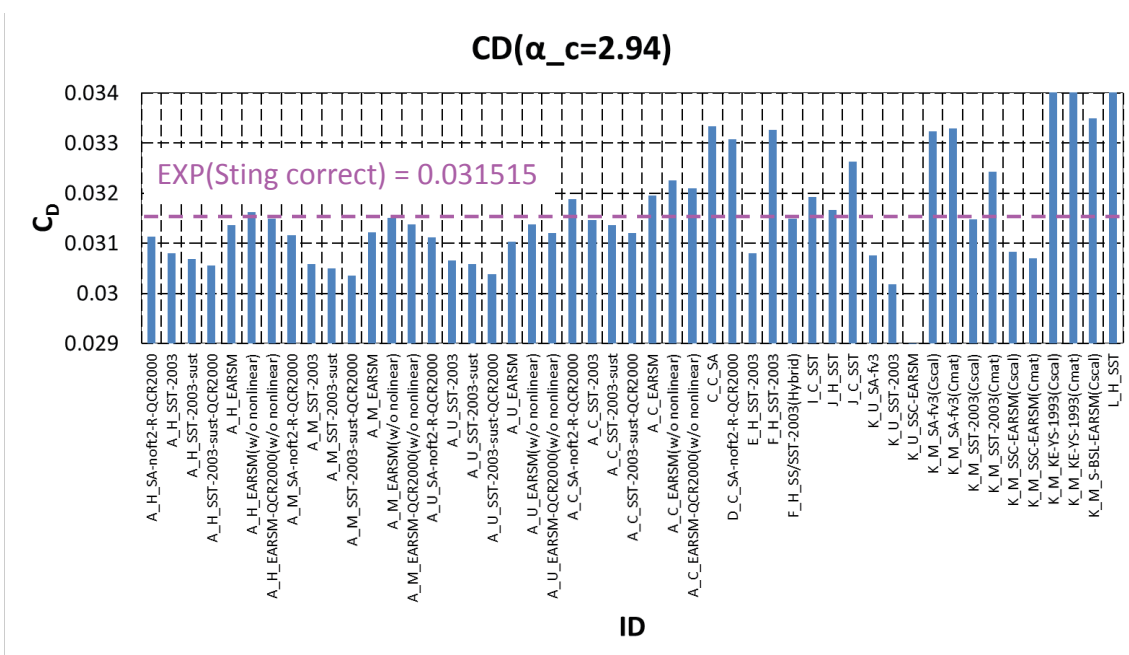
Comparison of Cp under the cruise condition



EARSM predicts the shock location well for all cross sections.

45

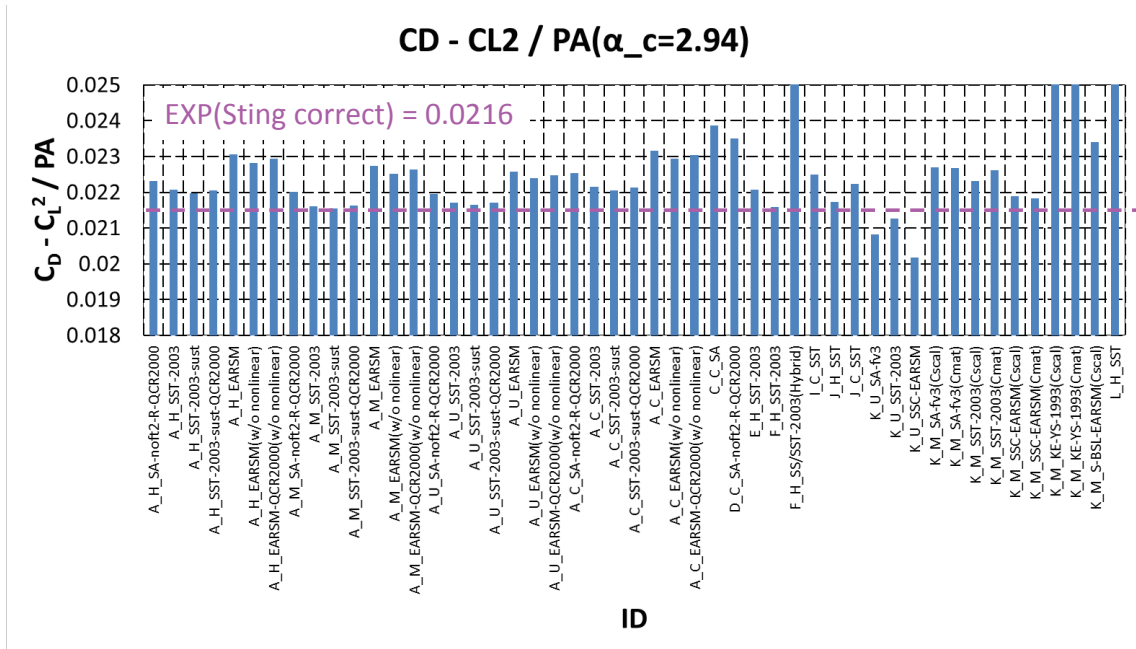
Case 1: Aerodynamic coefficients at cruise



46

Case 1: Aerodynamic coefficients at cruise

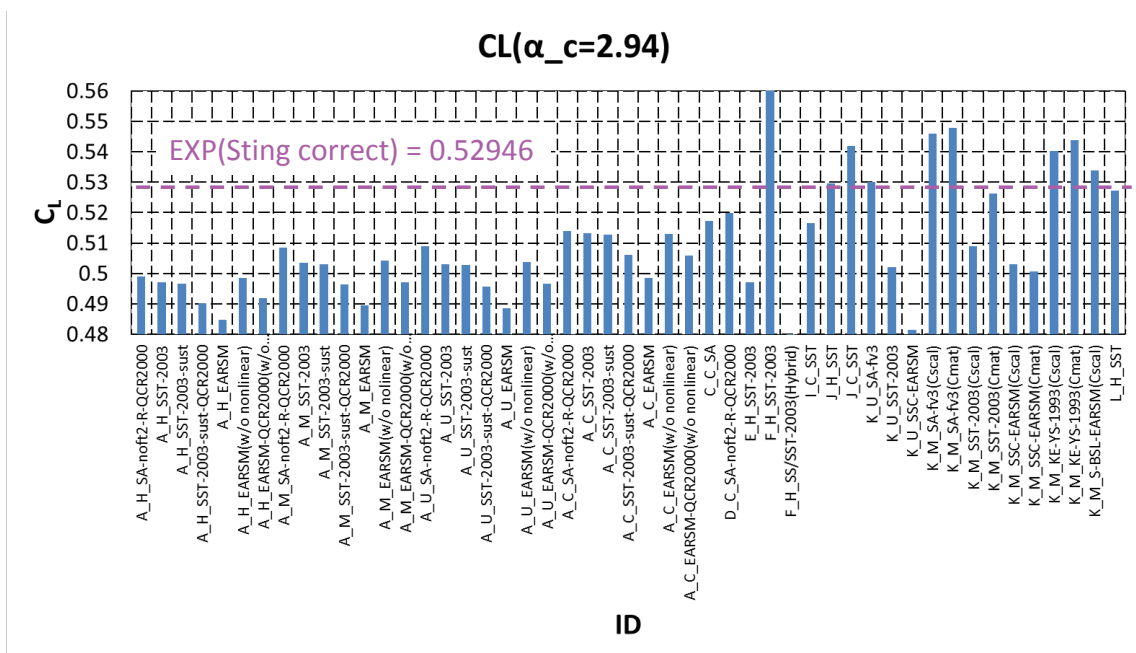
Idealized profile drag CDi



CFD is higher than EXP.

47

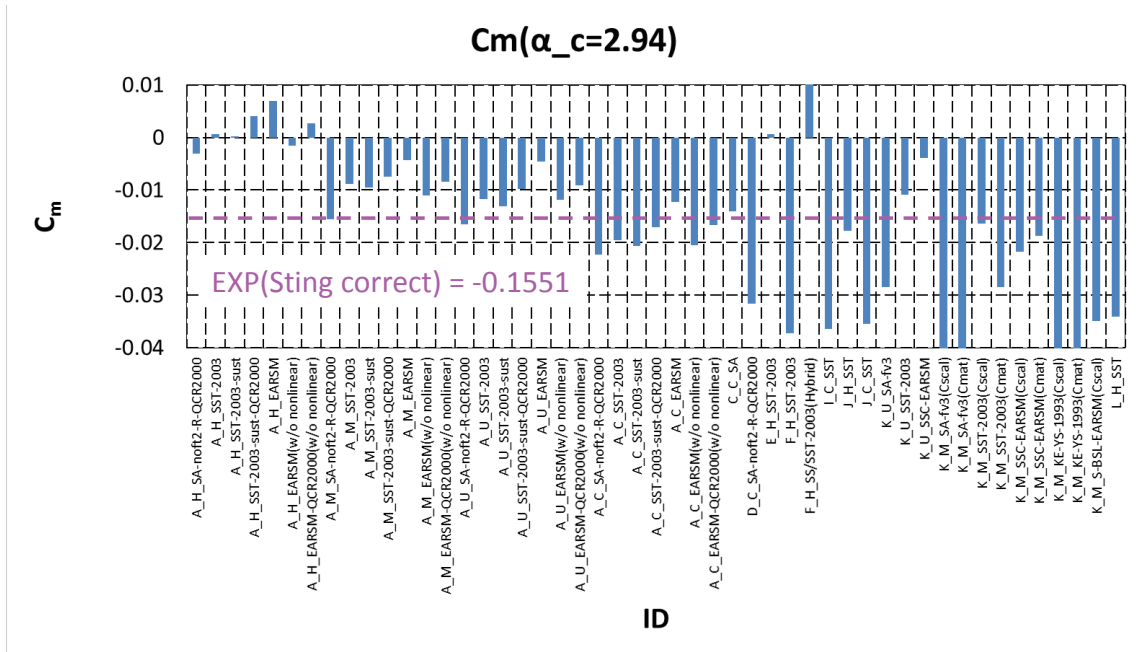
Case 1: Aerodynamic coefficients at cruise



CFD is lower than EXP.

48

Case 1: Aerodynamic coefficients at cruise



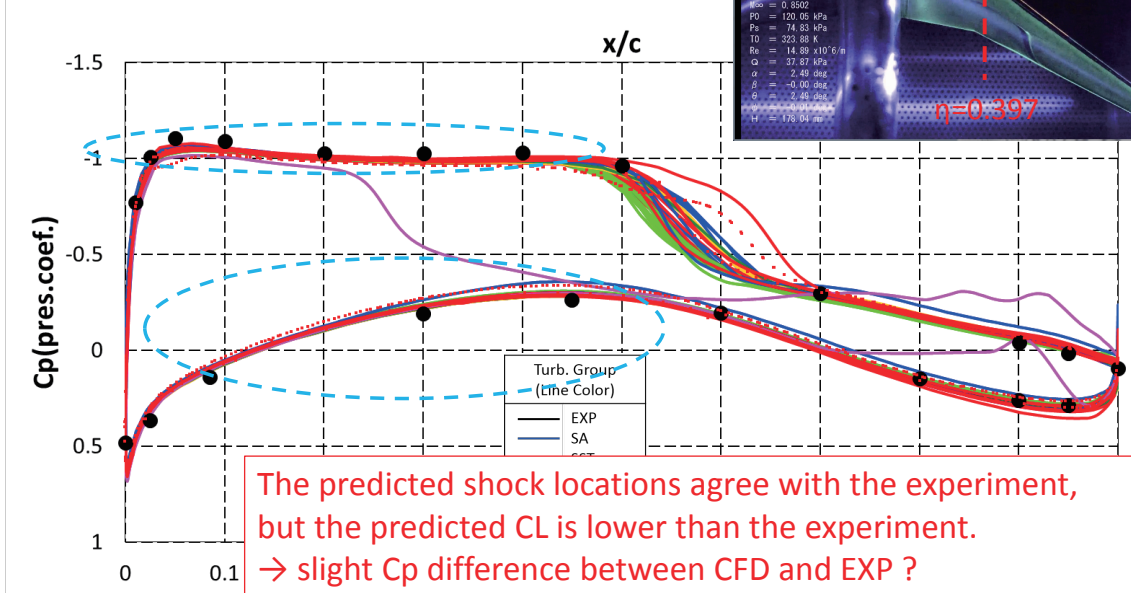
49

Case 1: Cp at cruise

Comparison of Cp under the cruise condition

Section D

Section D ($\alpha_c=2.94$)

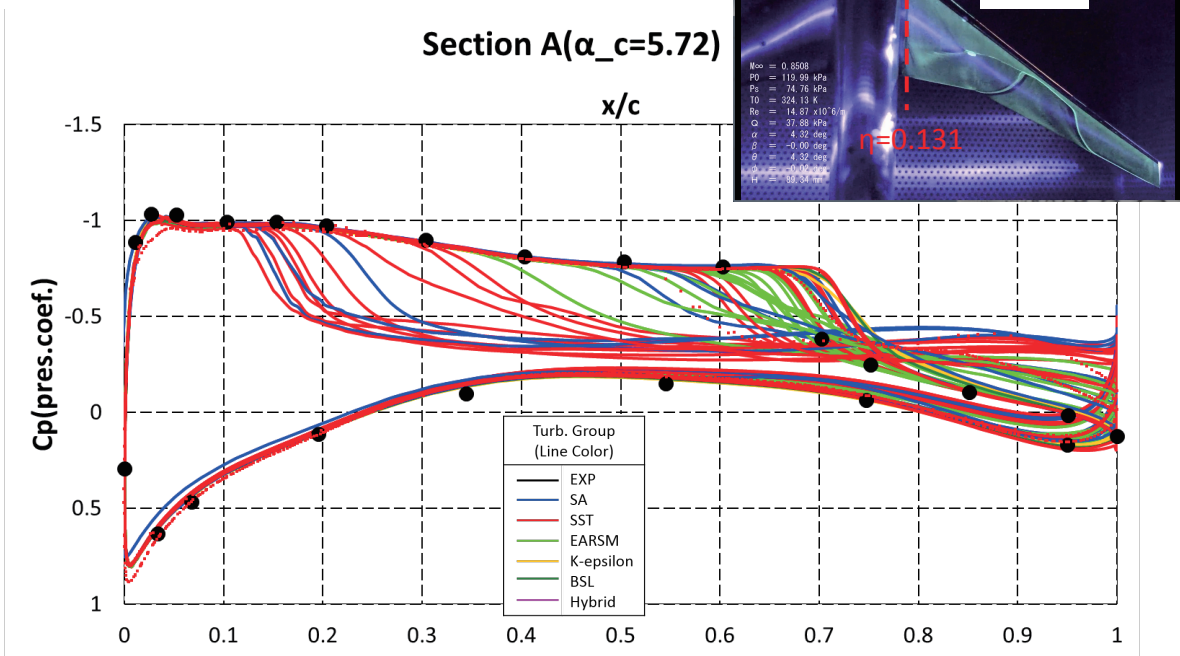


50



Case 1: Cp at high AoA

Comparison of Cp under the high AoA condition



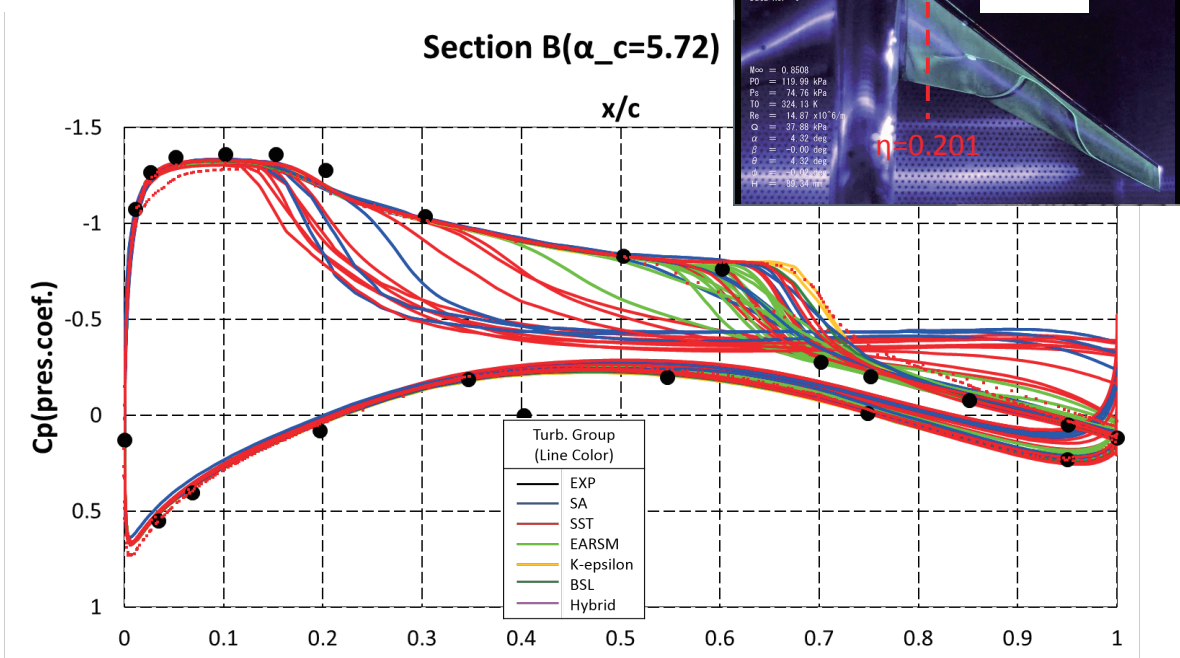
The shock location moves forward due to the separation.
 The separation is small for EARSM

51

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition



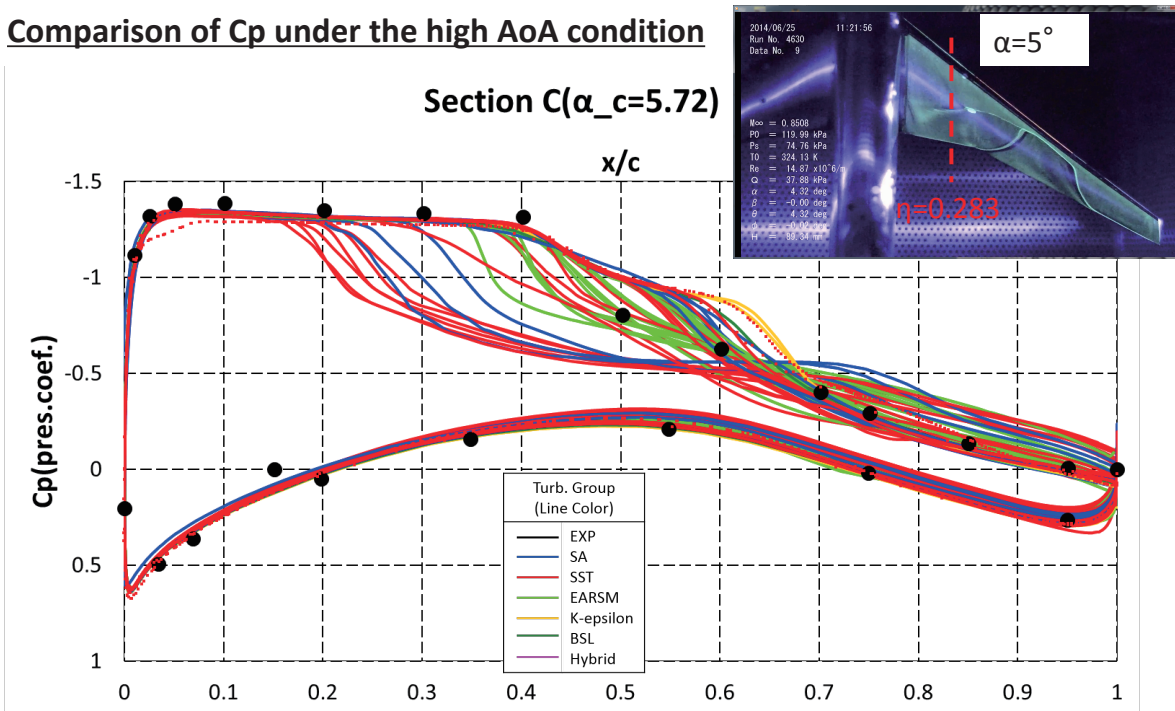
The shock location moves forward due to the separation.
 The separation is small for EARSM

52

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition

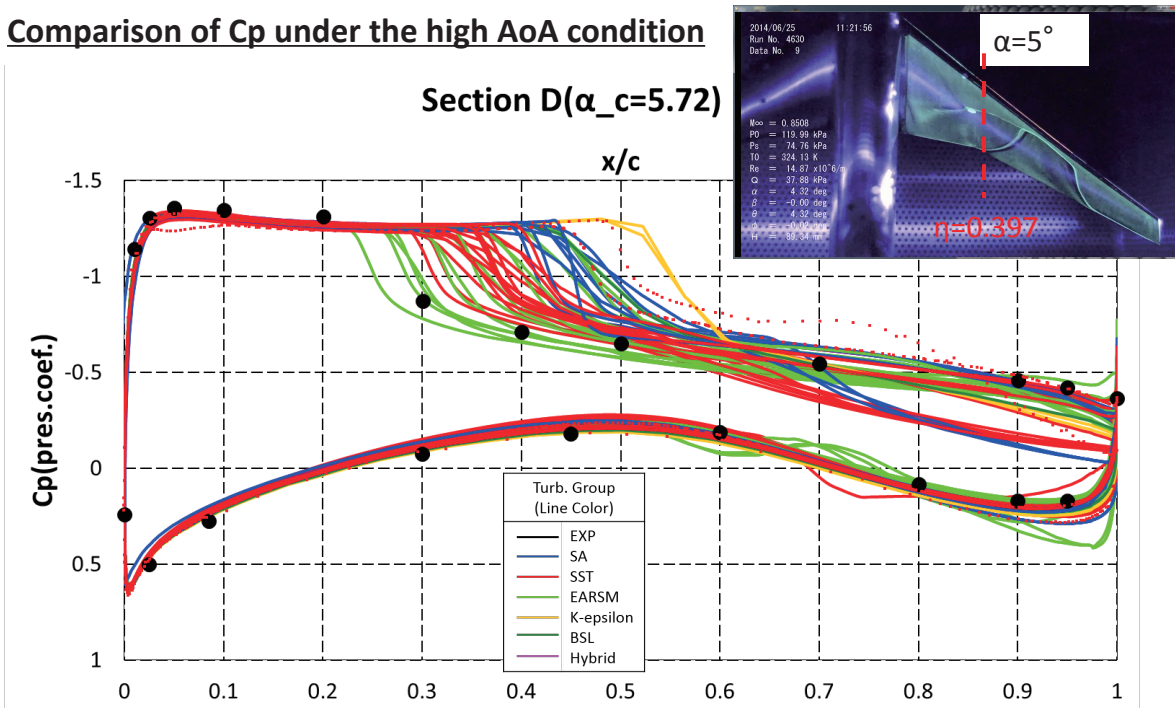


53

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition



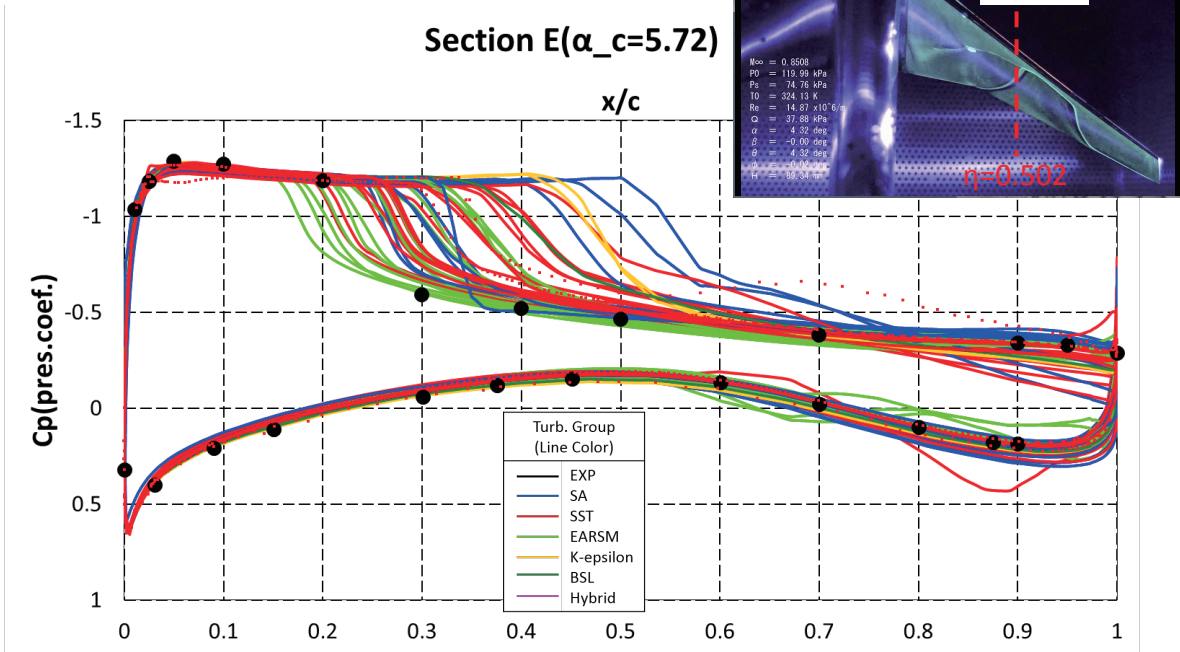
The turbulence model dependency is clear at this section.
 The order of shock location is EARSM, SST, SA, k-ε.

54



Case 1: Cp at high AoA

Comparison of Cp under the high AoA condition

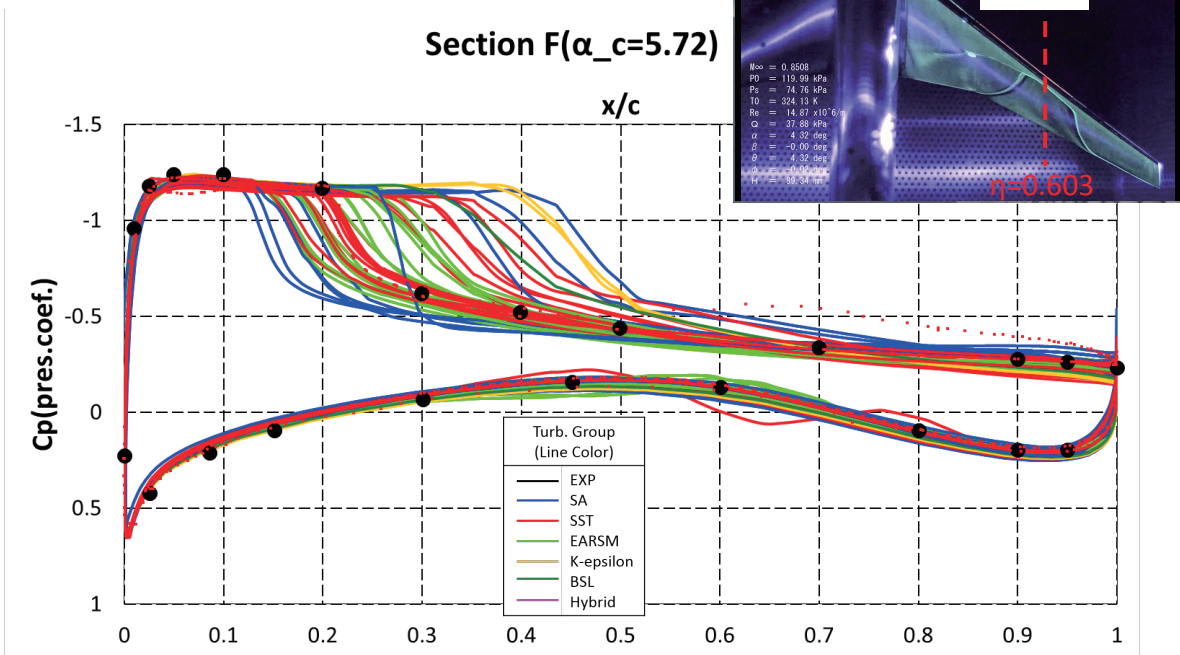


55

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition

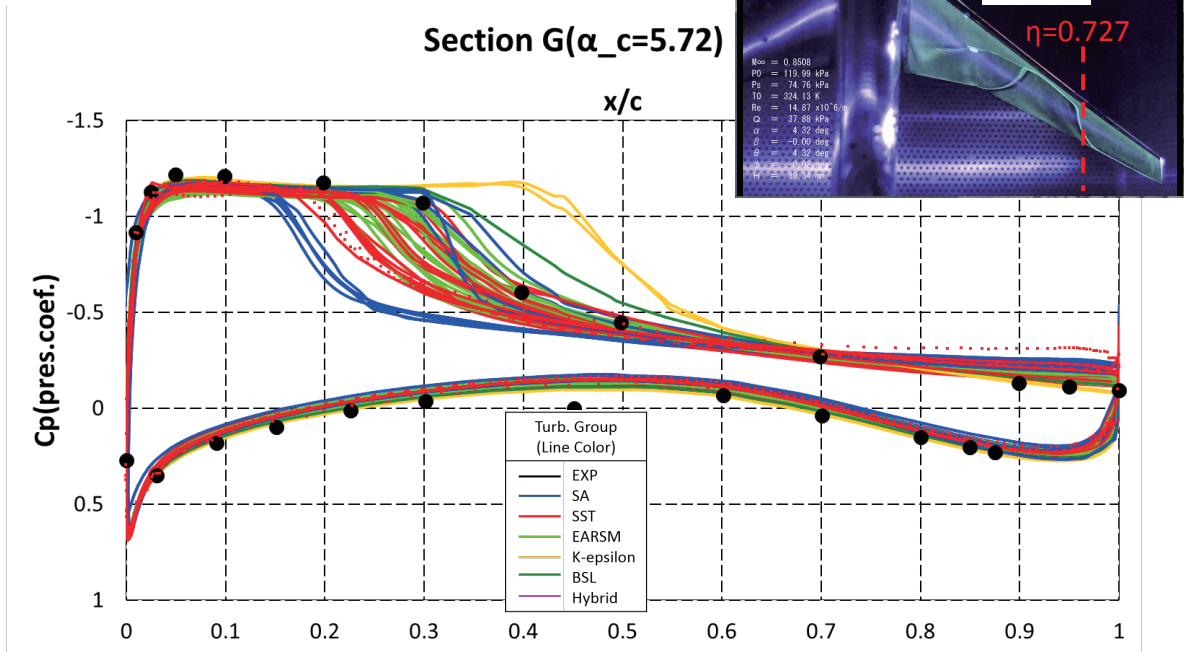


56

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition

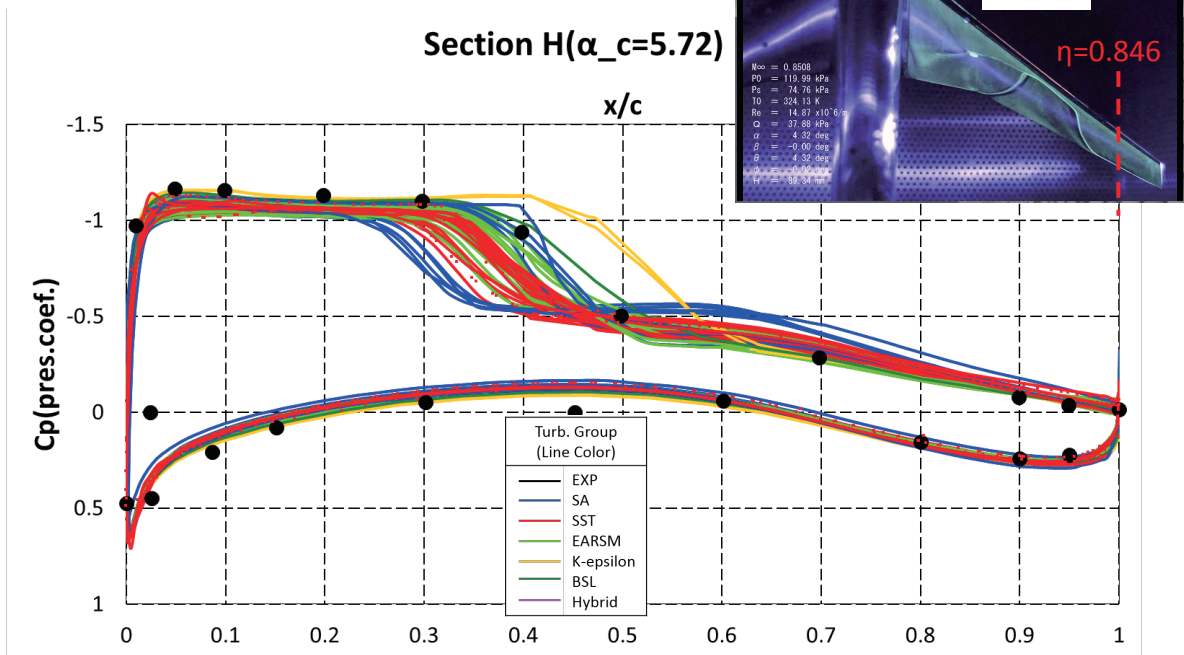


57

Case 1: Cp at high AoA



Comparison of Cp under the high AoA condition



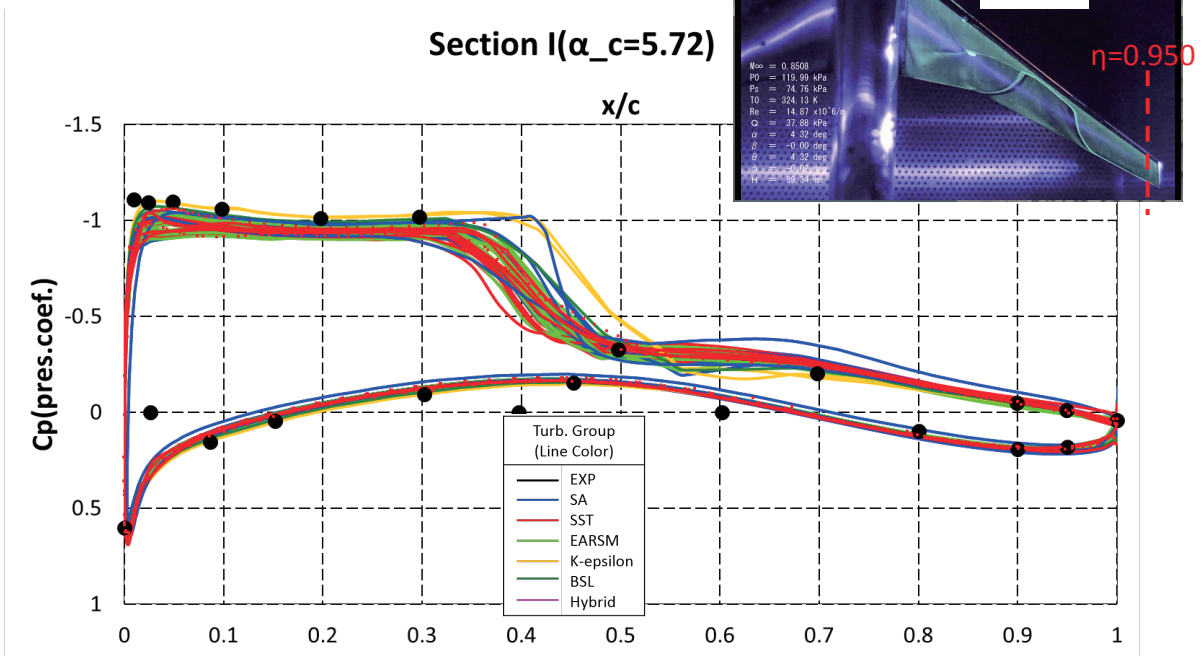
The variation is small for outboard sections (The flow is attached here).

58



Case 1: Cp at high AoA

Comparison of Cp under the high AoA condition

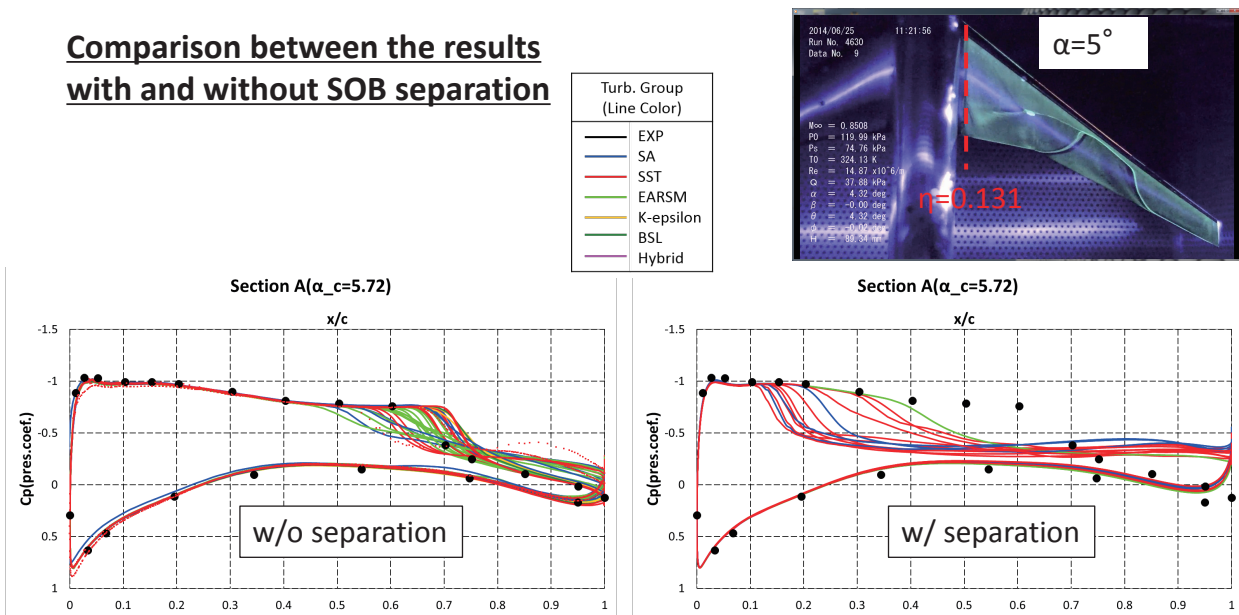


The variation is small for outboard sections (The flow is attached here).

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation



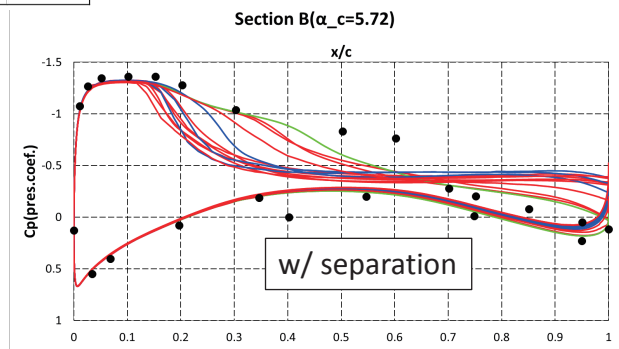
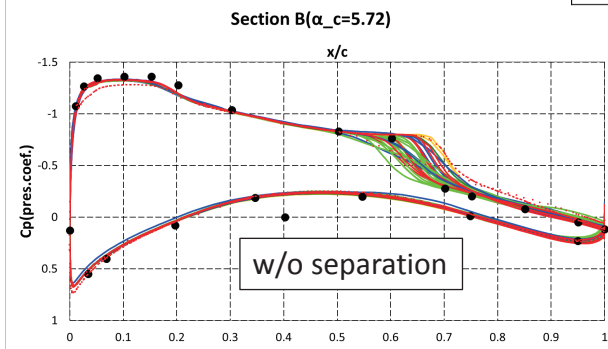
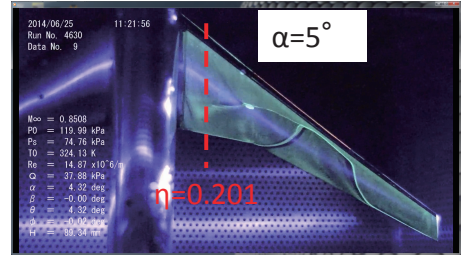
We classify the results into two groups with and without the side-of-body separation.

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black)
SA (Blue)
SST (Red)
EARSM (Green)
K-epsilon (Yellow)
BSL (Cyan)
Hybrid (Purple)



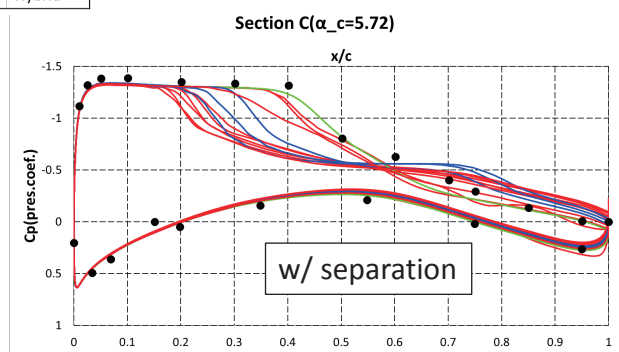
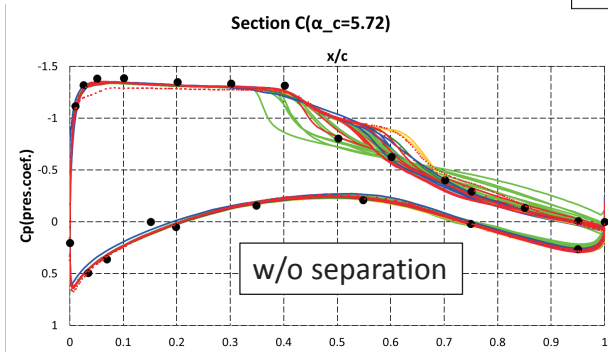
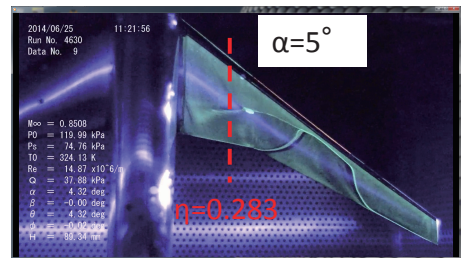
61

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black)
SA (Blue)
SST (Red)
EARSM (Green)
K-epsilon (Yellow)
BSL (Cyan)
Hybrid (Purple)



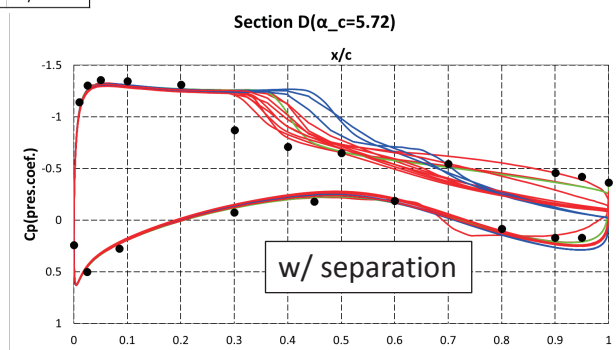
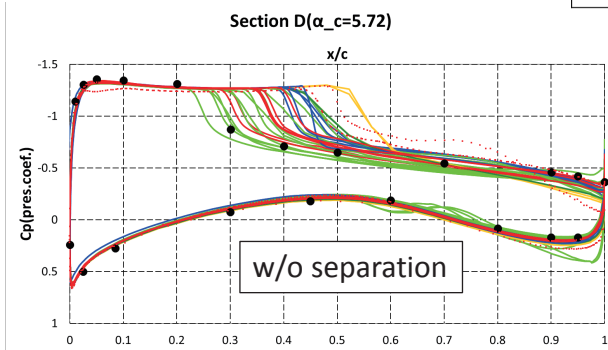
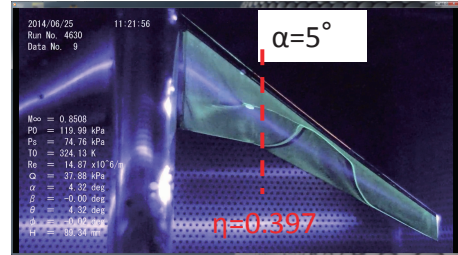
62



Case 1: Cp at high AoA

Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black)
SA (Blue)
SST (Red)
EARSM (Green)
K-epsilon (Yellow)
BSL (Cyan)
Hybrid (Purple)



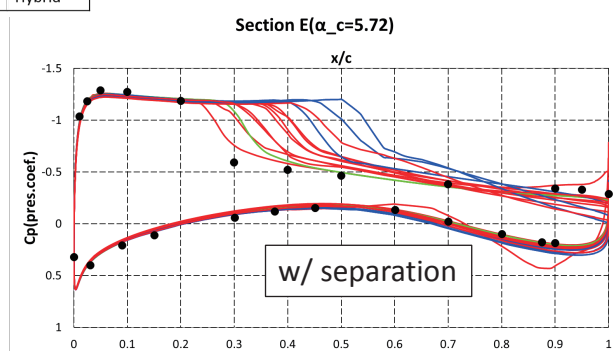
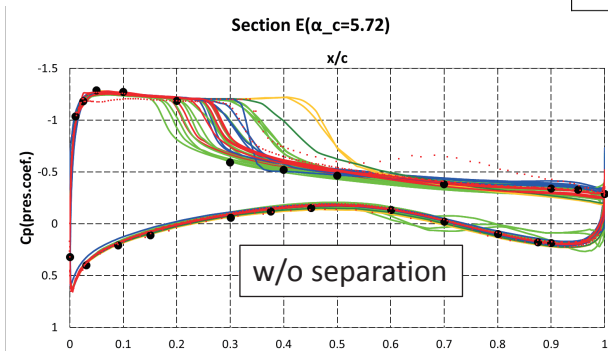
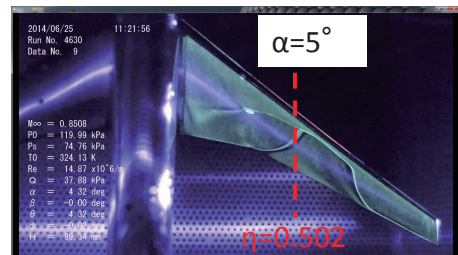
The shock wave locations are different even if the separation size is same at the wing root.
The order is EARSM, SST, SA, k-e.

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black)
SA (Blue)
SST (Red)
EARSM (Green)
K-epsilon (Yellow)
BSL (Cyan)
Hybrid (Purple)



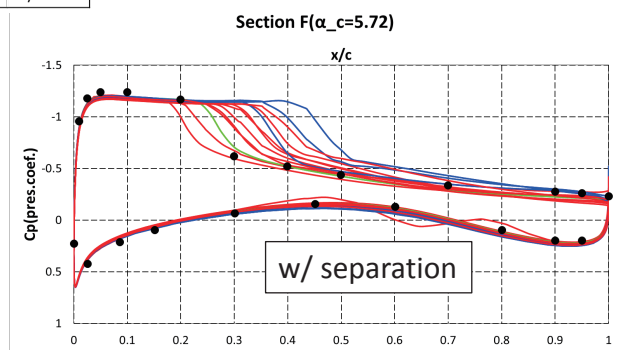
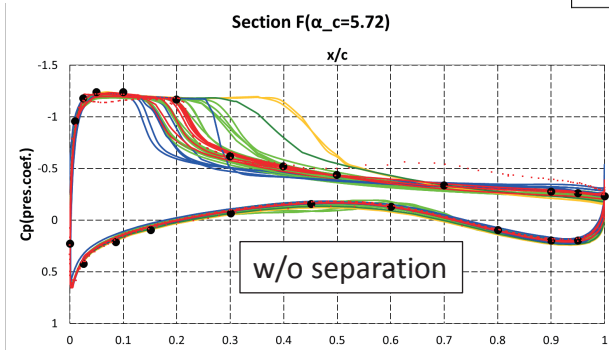
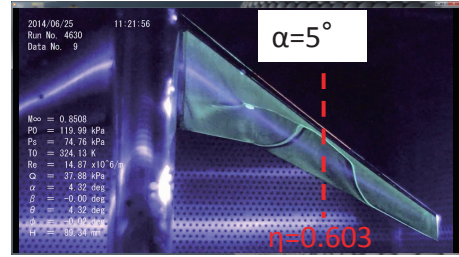
The order is EARSM, SST, SA, k-e.

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group	(Line Color)
EXP	Black
SA	Blue
SST	Red
EARSM	Green
K-epsilon	Yellow
BSL	Cyan
Hybrid	Purple



The order is SA, SST, EARSM, k-e.

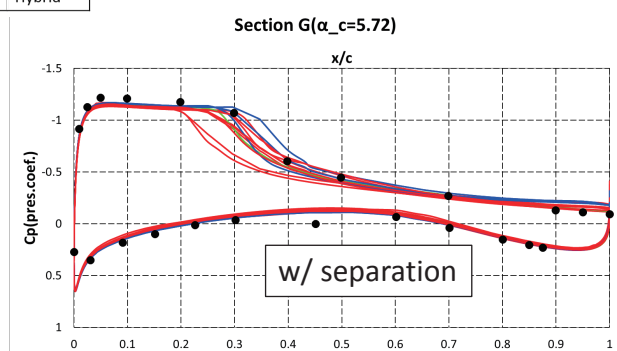
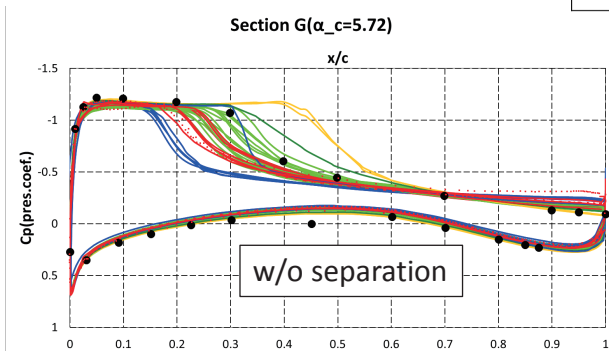
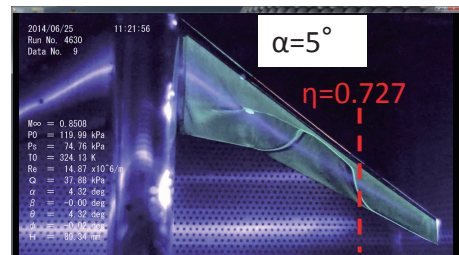
65

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group	(Line Color)
EXP	Black
SA	Blue
SST	Red
EARSM	Green
K-epsilon	Yellow
BSL	Cyan
Hybrid	Purple



The order is SA, SST, EARSM, k-e.

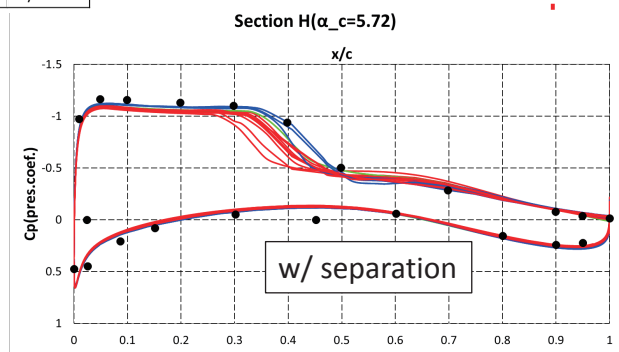
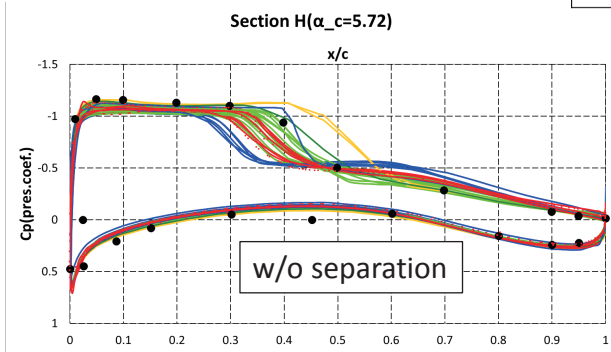
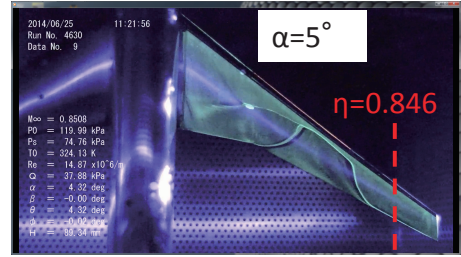
66



Case 1: Cp at high AoA

Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black dots)
SA (Blue line)
SST (Red line)
EARSM (Green line)
K-epsilon (Yellow line)
BSL (Cyan line)
Hybrid (Purple line)



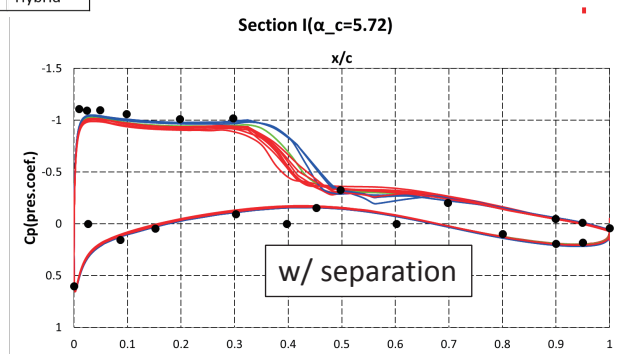
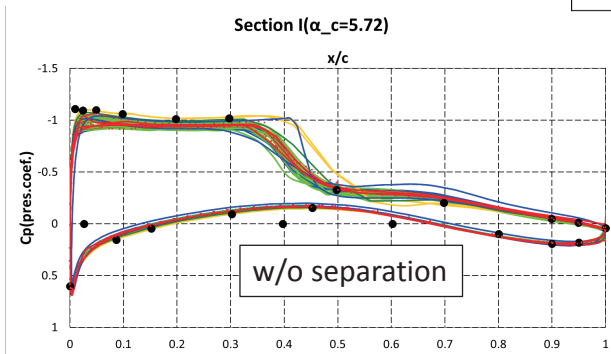
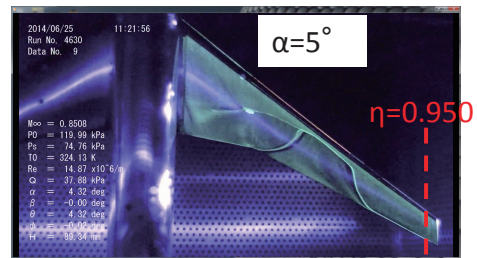
The order is SA, SST, EARSM, k-e.

Case 1: Cp at high AoA



Comparison between the results with and without SOB separation

Turb. Group (Line Color)
EXP (Black dots)
SA (Blue line)
SST (Red line)
EARSM (Green line)
K-epsilon (Yellow line)
BSL (Cyan line)
Hybrid (Purple line)

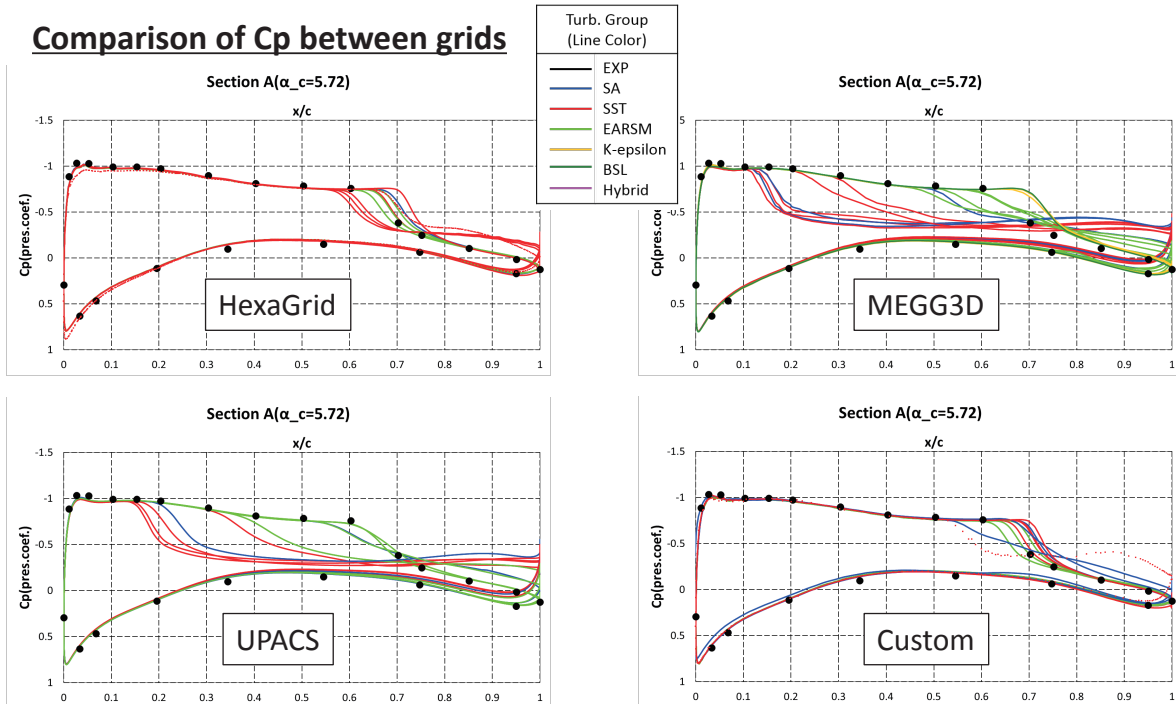


EARSM predicts the shock location well for all cross sections.

Case 1: Cp at high AoA



Comparison of Cp between grids

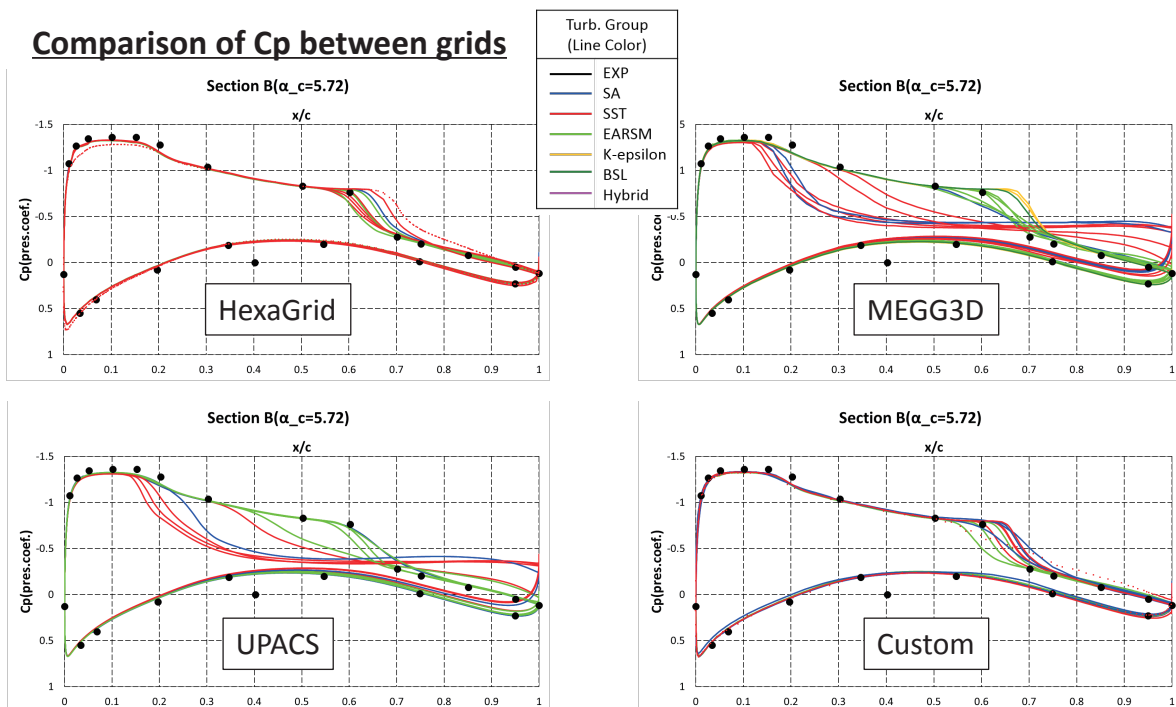


There are no side-of-body separations for HexaGrid
 whereas there are side-of-body separations for MEGG3D and UPACS

Case 1: Cp at high AoA



Comparison of Cp between grids

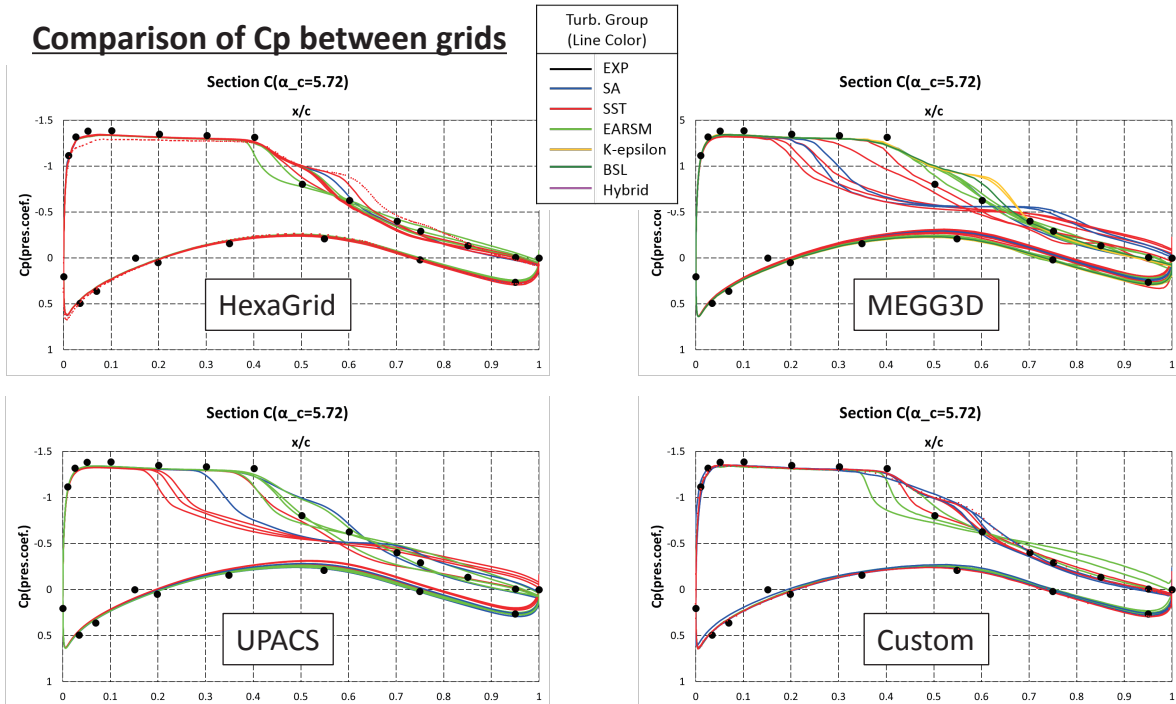


There are no side-of-body separations for HexaGrid
 whereas there are side-of-body separations for MEGG3D and UPACS



Case 1: Cp at high AoA

Comparison of Cp between grids

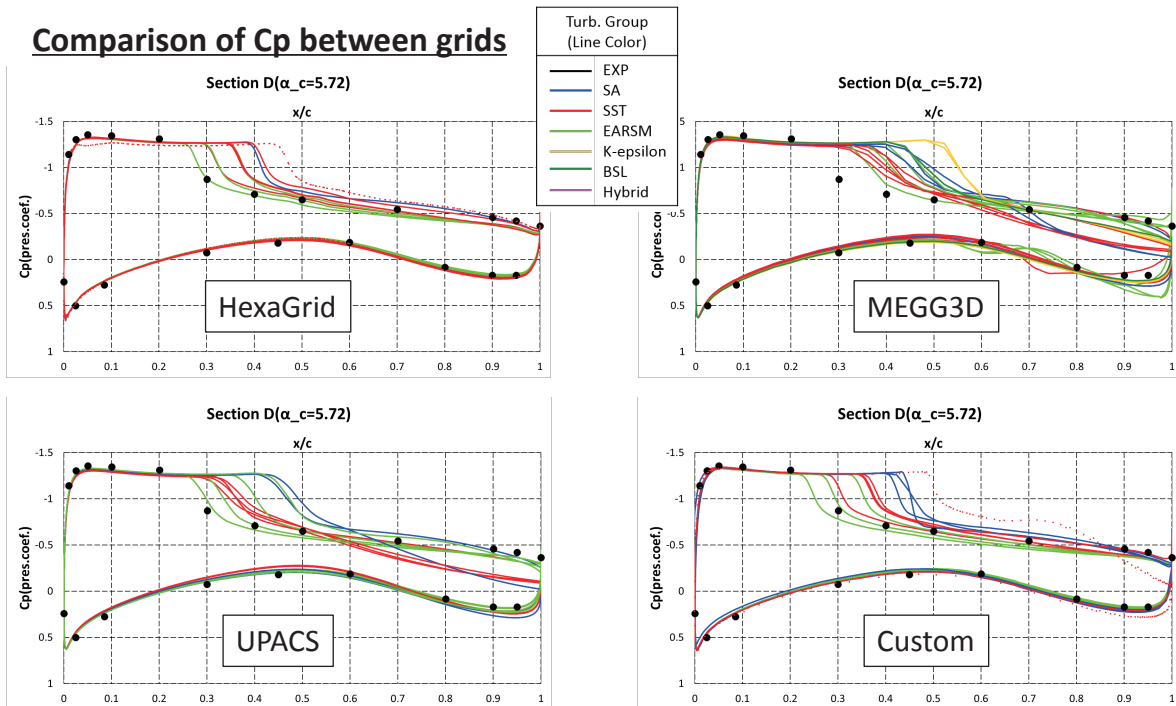


71

Case 1: Cp at high AoA



Comparison of Cp between grids

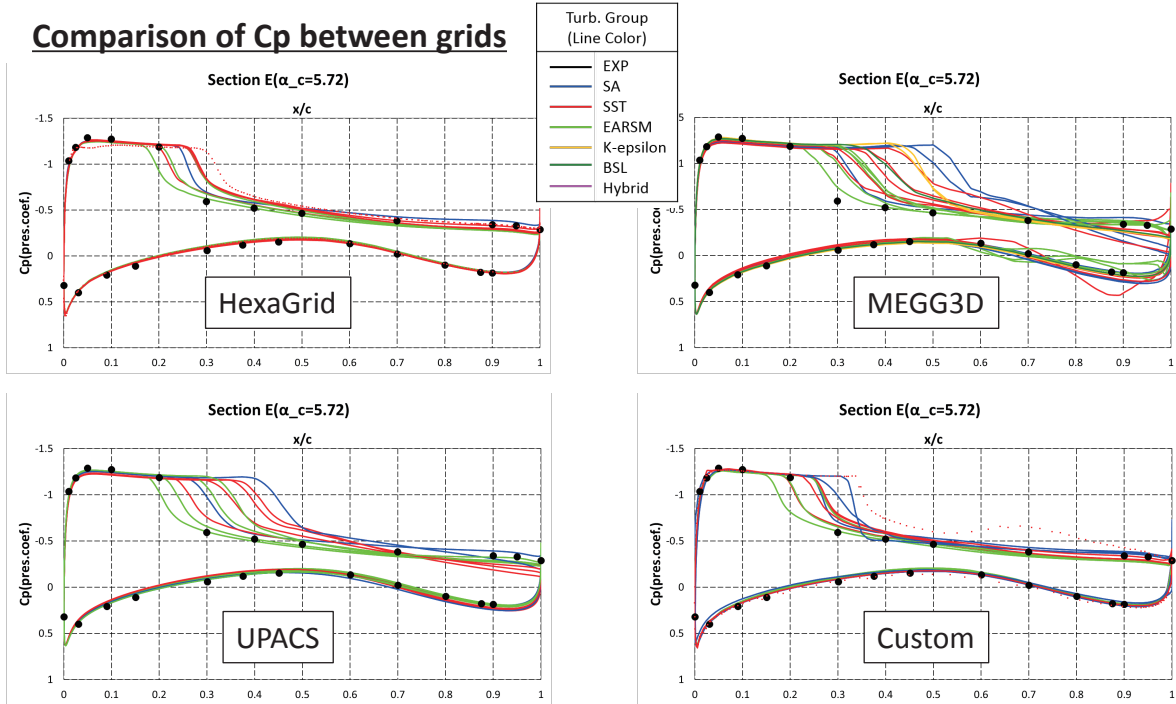


72

Case 1: Cp at high AoA



Comparison of Cp between grids

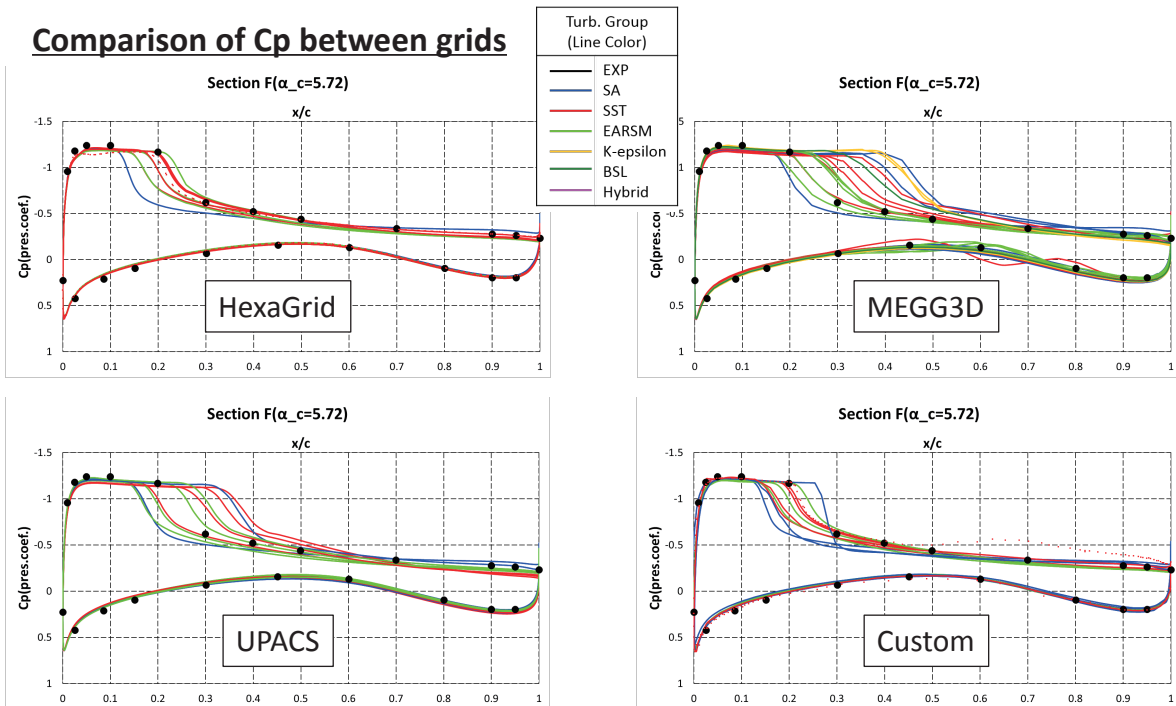


73

Case 1: Cp at high AoA



Comparison of Cp between grids

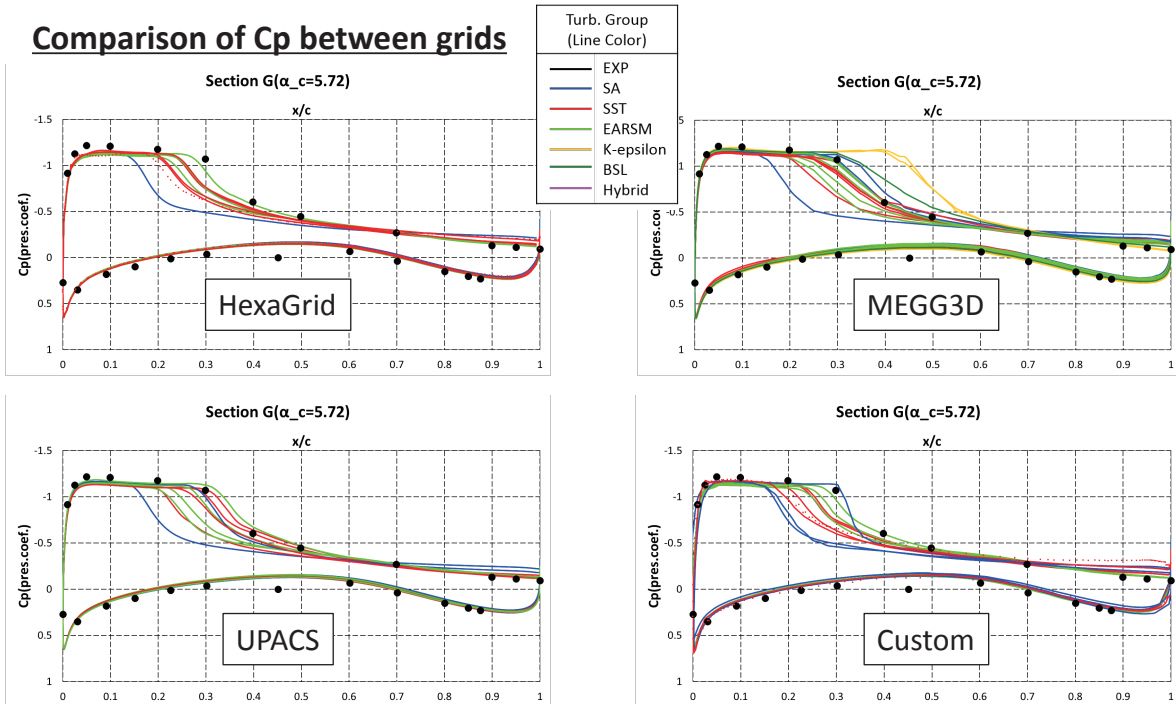


74



Case 1: Cp at high AoA

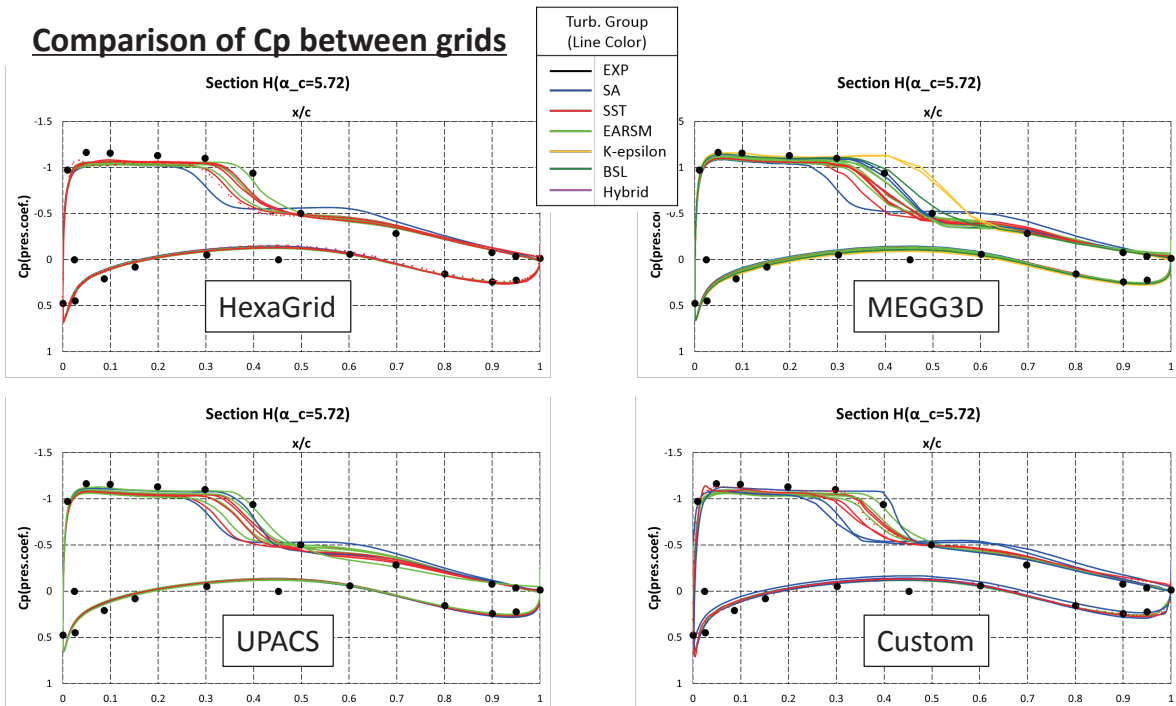
Comparison of Cp between grids



Case 1: Cp at high AoA



Comparison of Cp between grids

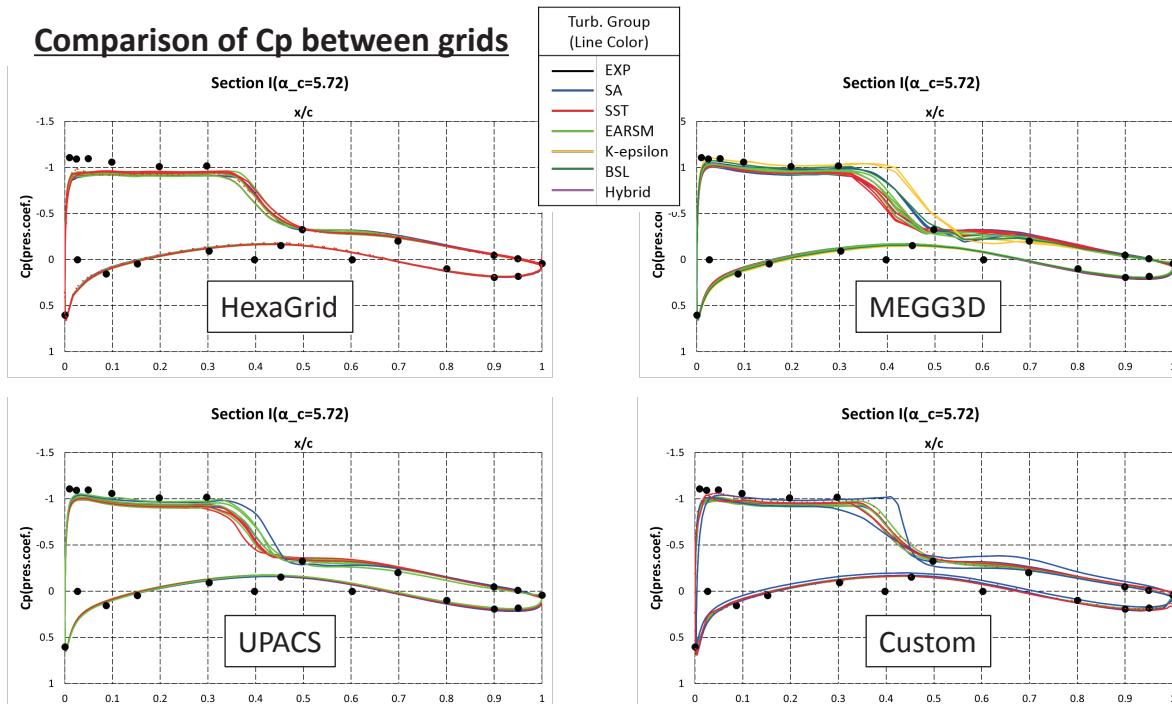


The peak of negative pressure is small for HexaGrid

Case 1: Cp at high AoA



Comparison of Cp between grids



The peak of negative pressure is small for HexaGrid

77

Case 1: Summary



- We have collected total 53 submitted data with different grids and turbulence models (SA, SST, EARSM, and etc.).
- Turbulence model effects
 - The trend is similar for the alpha-sweep. The CL and Cm move up and down due to the turbulence model, but the slopes are same between the models.
 - CL is large in the order of SA, SST, EARSM. Cm is large in the order of EARSM, SST, SA. This is related with the shock location.
 - The Cp distributions agree with the experiment under the cruise condition. EARSM predicts the shock wave location well.
 - The idealized profile drag is higher than the experiment. The CL is lower than the experiment. (The shock locations are predicted well, but the lift is small.)
 - EARSM predicts the Cp well for the high angle of attack.
- Grid effects
 - There is no separation at the wing root for HexaGrid. This is same as the other coarse Cartesian grid.
 - The negative pressure is small for HexaGrid. The Cm is large for HexaGrid.
 - The nonlinear models (QCR, EARSM) have to be used for UPACS and MEGG3D grids to suppress the side-of-body separation.

78

Case 2: Follow-up discussion



- Model: NASA-CRM (arbitrary configurations)
- Grid: arbitrary grids
- Conditions: arbitrary conditions
- Angles: arbitrary angles
- Data to be submitted: None
- Recommendations:
 - Discussion on the difference observed in APC-I and APC-II
 - Aeroelasticity
 - Wall interference
 - Transition
 - No tails
 - High Re
 - Subsonic

79

Case 2: Follow-up discussion



- Wall interference (JAXA)
 - The wall interference is small
 - Correction is almost same as the experiment
- Flow conditions (Toyama Univ.)
 - The lift curve slope is affected by Mach number.
- ETW (KHI)
 - The lift curve slope agrees with ETW.

80

Case 3: Buffet



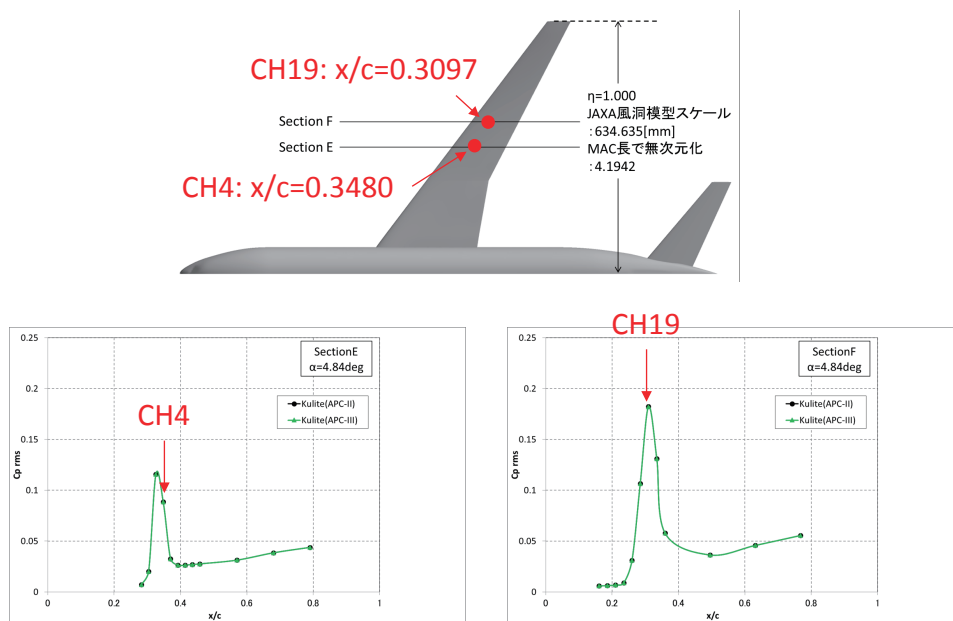
- Model: NASA-CRM($i_H=0\text{deg}$) with deformation
- Grid: Arbitrary grids
- Conditions: $M = 0.85$, $Re_c = 1.5 \times 10^6$, $T_{ref} = 282\text{K}$
- Angles: 4.87deg , 5.92deg
- Data to be submitted:
 - Aerodynamic coefficients(C_D, C_L, C_m)
 - Surface C_p distributions
 - Average, RMS
 - Frequency spectra
 - Flow field contours (Pressure, Mach number, eddy viscosity)

81

Case 3: Comparison locations



- Unsteady pressure is compared at Section E($\eta=0.50$) and Section F ($\eta=0.60$).
- Time histories and frequency spectra are compared at CH4 and CH19



82

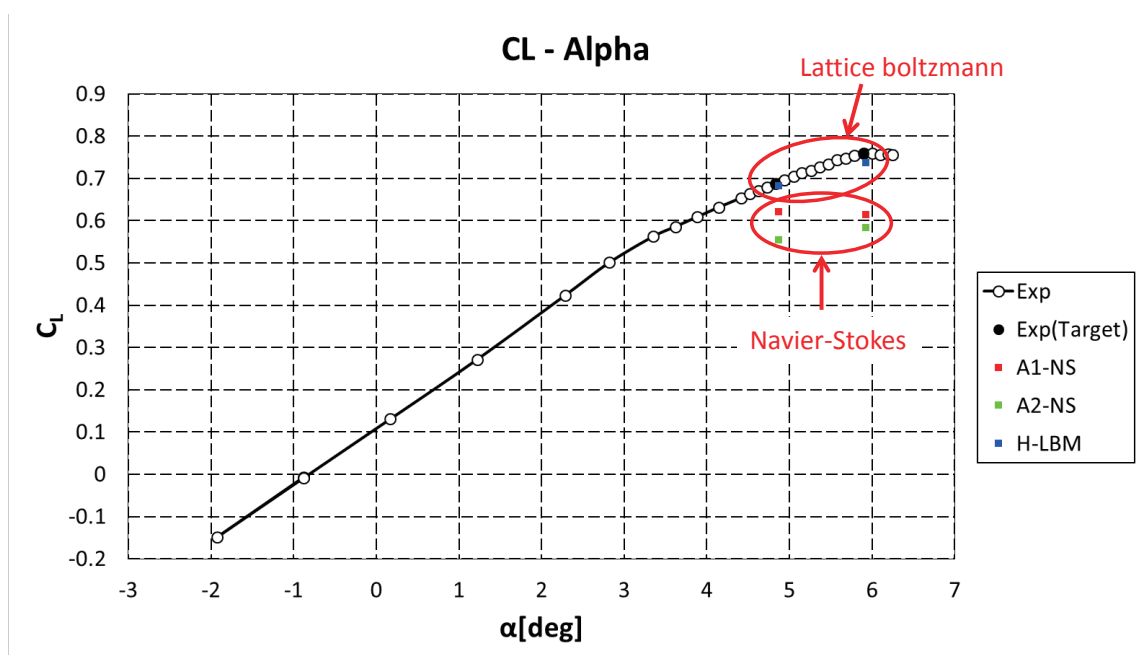


Case 3: List of data

- Aerodynamic coefficient(C_L)
- Results of 4.87deg
 - C_p average and RMS(Section E, F)
 - C_p time histories and PSD (CH4, CH19)
 - Wing surface C_p (Average/RMS), Streamline(Average)
 - Cross sectional C_p (Average/RMS)
 - Cross sectional Mach number(Average/RMS)
 - Cross sectional eddy viscosity(Average)
- Results of 5.92deg
 - C_p average and RMS(Section E, F)
 - C_p time histories and PSD (CH4, CH19)
 - Wing surface C_p (Average/RMS), Streamline(Average)
 - Cross sectional C_p (Average/RMS)
 - Cross sectional Mach number(Average/RMS)
 - Cross sectional eddy viscosity(Average)

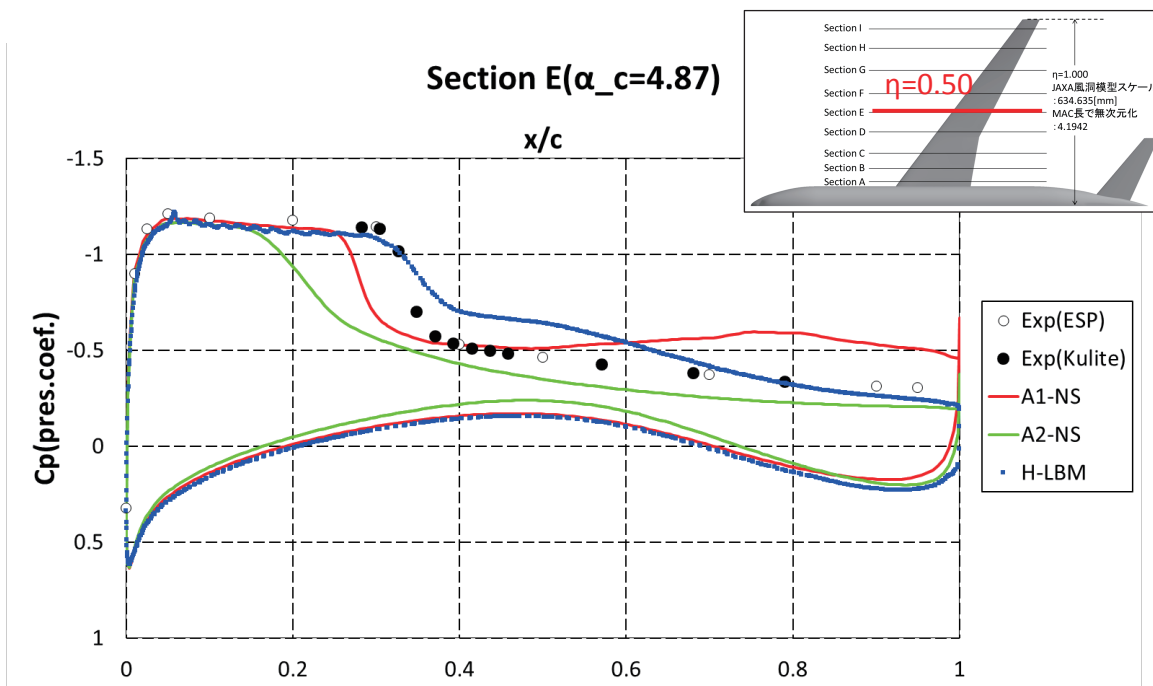
83

Case 3: Aerodynamic coefficient



84

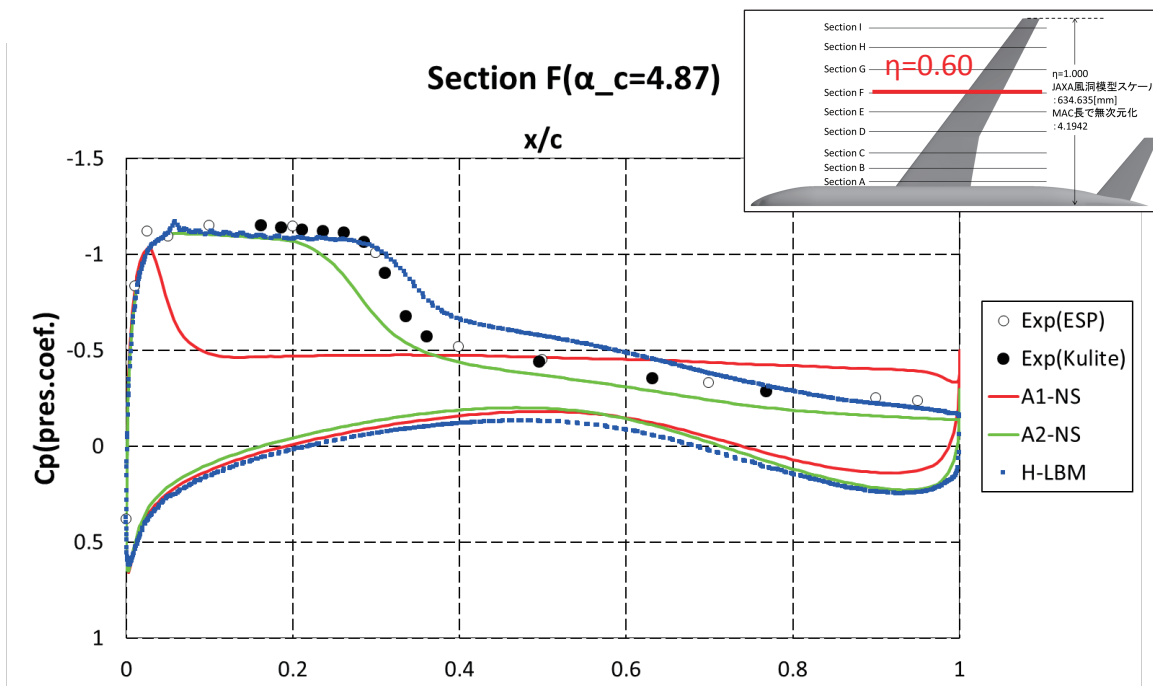
Case 3 : Cp average (4.87deg)



Variation of the shock wave location is large

85

Case 3 : Cp average (4.87deg)

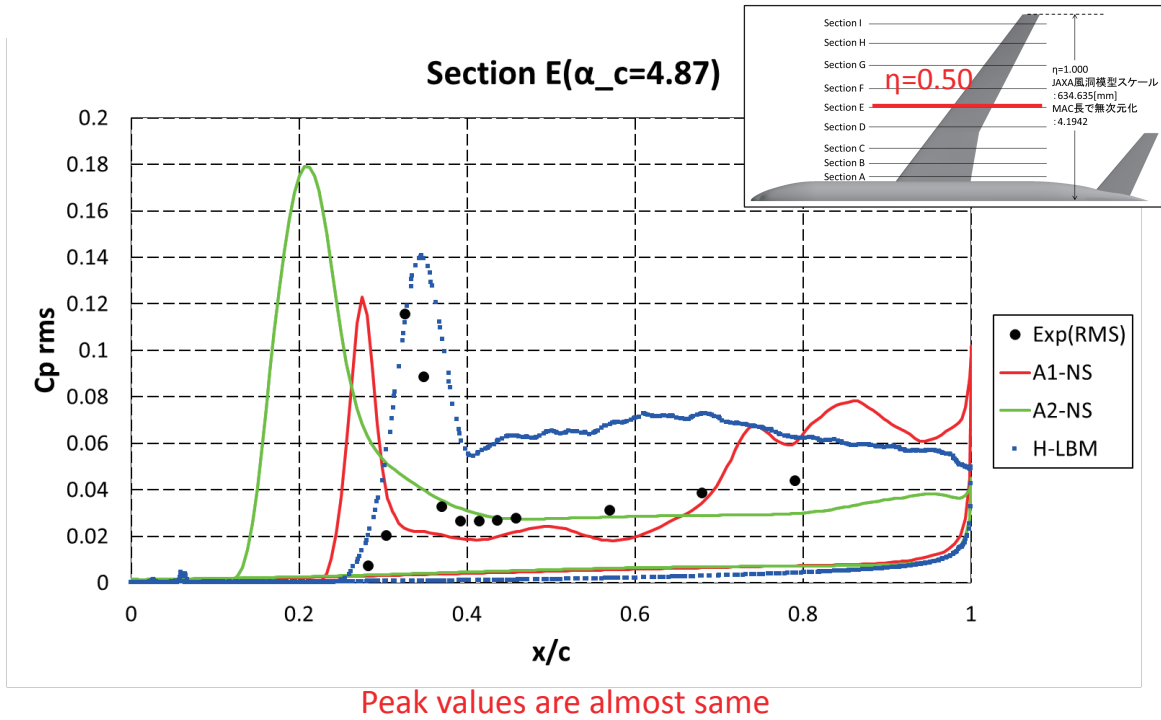


Variation of the shock wave location is large

86

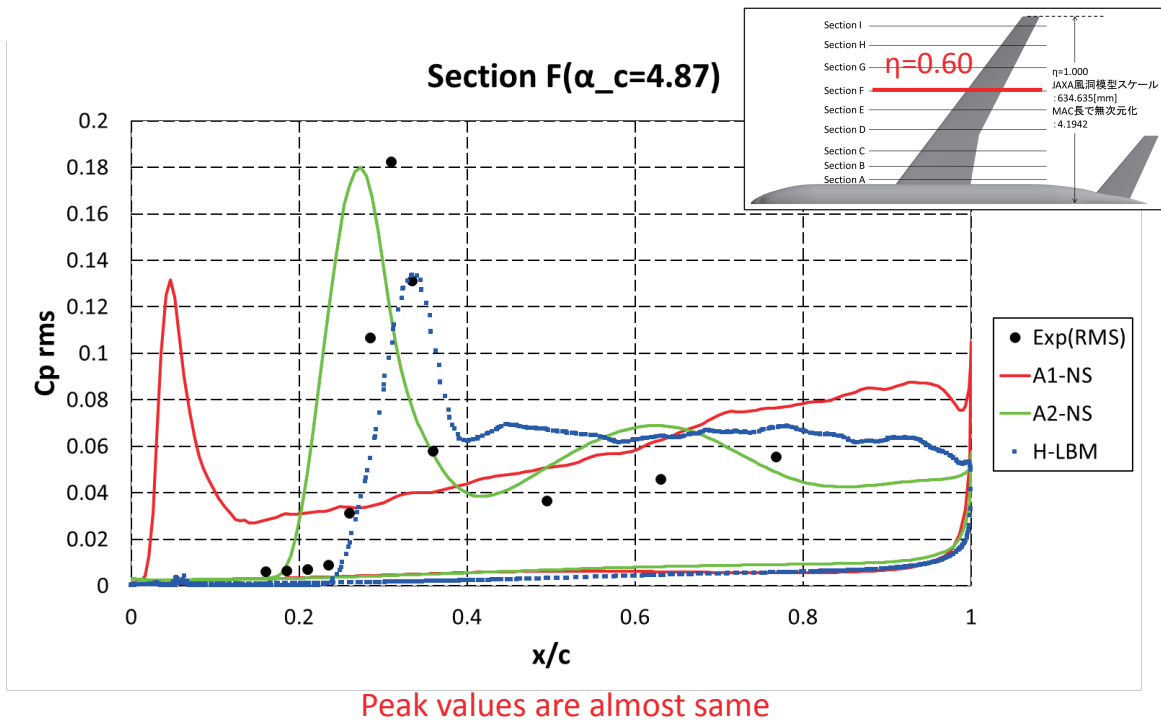


Case 3 : Cp RMS (4.87deg)



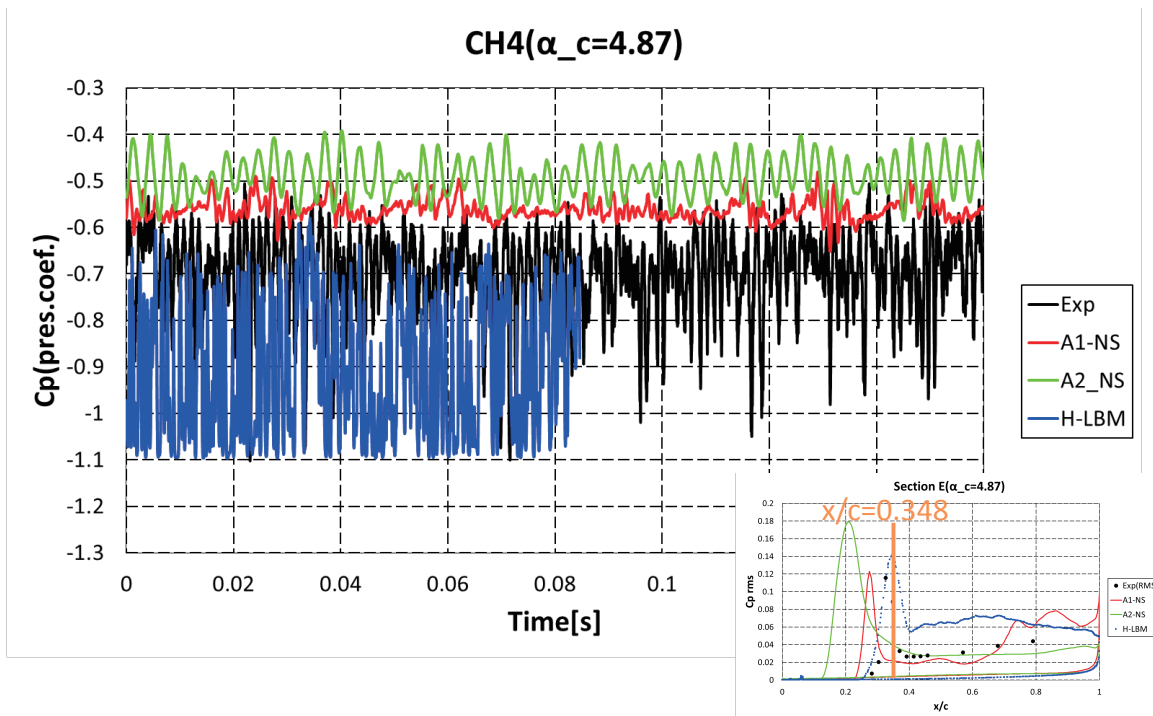
87

Case 3 : Cp RMS (4.87deg)



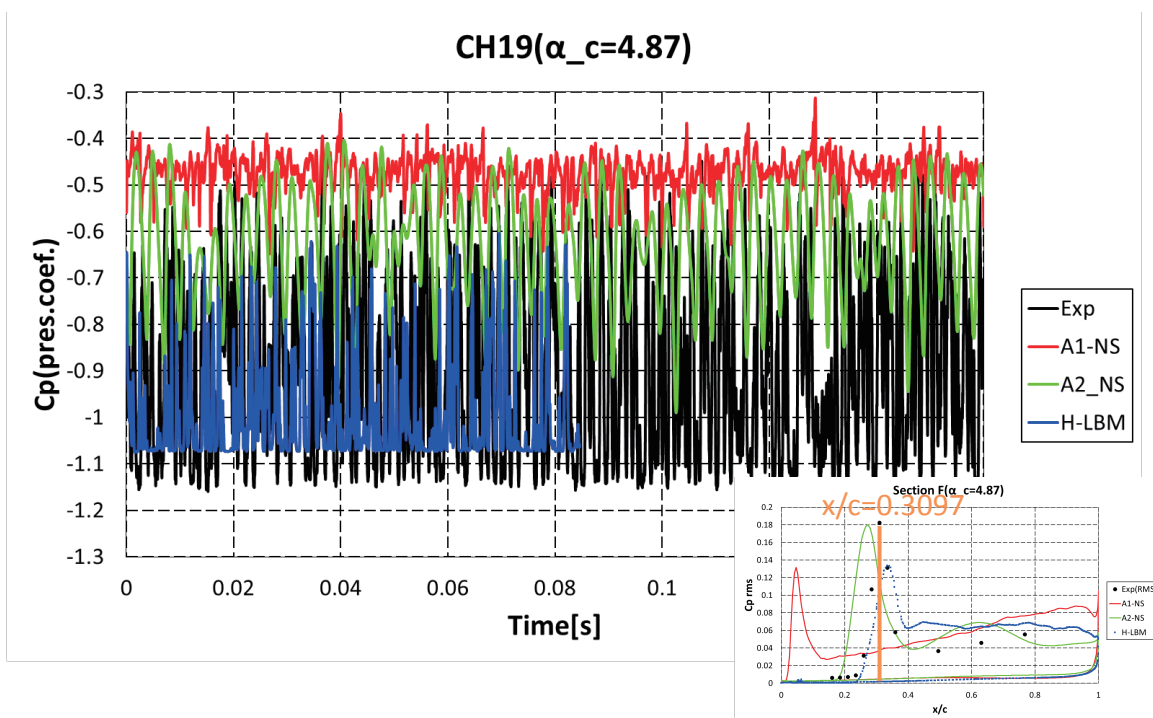
88

Case 3 : Cp time history (4.87deg)



89

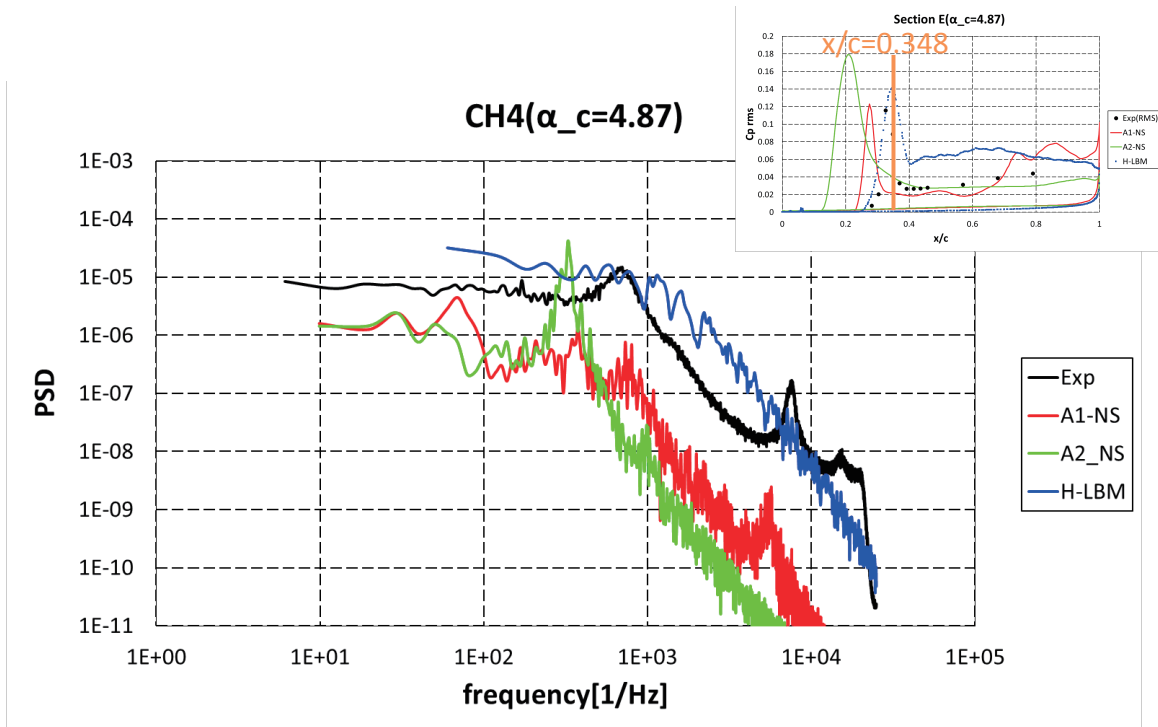
Case 3 : Cp time history (4.87deg)



90

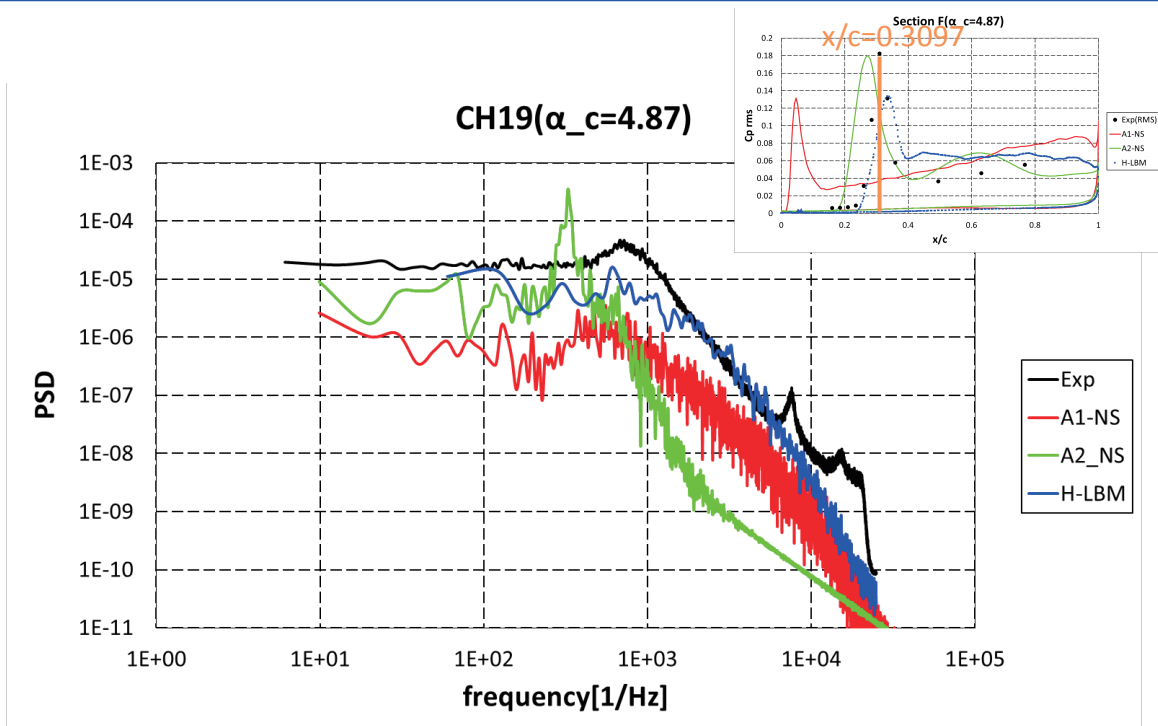


Case 3 : Cp PSD (4.87deg)



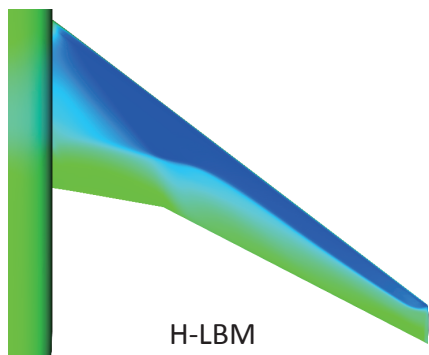
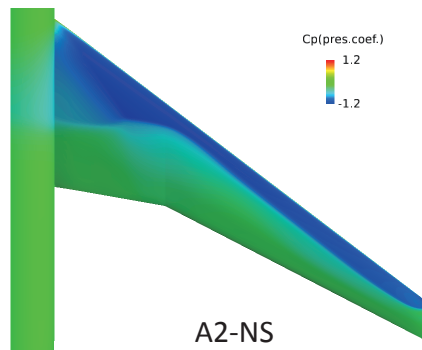
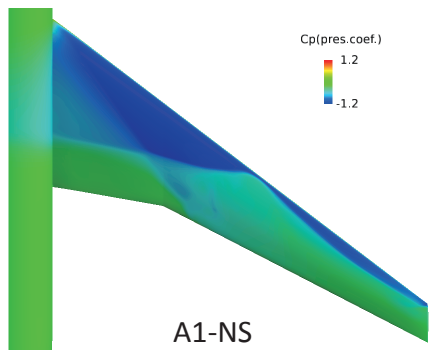
91

Case 3 : Cp PSD (4.87deg)



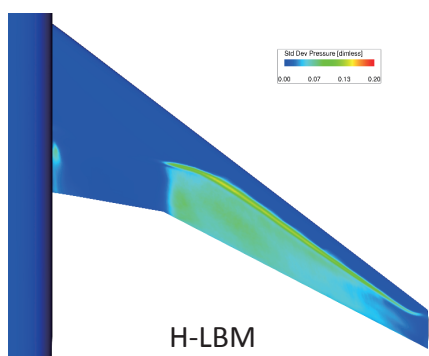
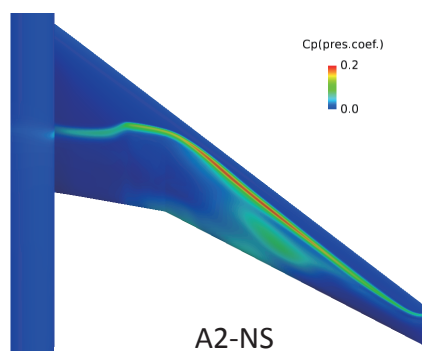
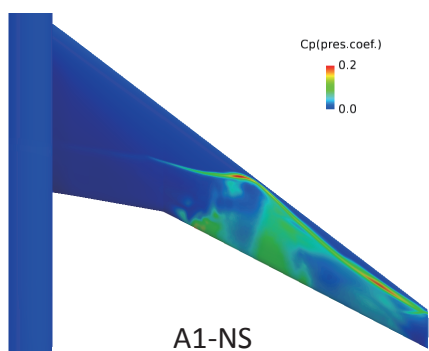
92

Case 3: Cp average ($\alpha=4.87\text{deg}$)



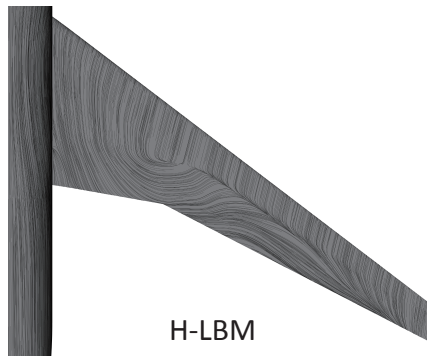
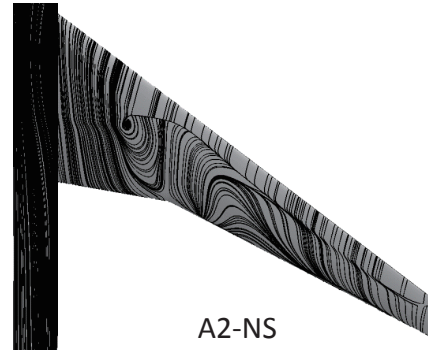
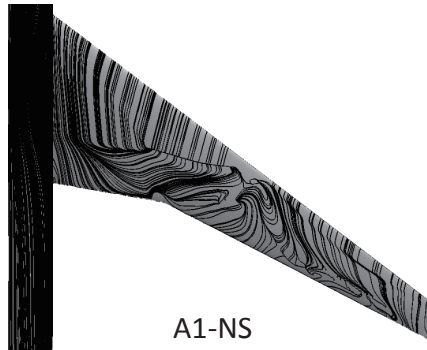
93

Case 3: Cp RMS ($\alpha=4.87\text{deg}$)



94

Case 3: Streamline ($\alpha=4.87\text{deg}$)

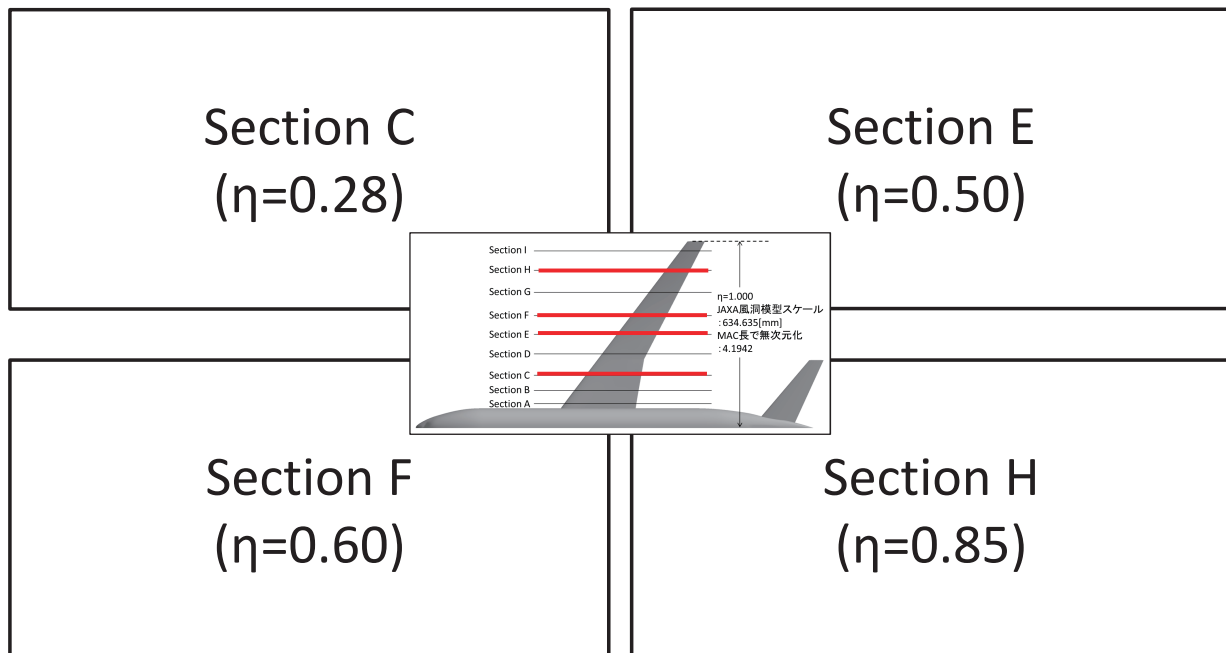


95

Case 3: Cross sectional contours



We show the cross-sectional contours as follows,

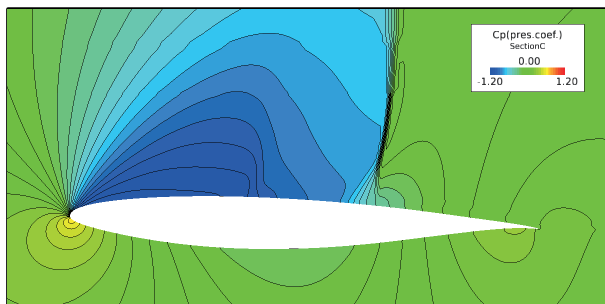


96

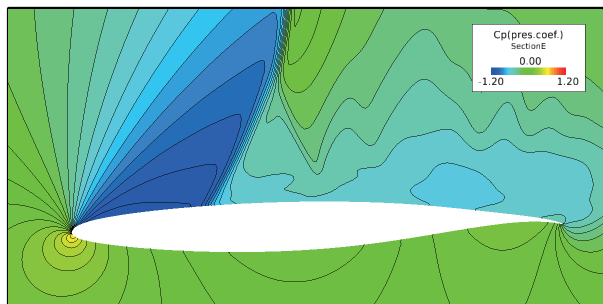
Case 3: Cp average ($\alpha=4.87\text{deg}$)



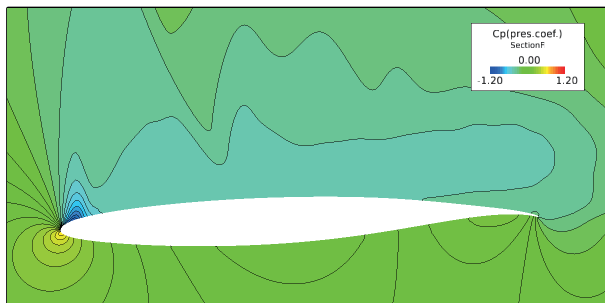
ID:A1



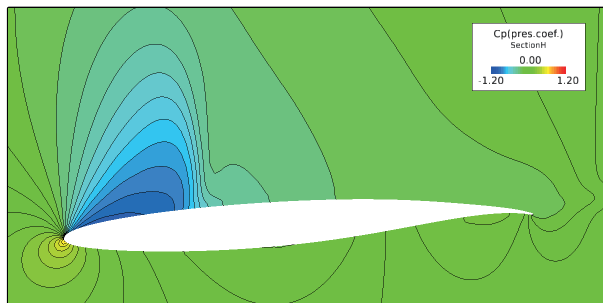
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



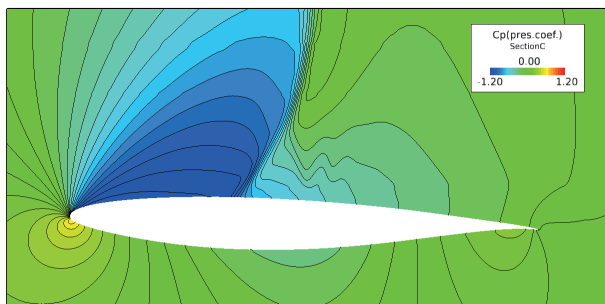
Section H ($\eta=0.85$)

97

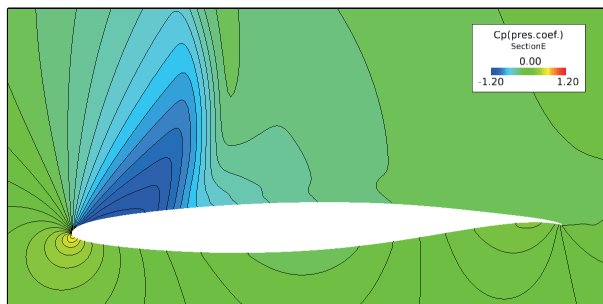
Case 3: Cp average ($\alpha=4.87\text{deg}$)



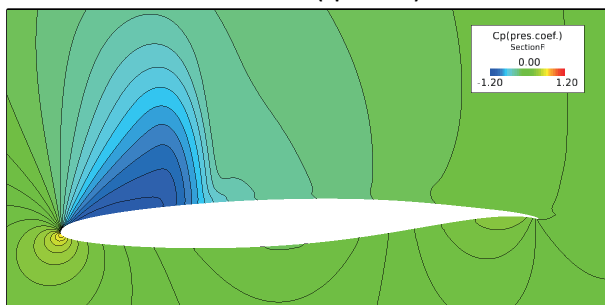
ID:A2



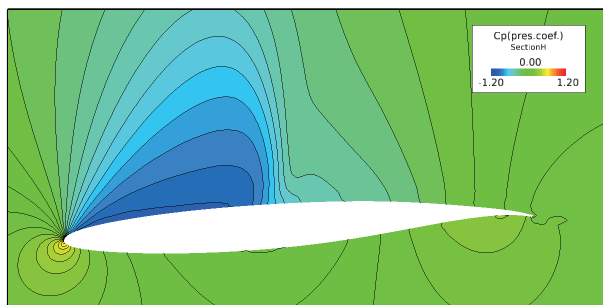
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



Section H ($\eta=0.85$)

98

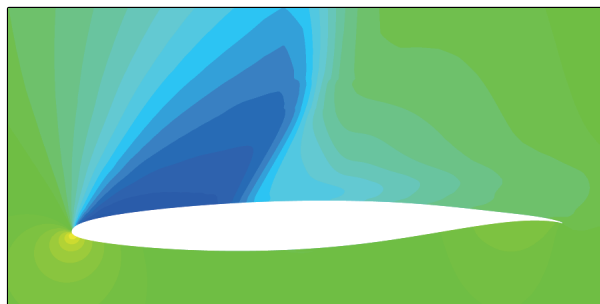
Case 3: Cp average ($\alpha=4.87\text{deg}$)



ID:H



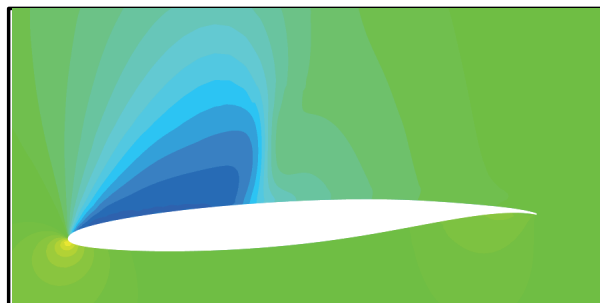
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



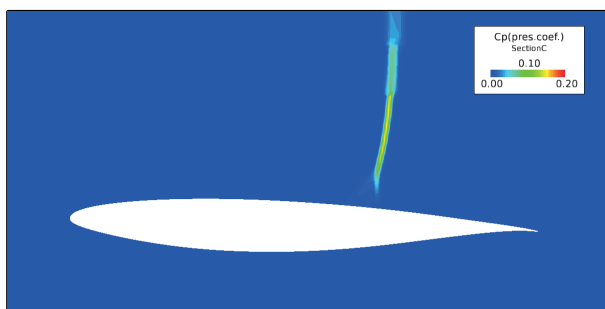
Section H ($\eta=0.85$)

99

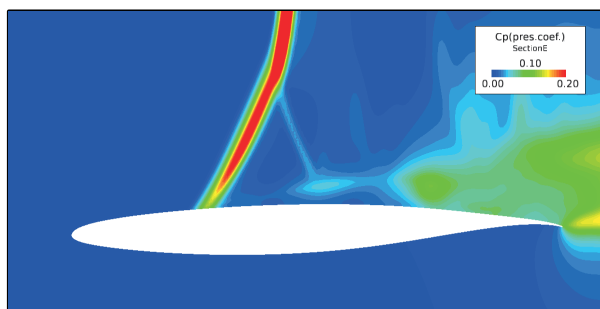
Case 3: Cp RMS ($\alpha=4.87\text{deg}$)



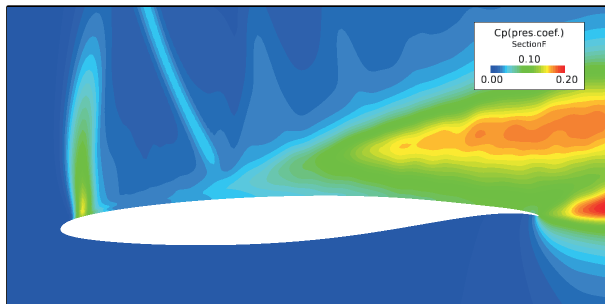
ID:A1



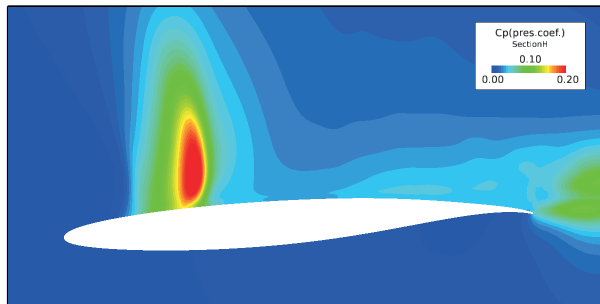
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



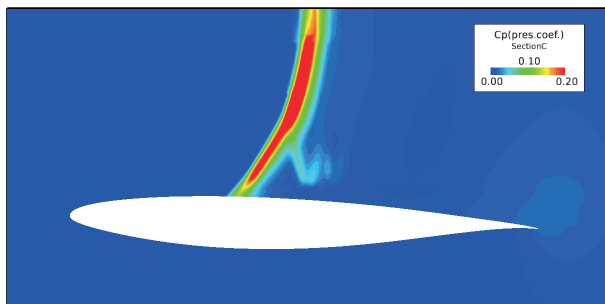
Section H ($\eta=0.85$)

100

Case 3: Cp RMS ($\alpha=4.87\text{deg}$)



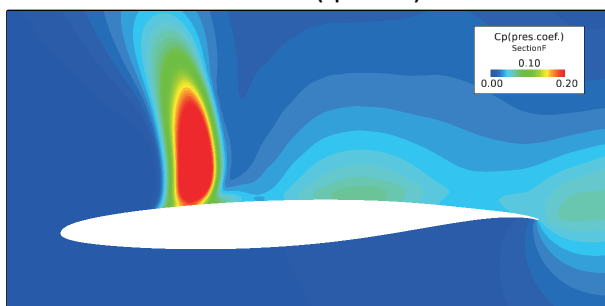
ID:A2



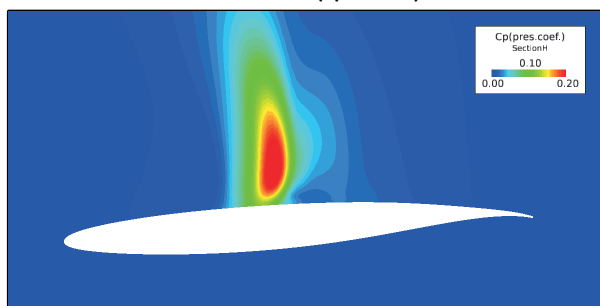
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



Section H ($\eta=0.85$)

101

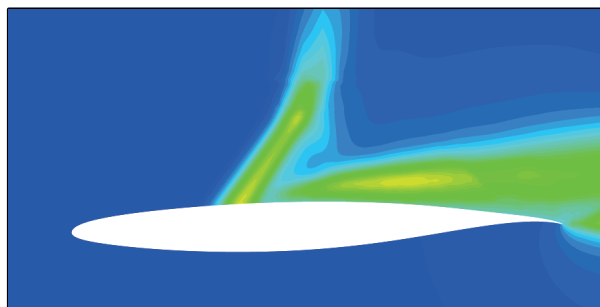
Case 3: Cp RMS ($\alpha=4.87\text{deg}$)



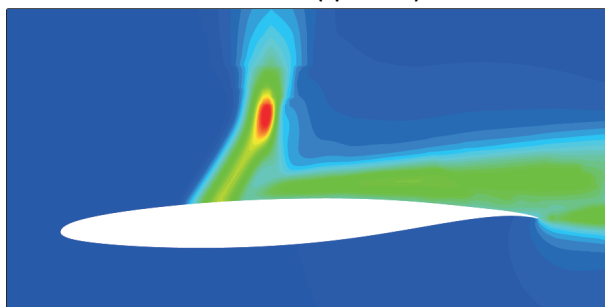
ID:H



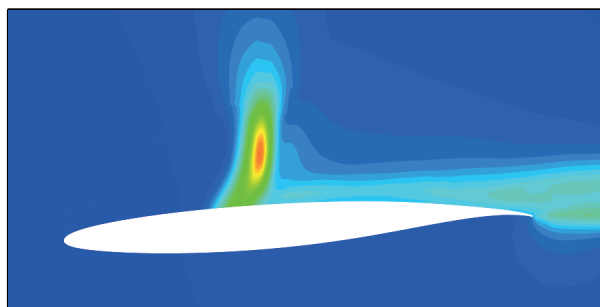
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



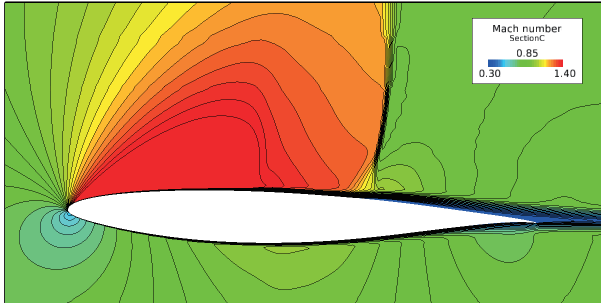
Section H ($\eta=0.85$)

102

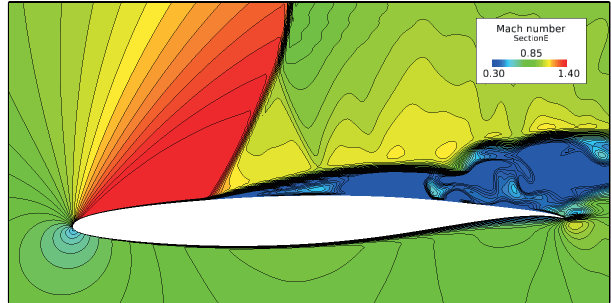
Case 3: Mach number ($\alpha=4.87\text{deg}$)



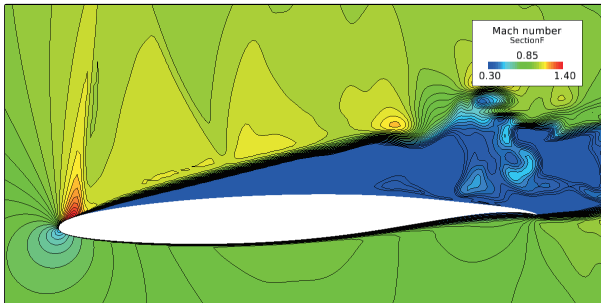
ID:A1



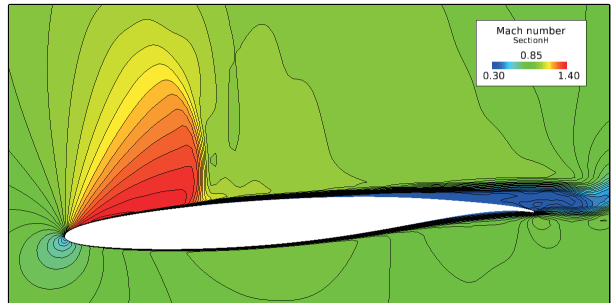
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



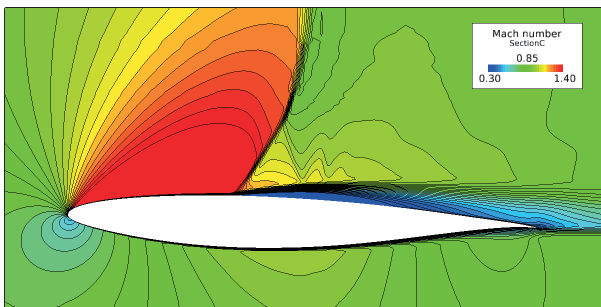
Section H ($\eta=0.85$)

103

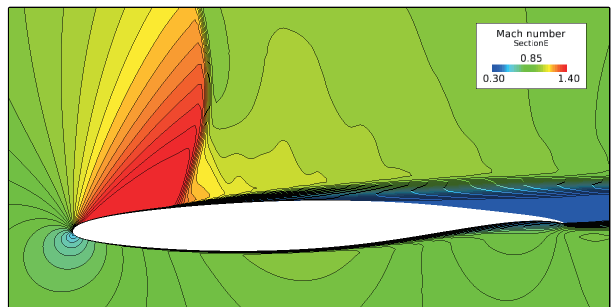
Case 3: Mach number ($\alpha=4.87\text{deg}$)



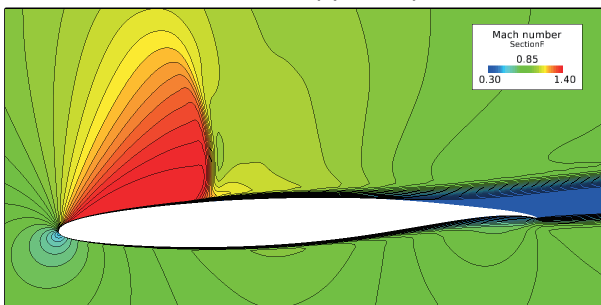
ID:A2



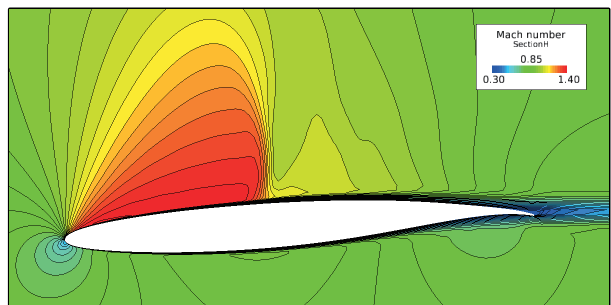
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



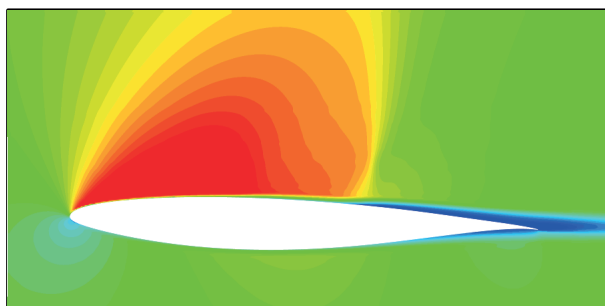
Section H ($\eta=0.85$)

104

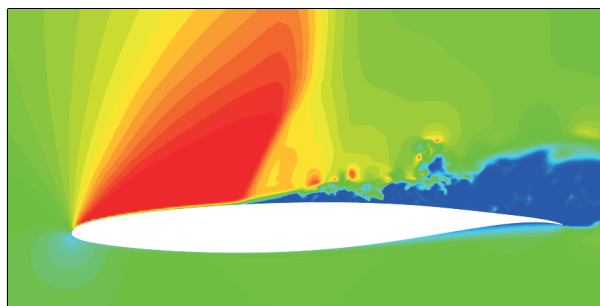
Case 3: Mach number ($\alpha=4.87\text{deg}$)



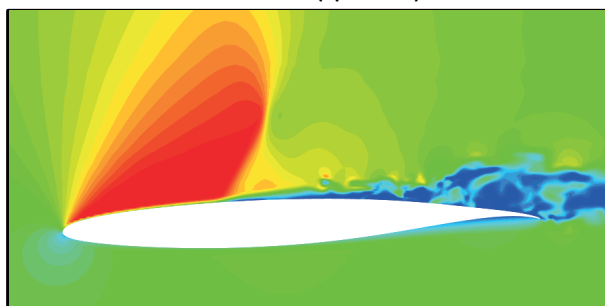
ID:H



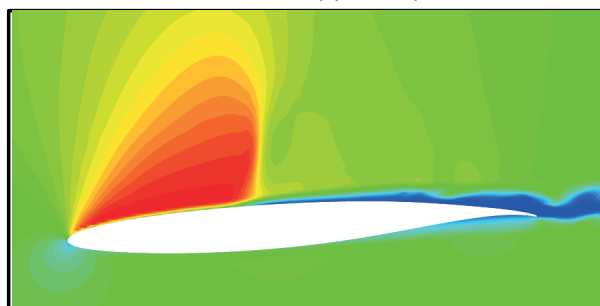
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



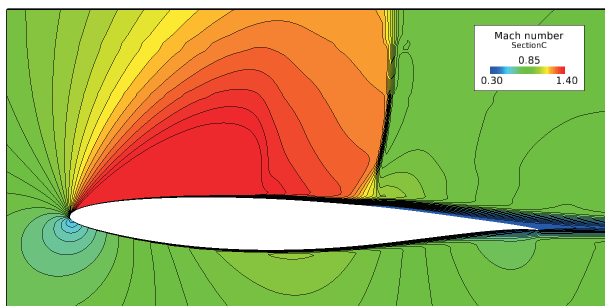
Section H ($\eta=0.85$)

105

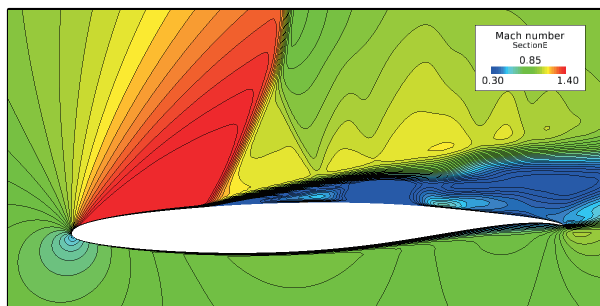
Case 3: Mach number average ($\alpha=4.87\text{deg}$)



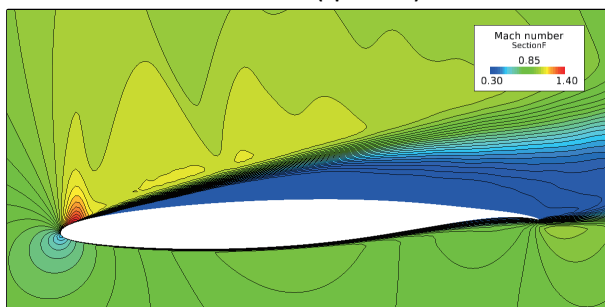
ID:A1



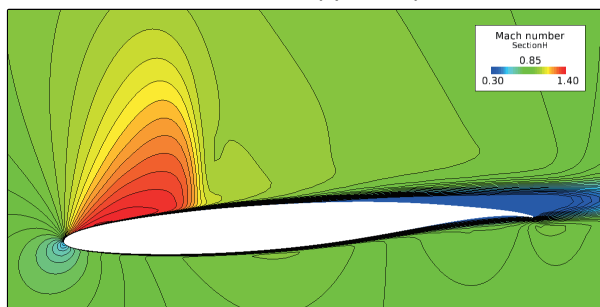
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



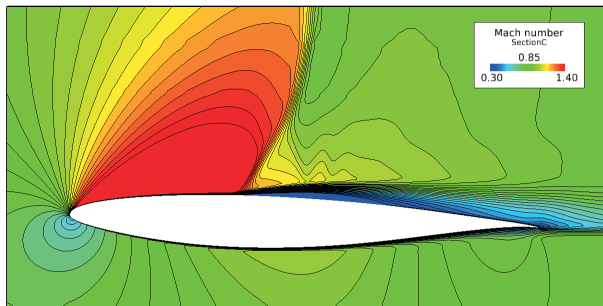
Section H ($\eta=0.85$)

106

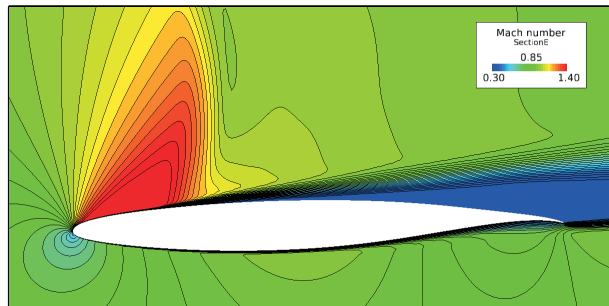
Case 3: Mach number average ($\alpha=4.87\text{deg}$)



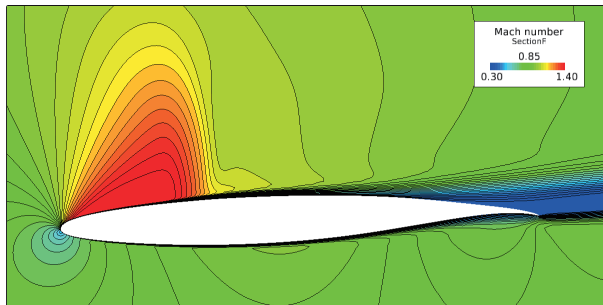
ID:A2



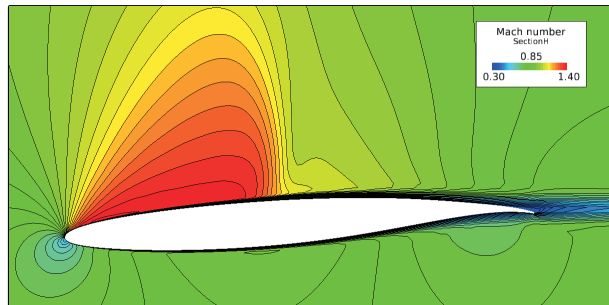
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



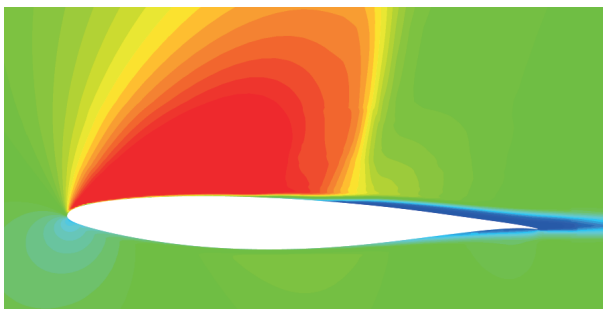
Section H ($\eta=0.85$)

107

Case 3: Mach number average ($\alpha=4.87\text{deg}$)



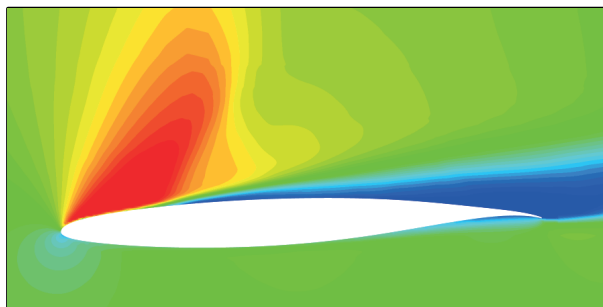
ID:H



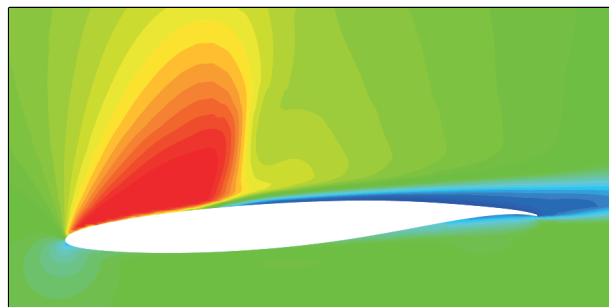
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



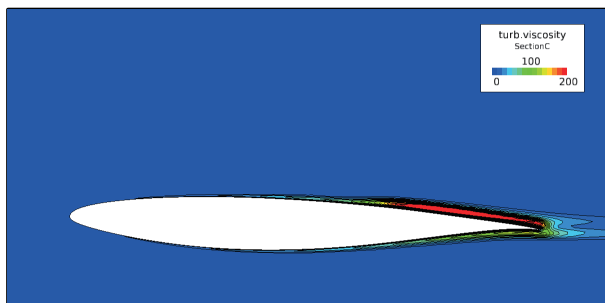
Section H ($\eta=0.85$)

108

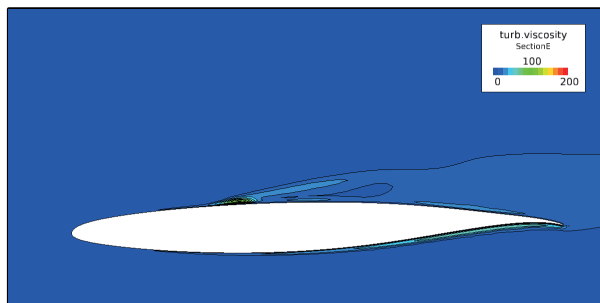
Case 3: Eddy viscosity average ($\alpha=4.87\text{deg}$)



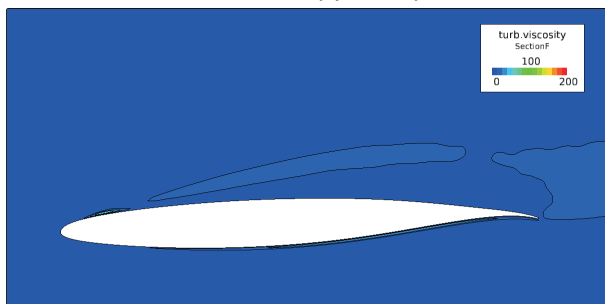
ID:A1



Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



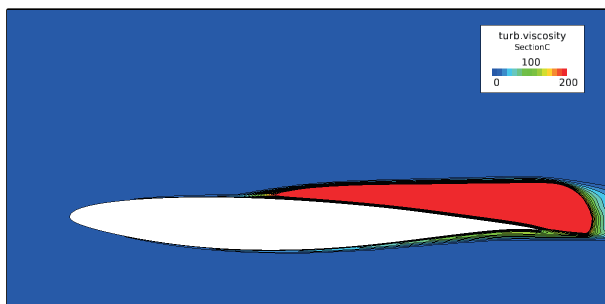
Section H ($\eta=0.85$)

109

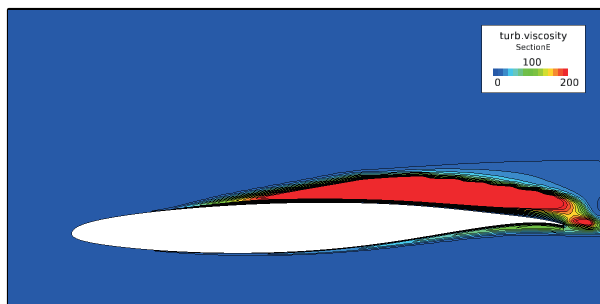
Case 3: Eddy viscosity average ($\alpha=4.87\text{deg}$)



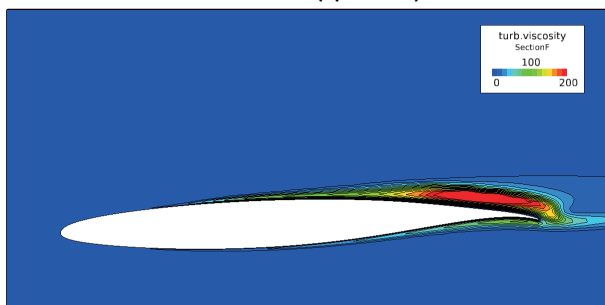
ID:A2



Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



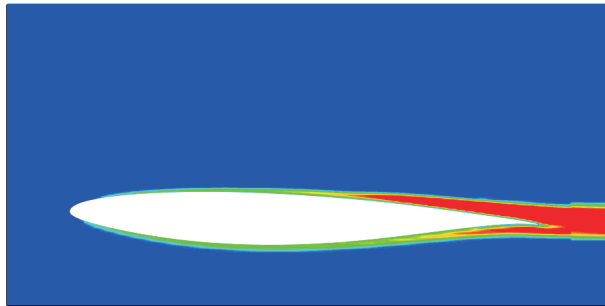
Section H ($\eta=0.85$)

110

Case 3: Eddy viscosity average ($\alpha=4.87\text{deg}$)



ID:H



Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



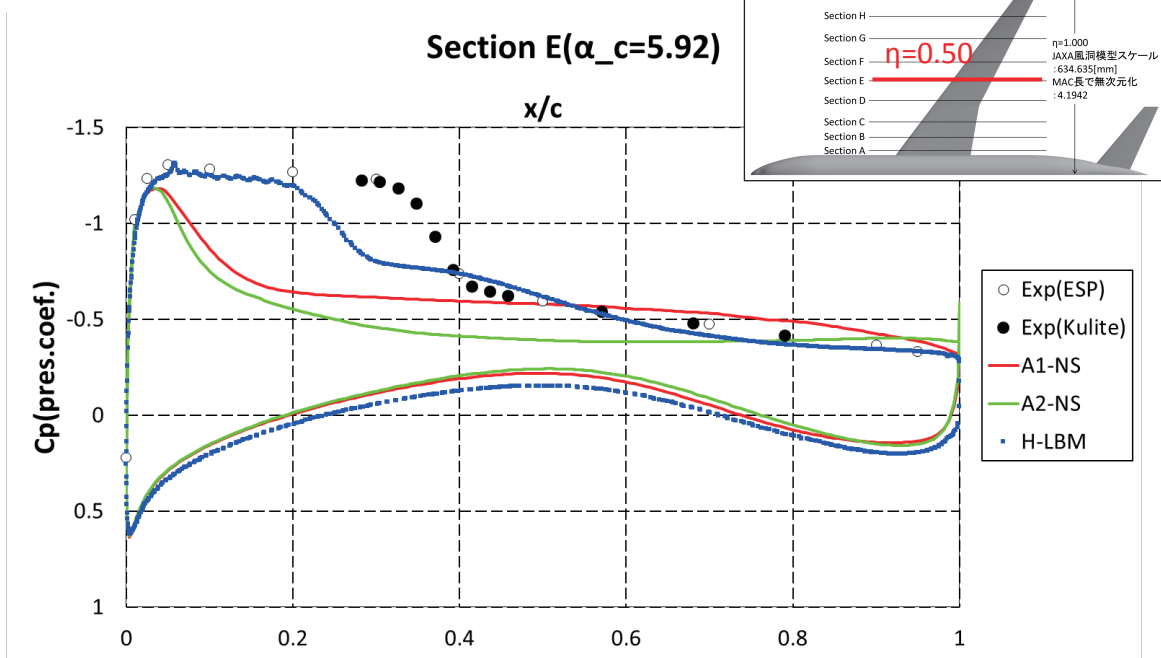
Section H ($\eta=0.85$)

111

Case 3 : Cp average (5.92deg)



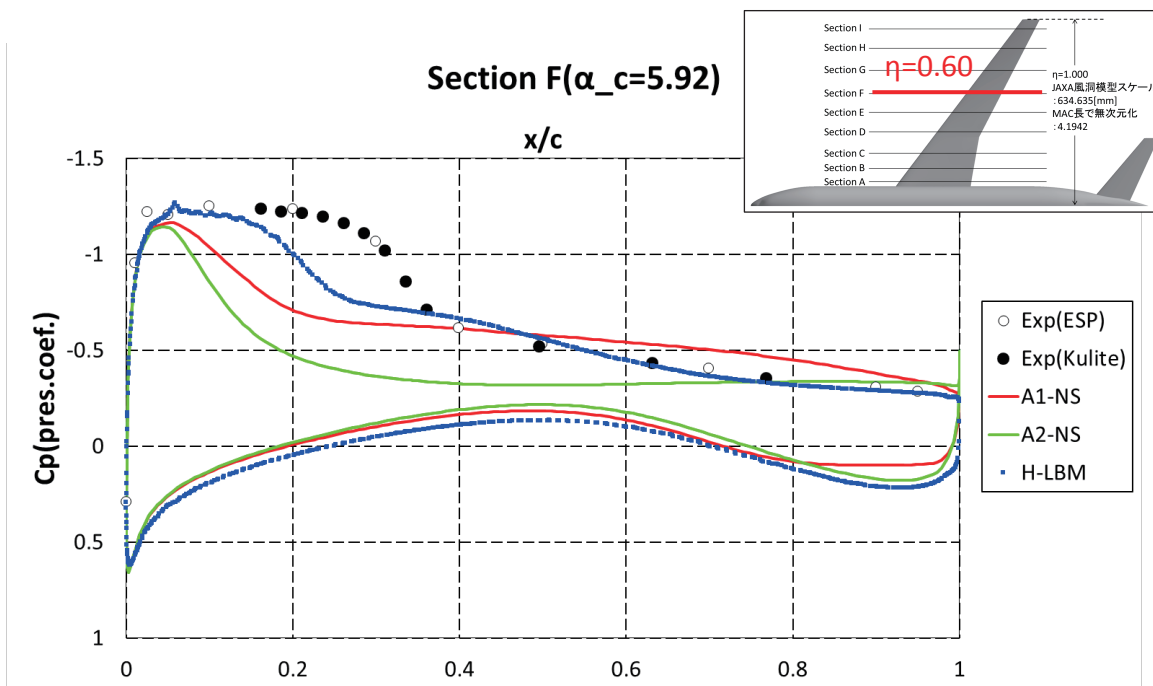
非定常解析でパフエットが予測できるか



The shock wave moves forward for 5.92deg.

112

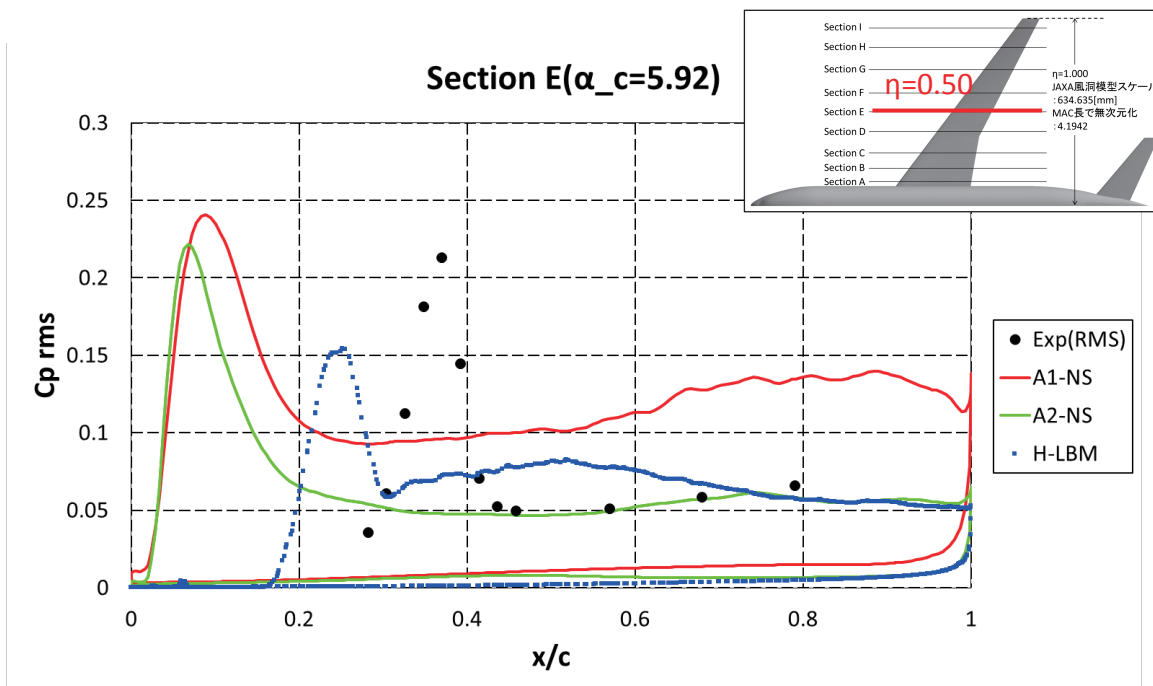
Case 3 : Cp average (5.92deg)



The shock wave moves forward for 5.92deg.

113

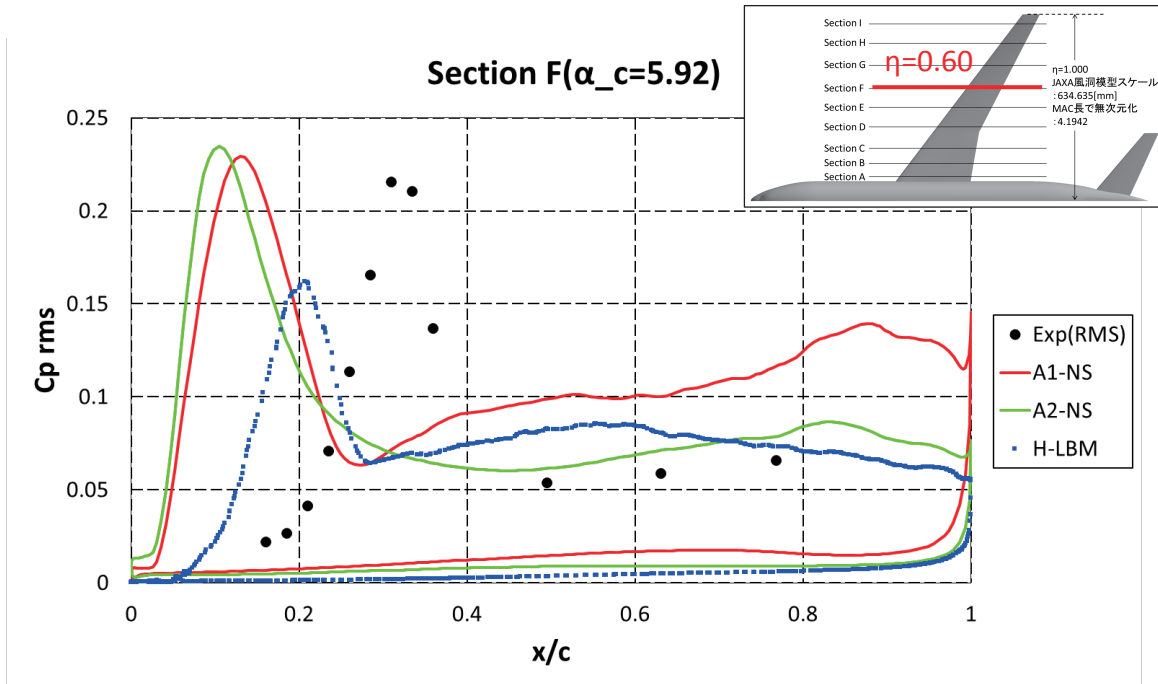
Case 3 : Cp RMS (5.92deg)



114

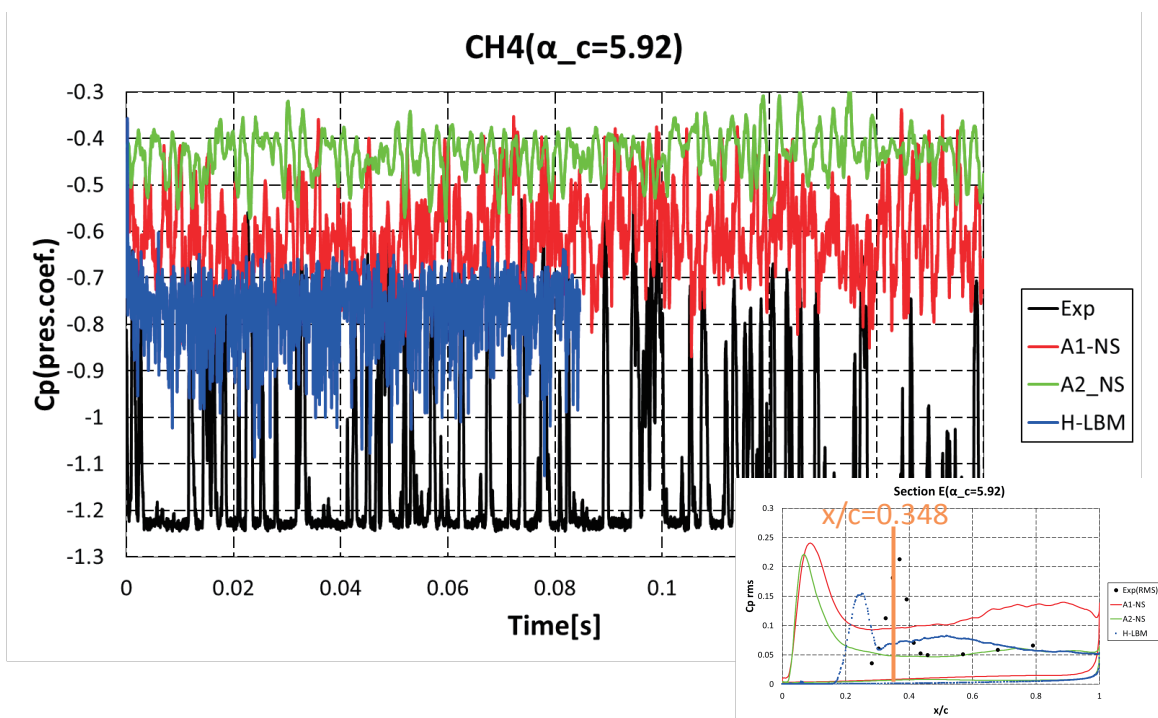


Case 3 : Cp RMS (5.92deg)



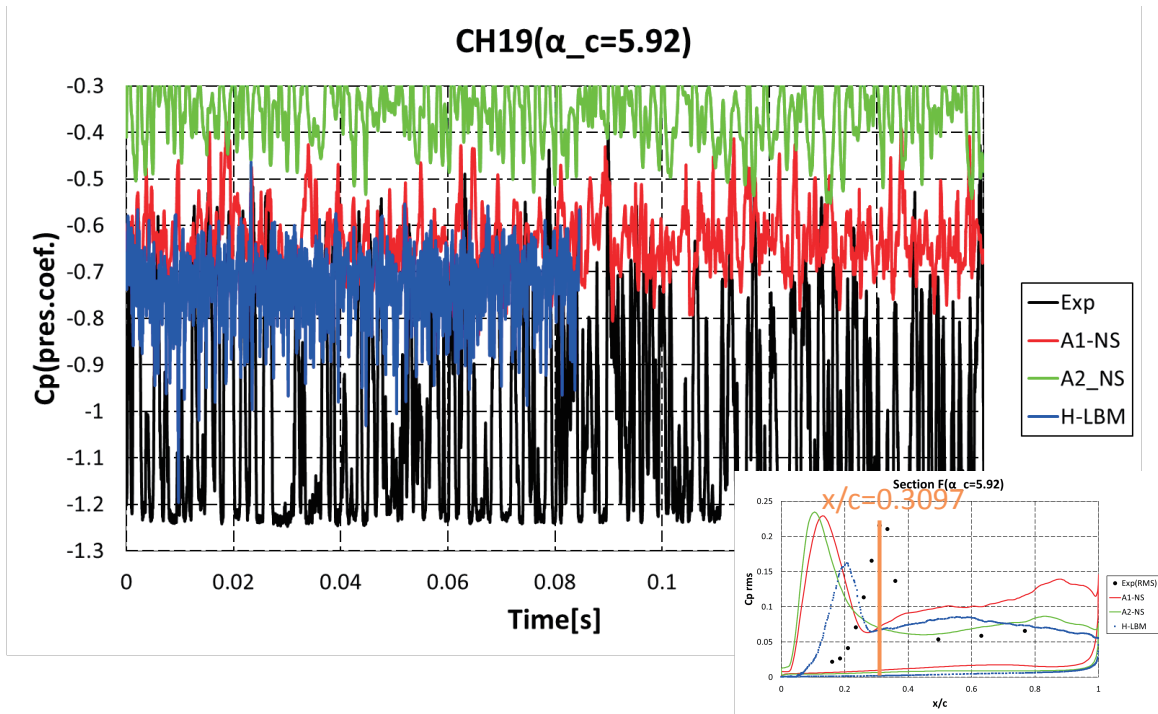
115

Case 3 : Cp time history (5.92deg)



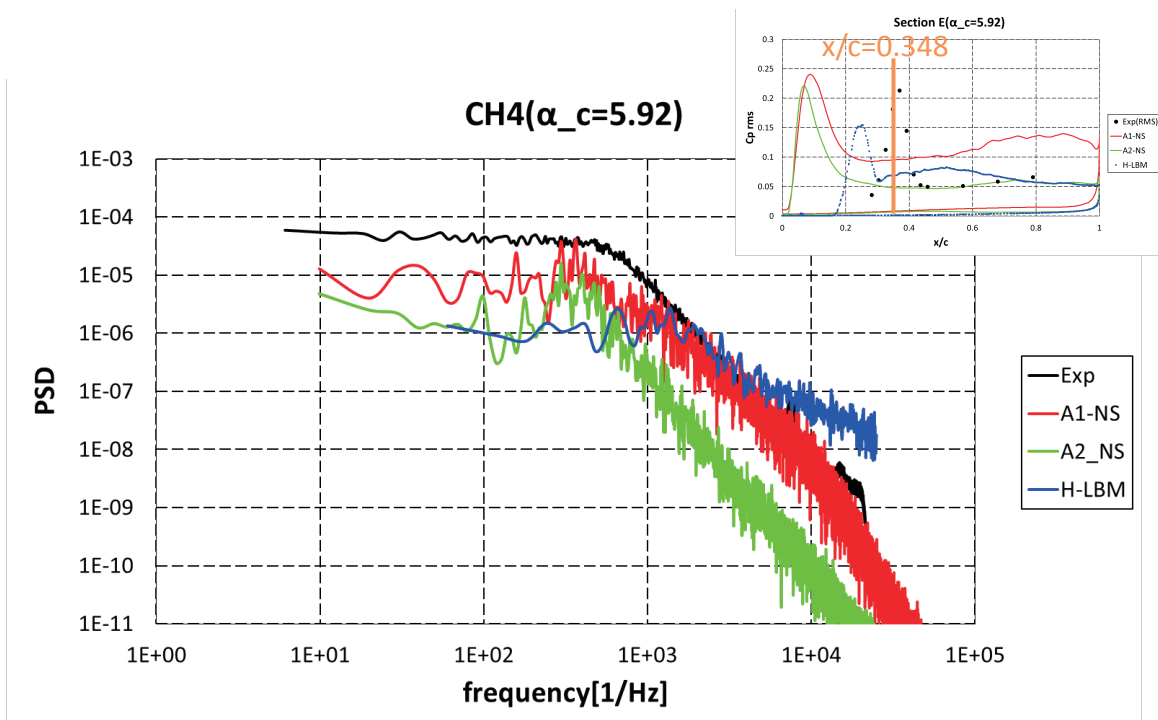
116

Case 3 : Cp time history (5.92deg)



117

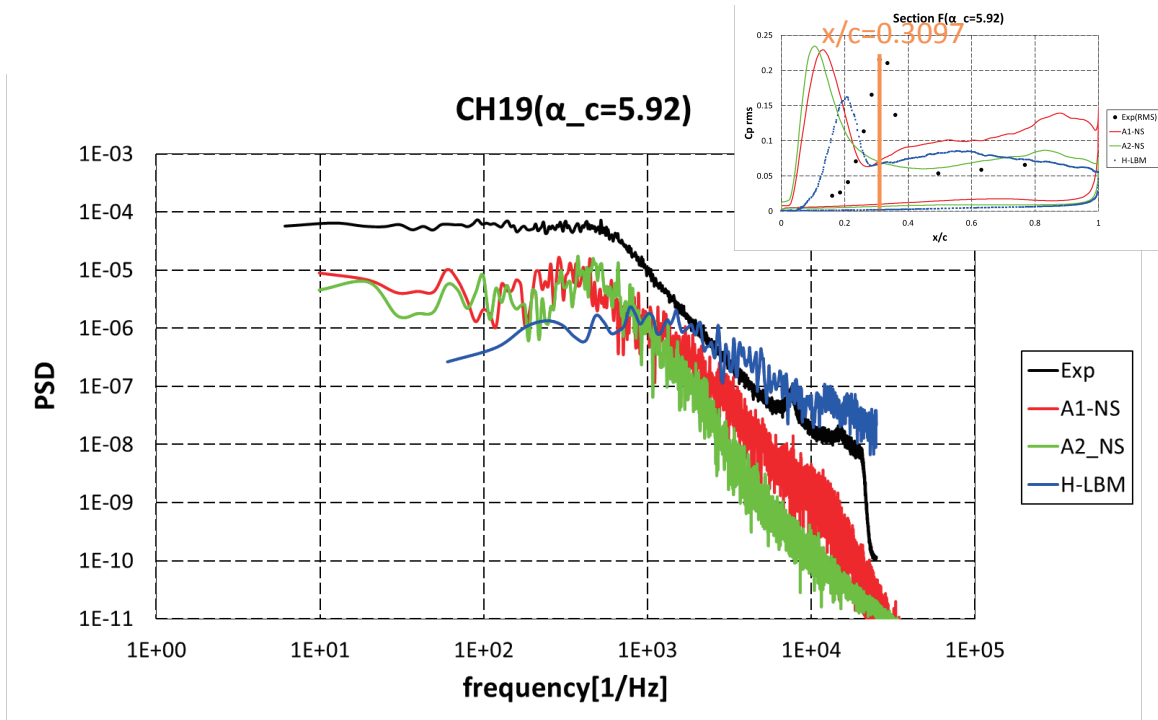
Case 3 : Cp PSD (5.92deg)



118

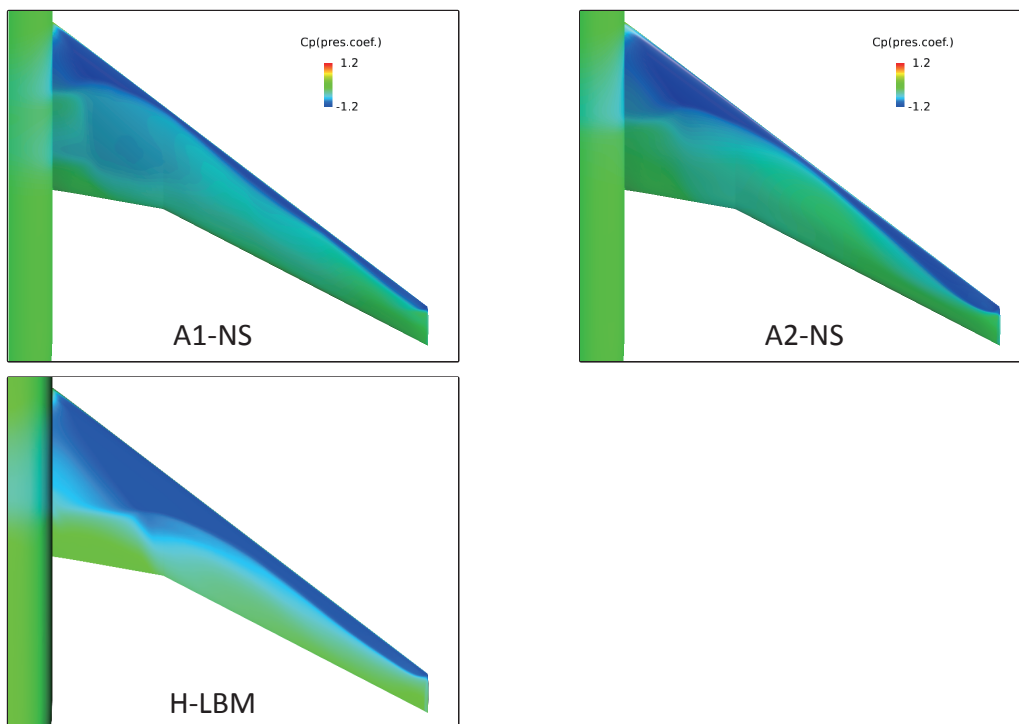


Case 3 : Cp PSD (5.92deg)



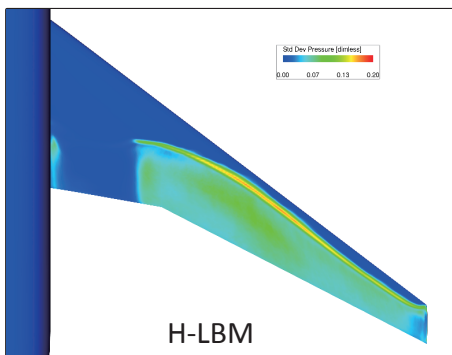
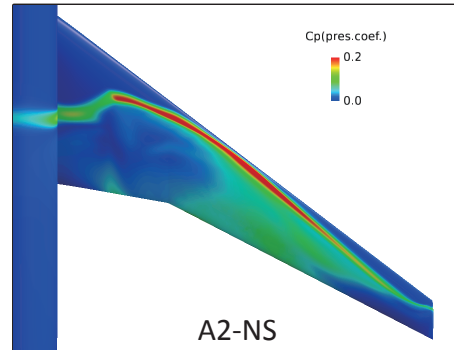
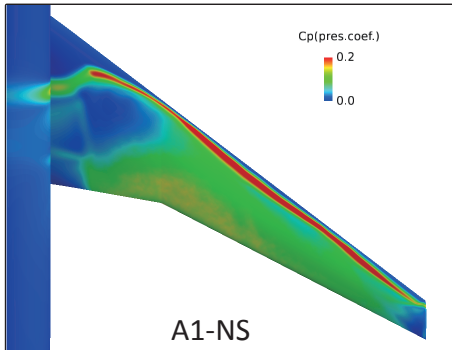
119

Case 3 : Cp average (α=5.92deg)



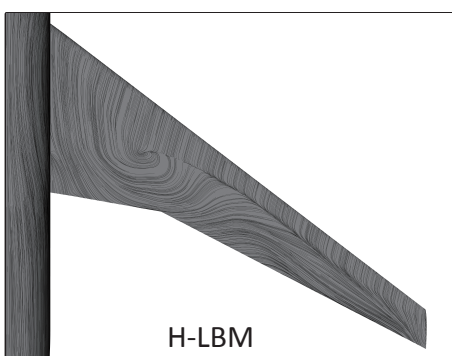
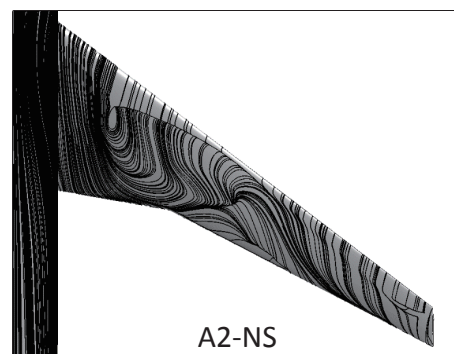
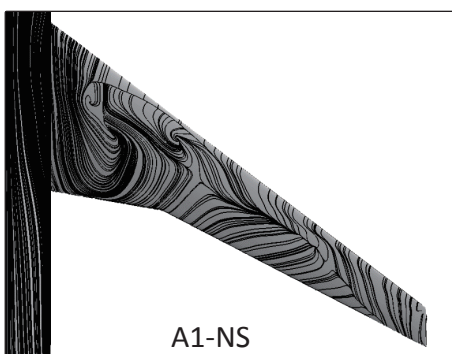
120

Case 3 : Cp RMS ($\alpha=5.92\text{deg}$)



121

Case 3 : Streamline ($\alpha=5.92\text{deg}$)

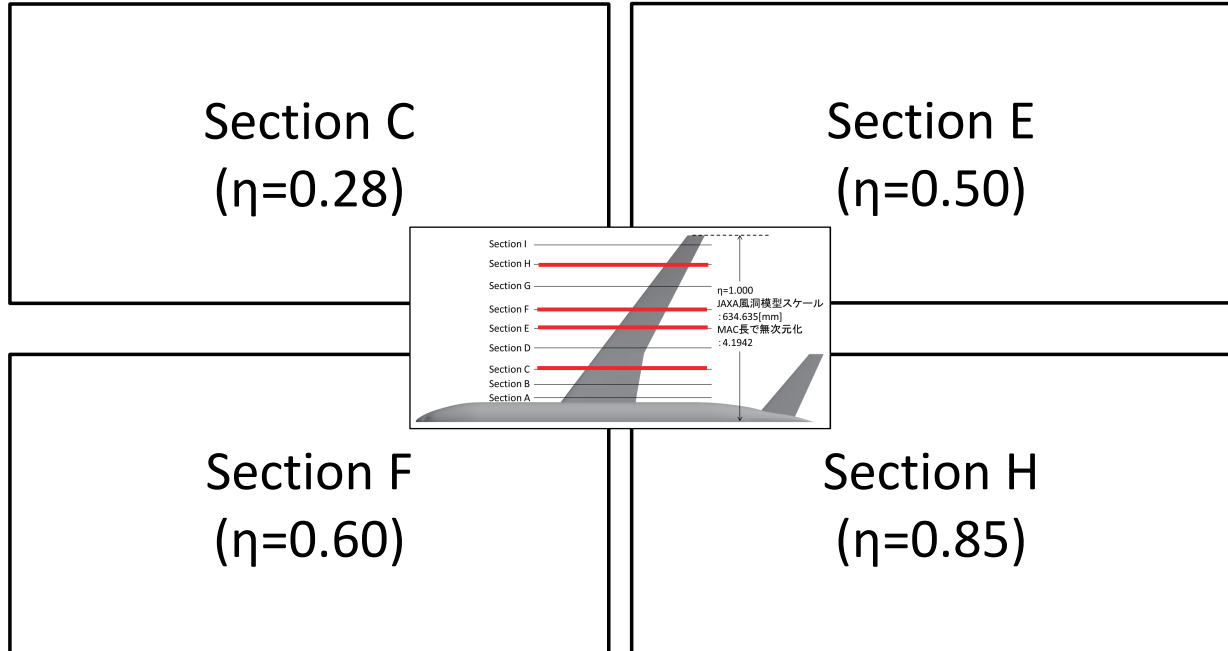


122

Case 3: Cross sectional contours



We show the cross-sectional contours as follows,

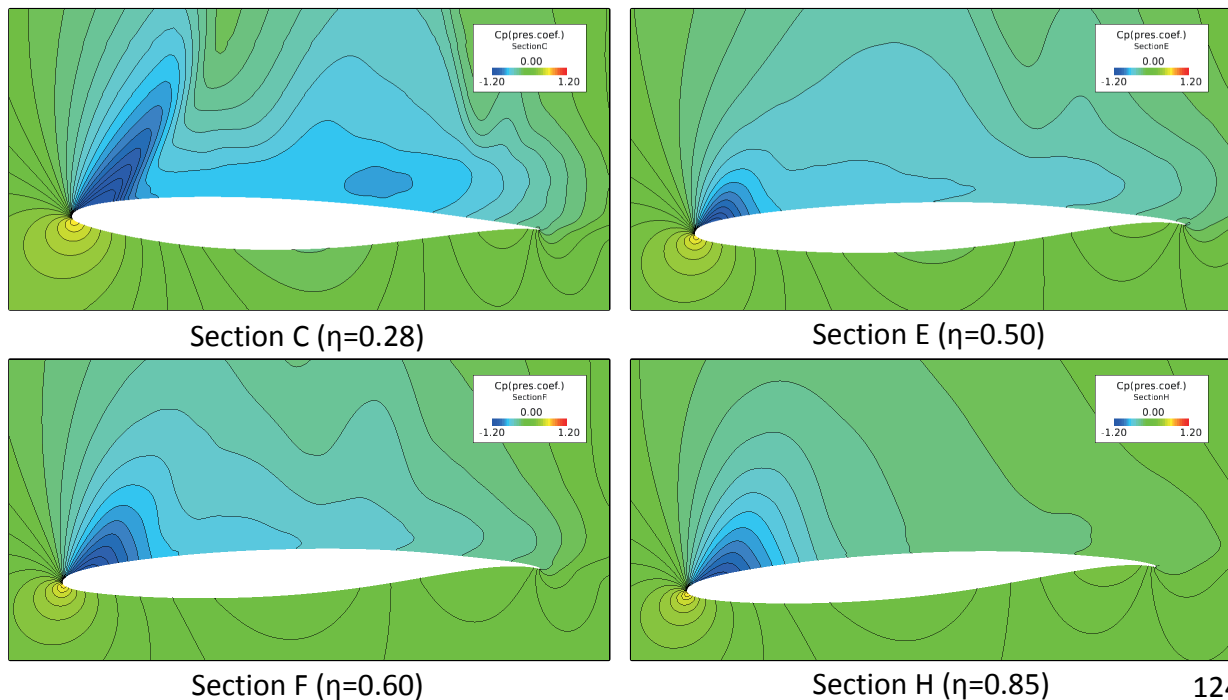


123

Case 3: Cp average ($\alpha=5.92\text{deg}$)



ID:A1

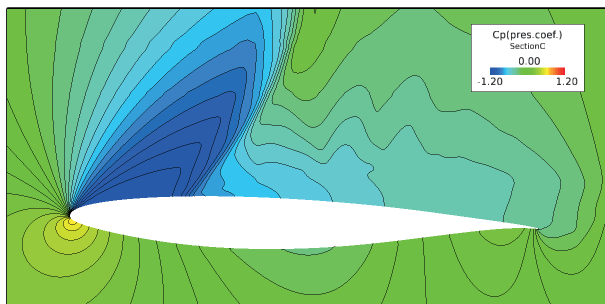


124

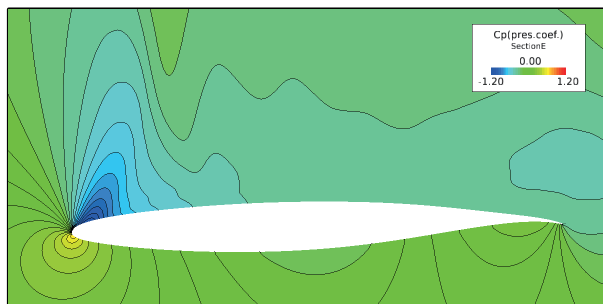
Case 3: Cp average ($\alpha=5.92\text{deg}$)



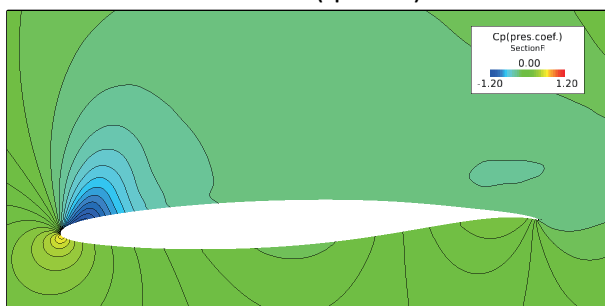
ID:A2



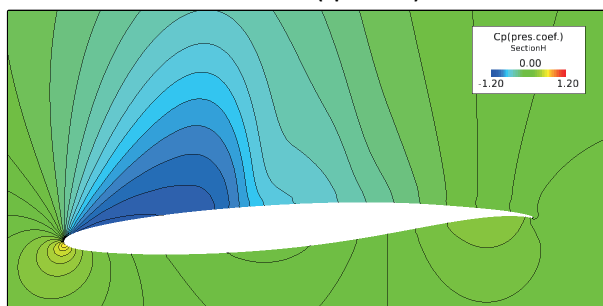
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



Section H ($\eta=0.85$)

125

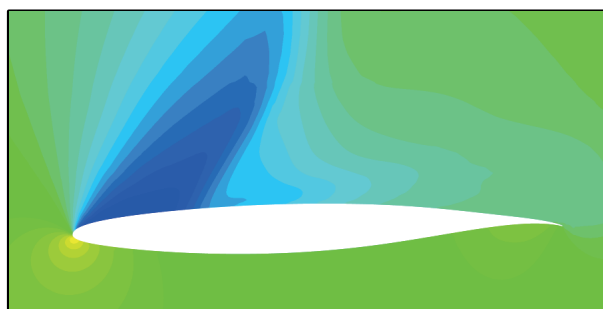
Case 3: Cp average ($\alpha=5.92\text{deg}$)



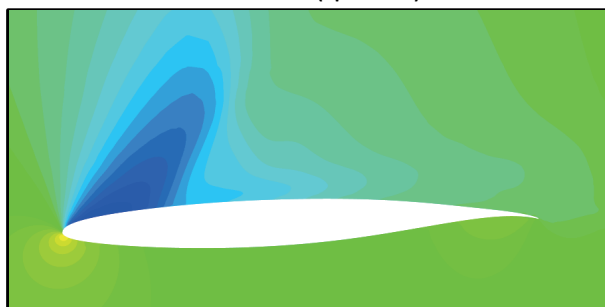
ID:H



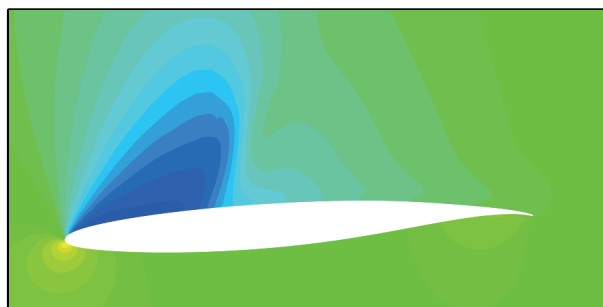
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



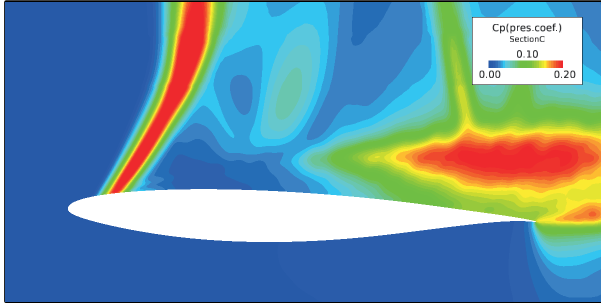
Section H ($\eta=0.85$)

126

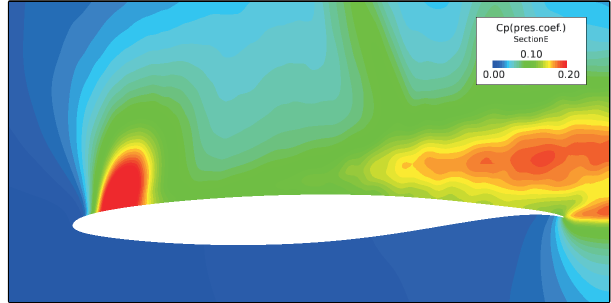
Case 3: Cp RMS ($\alpha=5.92\text{deg}$)



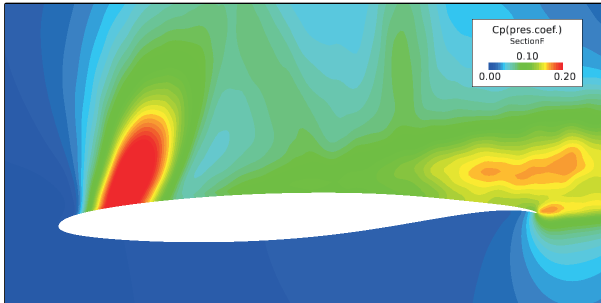
ID:A1



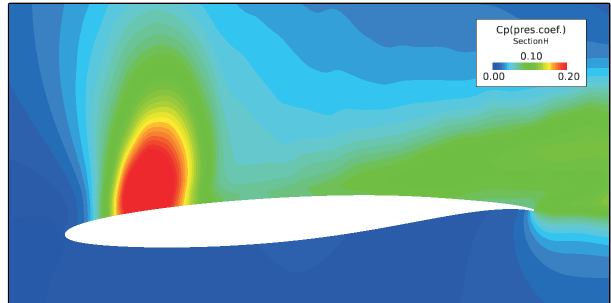
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



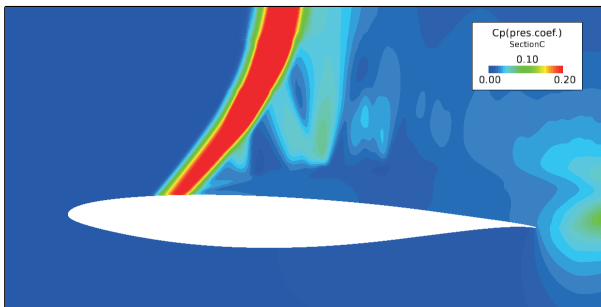
Section H ($\eta=0.85$)

127

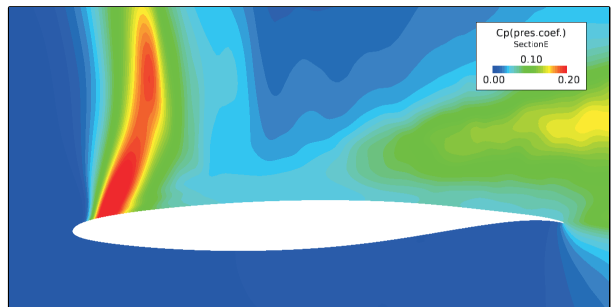
Case 3: Cp RMS ($\alpha=5.92\text{deg}$)



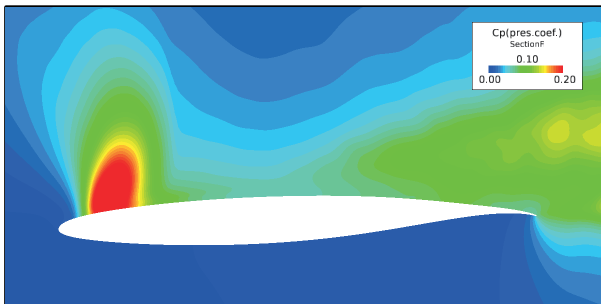
ID:A2



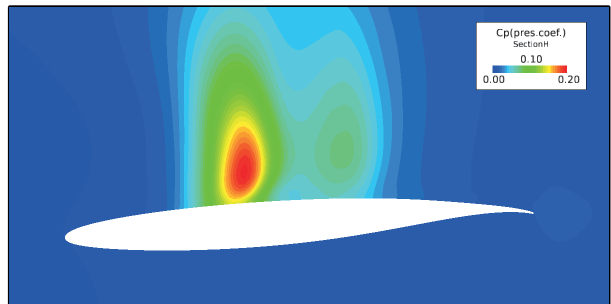
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



Section H ($\eta=0.85$)

128

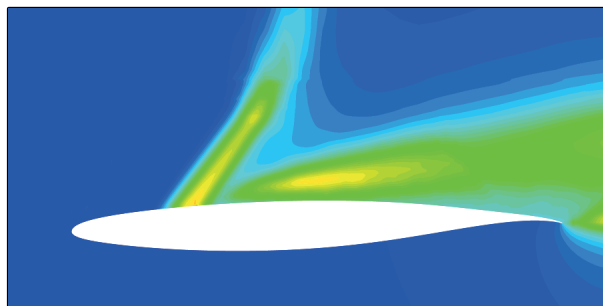
Case 3: Cp RMS ($\alpha=5.92\text{deg}$)



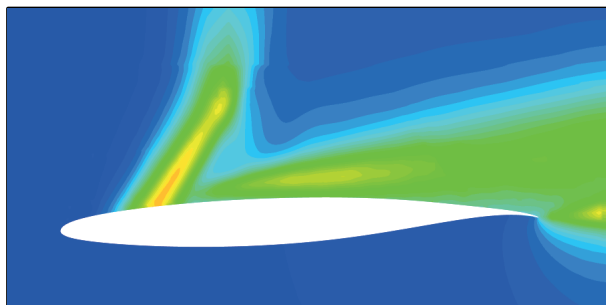
ID:H



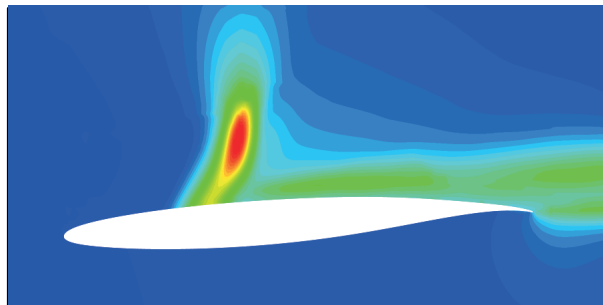
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



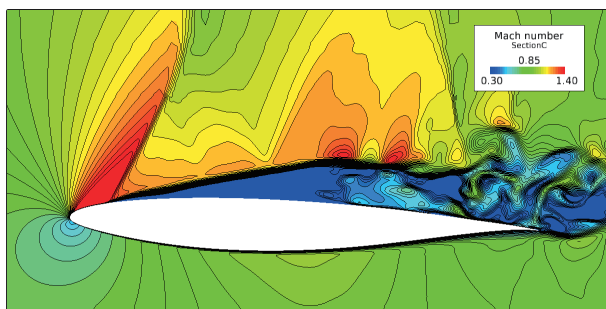
Section H ($\eta=0.85$)

129

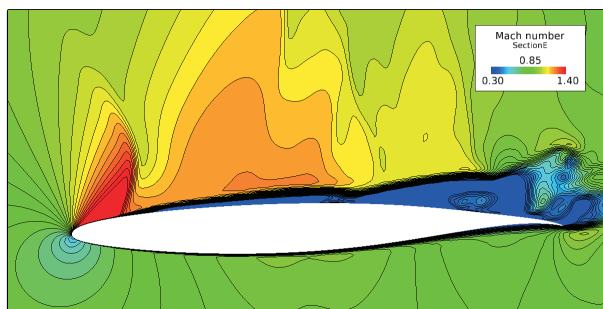
Case 3: Mach number ($\alpha=5.92\text{deg}$)



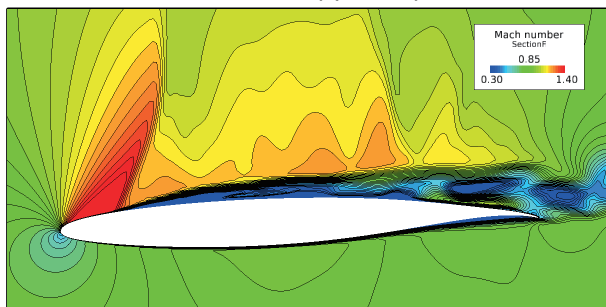
ID:A1



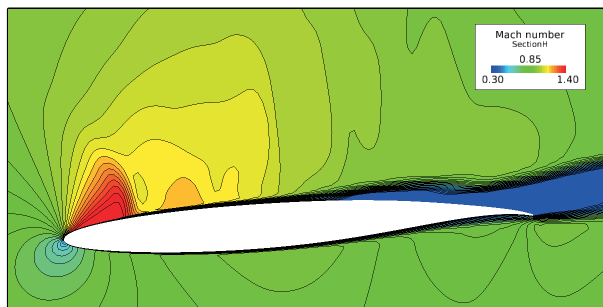
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



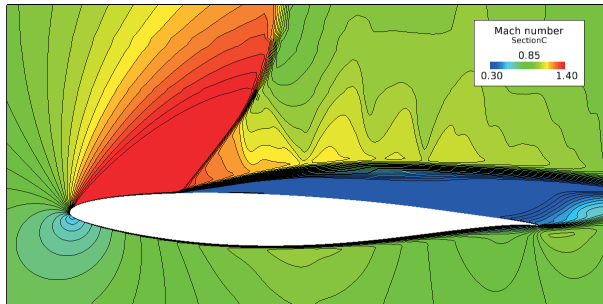
Section H ($\eta=0.85$)

130

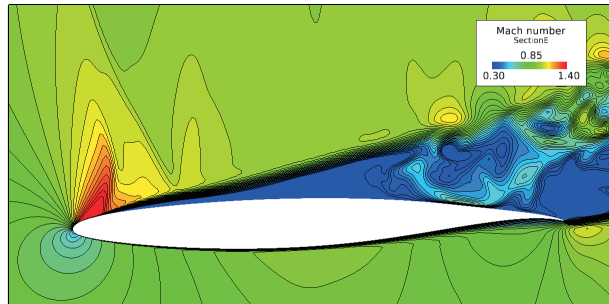
Case 3: Mach number ($\alpha=5.92\text{deg}$)



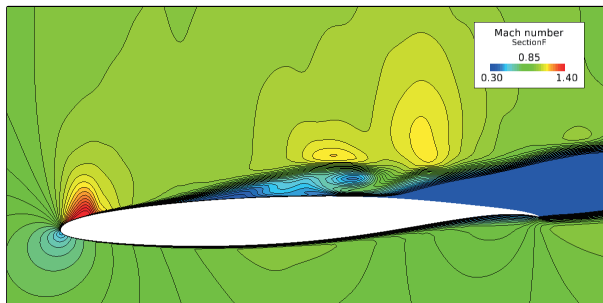
ID:A2



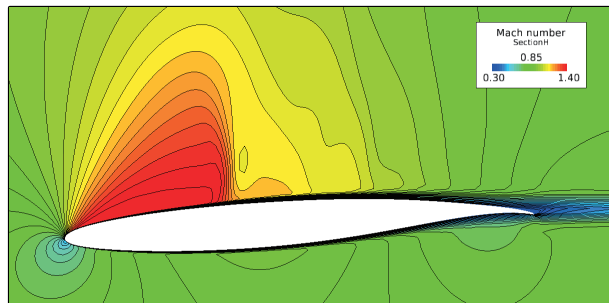
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



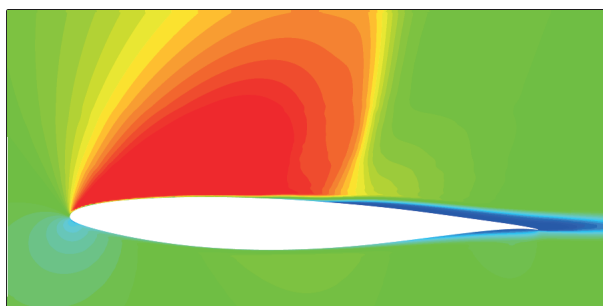
Section H ($\eta=0.85$)

131

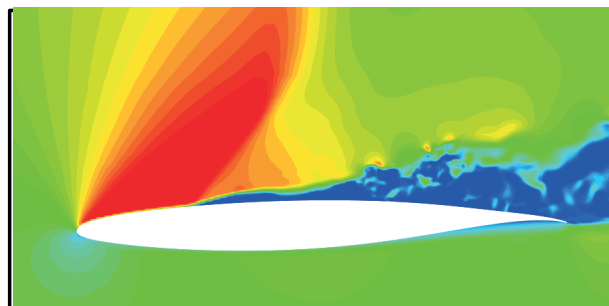
Case 3: Mach number ($\alpha=5.92\text{deg}$)



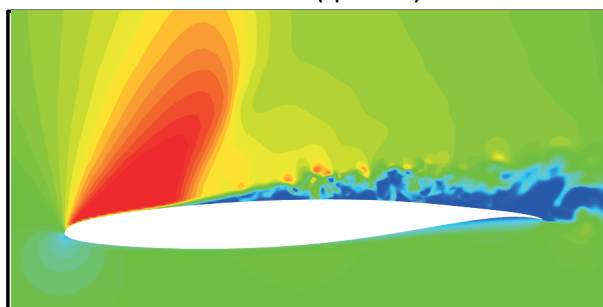
ID:H



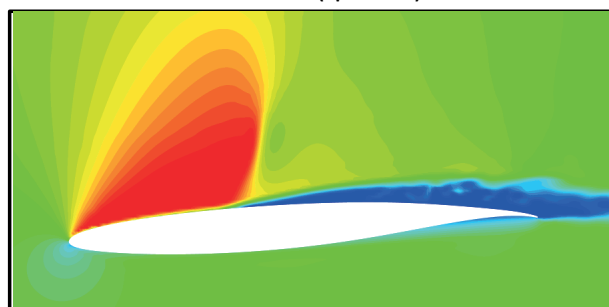
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



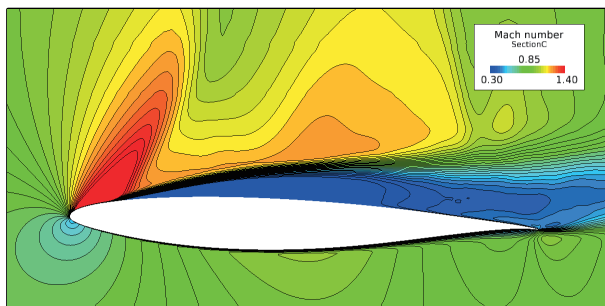
Section H ($\eta=0.85$)

132

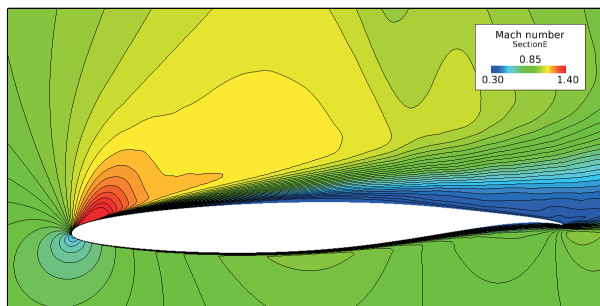
Case 3: Mach number average ($\alpha=5.92\text{deg}$)



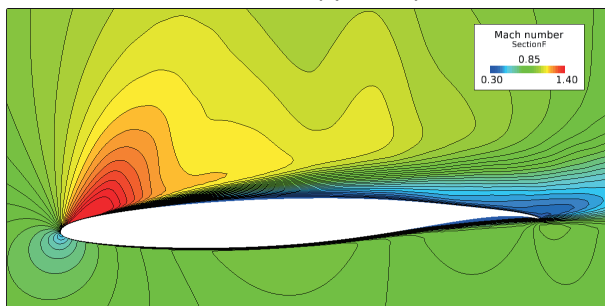
ID:A1



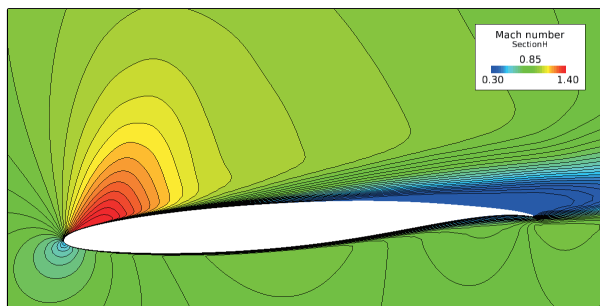
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



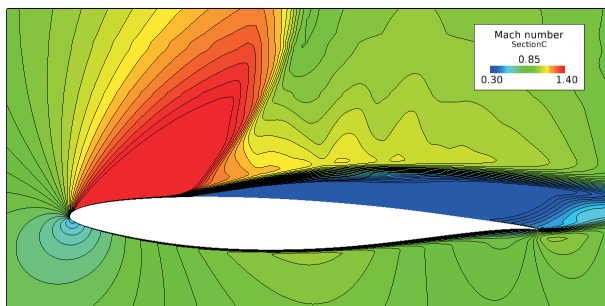
Section H ($\eta=0.85$)

133

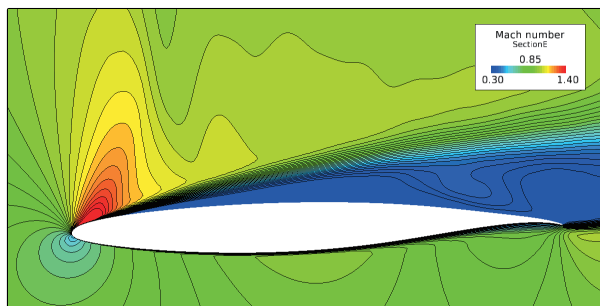
Case 3: Mach number average ($\alpha=5.92\text{deg}$)



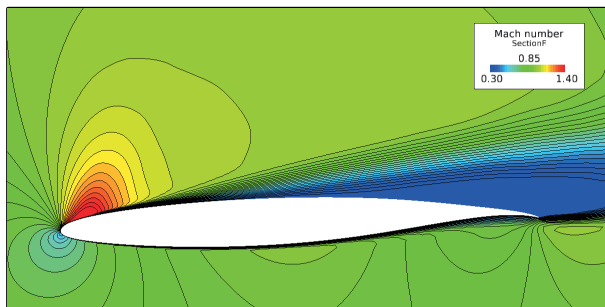
ID:A2



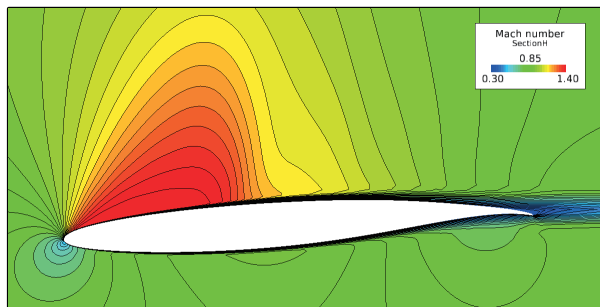
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)

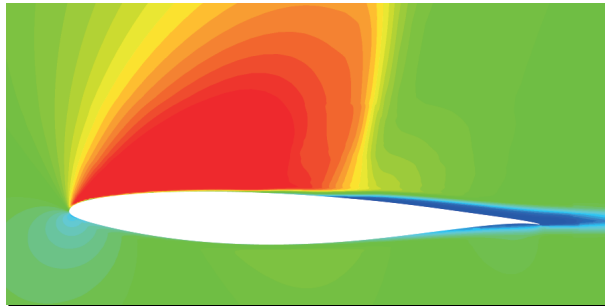
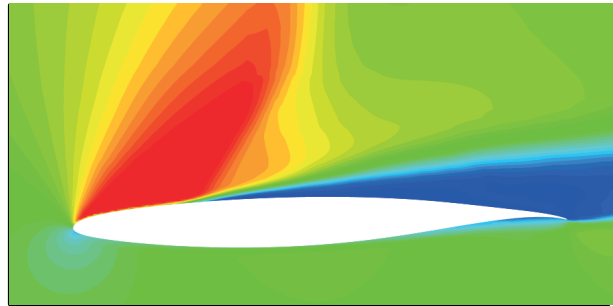
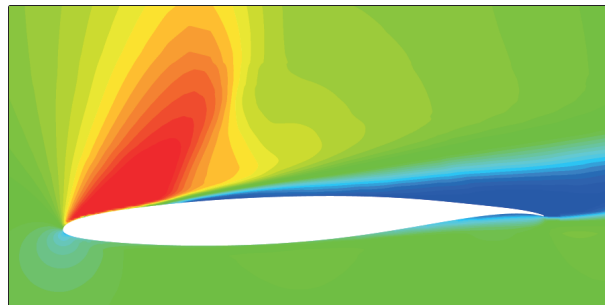
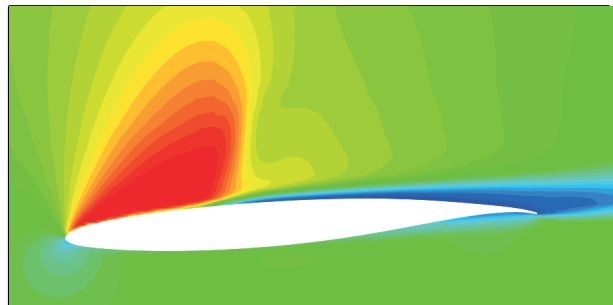


Section H ($\eta=0.85$)

134

Case 3: Mach number average ($\alpha=5.92\text{deg}$)

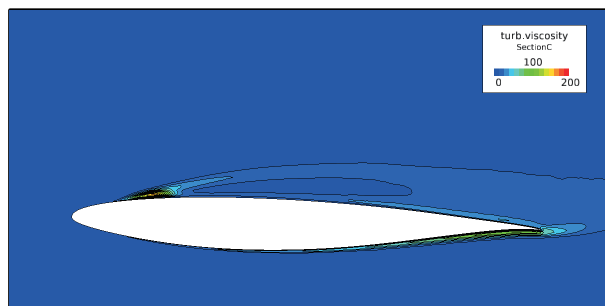
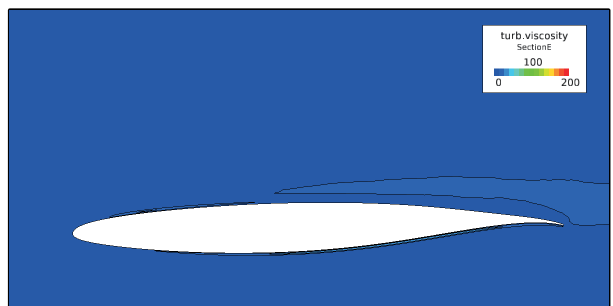
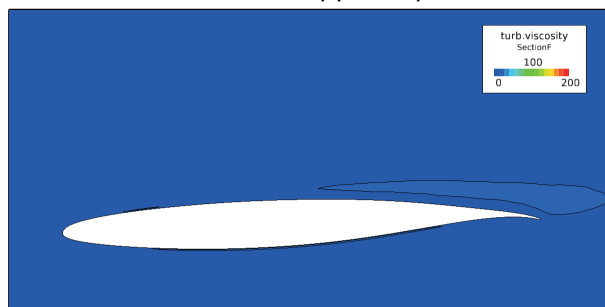
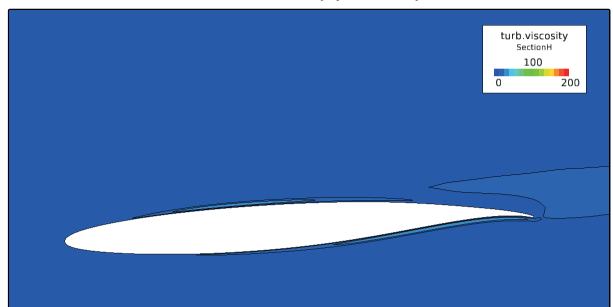
ID:H

Section C ($\eta=0.28$)Section E ($\eta=0.50$)Section F ($\eta=0.60$)Section H ($\eta=0.85$)

135

Case 3: Eddy viscosity average ($\alpha=5.92\text{deg}$)

ID:A1

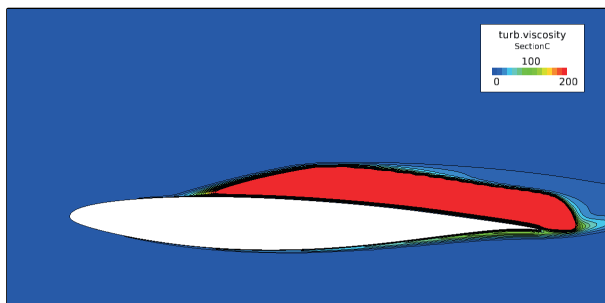
Section C ($\eta=0.28$)Section E ($\eta=0.50$)Section F ($\eta=0.60$)Section H ($\eta=0.85$)

136

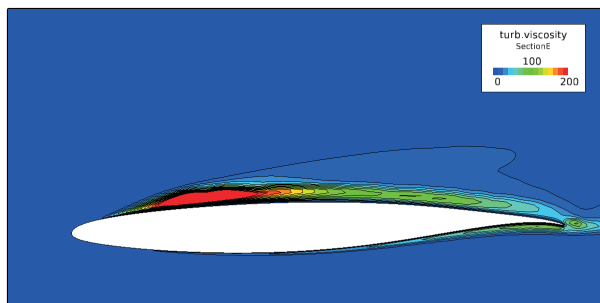
Case 3: Eddy viscosity average ($\alpha=5.92\text{deg}$)



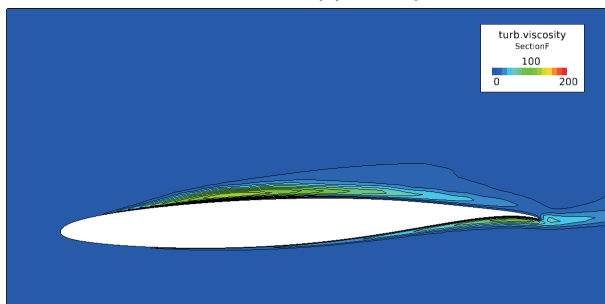
ID:A2



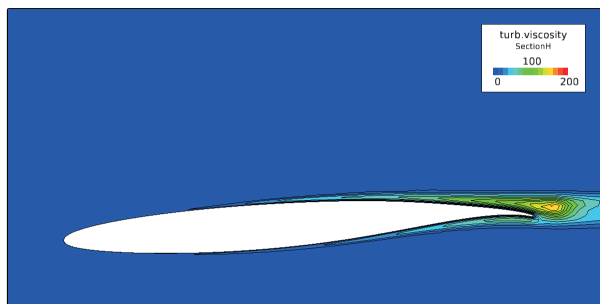
Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



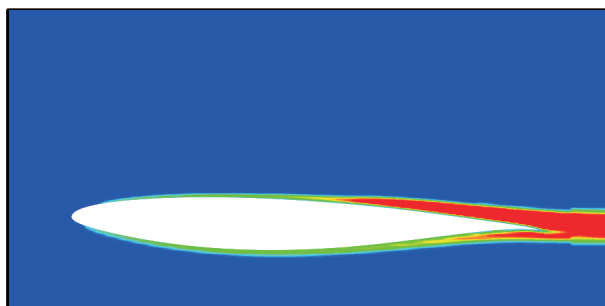
Section H ($\eta=0.85$)

137

Case 3: Eddy viscosity average ($\alpha=5.92\text{deg}$)



ID:H



Section C ($\eta=0.28$)



Section E ($\eta=0.50$)



Section F ($\eta=0.60$)



Section H ($\eta=0.85$)

138

Case 3: Summary



- We collected three submitted data from two groups.
- The prediction of shock wave location is still difficult. (The results are almost same as those of APC-II)
- The PSD is similar to the experiment.
- The resolution of separated flow behind the shock wave is different between the data.
- The eddy viscosity development is different between the data.

139

Important days



- Submission of PowerPoint files
 - Deadline: 14 July
 - The slides are published as JAXA-SP
 - Please submit a PowerPoint file (Do not submit a PD). Read-only PowerPoint is also acceptable.
- The 53rd Aircraft Symposium (20-22 November)
 - Organized session “APC-III”

140

Acknowledgements



- We would like to thank all participants for submitting data.
- We also would like to thank for the following corporations,
 - Grid generation: Dr. Kazuomi Yamamoto, Dr. Mitsuhiro Murayama, Dr. Yasushi Ito (JAXA), Mr. Kentaro Tanaka (Ryoyu Sysmtems)
 - Grid deformation: Dr. Kanako Yasue (JAXA)
 - Web, Pre/Post processing: Kenji Hayashi, Keiji Ueshima, Takahiro Yamamoto (Ryoyu Systems)
 - Experimental data: Shunsuke Koike (JAXA), Yosuke Sugioka, Taku Nonomura, Keisuke Asai (Tohoku University)

141

Computational Information



ID	Grid	Turbulence Model	Spec	Core	Time	Memory
A	HexaGrid	SA-noft2-R-QCR2000	SPARC64XIfx(2GHz) (JAXA Supercomputer System generation 2 SORA-MA)	96	3h6m	21.4G
		SST-2003			3h24m	29.7G
		SST-2003-sust			3h36m	29.7G
		SST-2003-sust-QCR2000			4h6m	29.7G
		EARSM			4h48m	29.4G
		EARSM(w/o nonlinear)			3h54m	29.4G
		EARSM-QCR2000 (w/o nonlinear)			4h12m	29.4G
	MEGG3D	SA-noft2-R-QCR2000			2h20m	26.1G
		SST-2003			8h56m	27.4G
		SST-2003-sust			8h56m	27.4G
		SST-2003-sust-QCR2000			11h48m	27.4G
		EARSM			14h6m	27.2G
		EARSM(w/o nonlinear)			13h30m	27.2G
		EARSM-QCR2000 (w/o nonlinear)			15h	27.2G

142

Computational Information



ID	Grid	Turbulence Model	Spec	Core	Time	Memory
A ●	UPACS	SA-noft2-R-QCR2000	SPARC64XIfx(2GHz) (JAXA Supercomputer System generation 2 SORA-MA)	96	1h26m	21.4G
		SST-2003			1h42m	22.4G
		SST-2003-sust			1h54m	22.4G
		SST-2003-sust-QCR2000			2h6m	22.4G
		EARSM			2h24m	22.2G
		EARSM(w/o nonlinear)			2h	22.2G
		EARSM-QCR2000 (w/o nonlinear)			2h6m	22.2G
	Custom (Cartesian based)	SA-noft2-R-QCR2000			3h29m	26.8G
		SST-2003			10h42m	28.3G
		SST-2003-sust			13h6m	28.3G
		SST-2003-sust-QCR2000			13h30m	28.3G
		EARSM			16h18m	28G
		EARSM(w/o nonlinear)			13h	28G
		EARSM-QCR2000 (w/o nonlinear)			14h6m	28G

143

Computational Information



ID	Grid	Turbulence Model	Spec	Core	Time	Memory
C ●	Custom (MEGG3D+BCM)	SA	SGI UV2000	160	168h	18G
D ●	Custom (Octree Cartesian)	SA-noft2-R-QCR2000	Xeon E5-2695 v4	144	5h20m	60G
E ●	HexaGrid	SST-2003	Intel Xeon CPU E5-2697 v4 @ 2.30GHz	36	18h30m	27.3G
F ●	HexaGrid	SST-2003	Intel Xeon E5-2697 v2 (2.7 GHz) (九州大学hakozaiki)	384	50h	613G
		SS/SST-2003 Hybrid			50h	613G
I ●	Custom (polyhedra)	SST	Intel(R) Xeon(R) CPU E5-2697 v3 @ 2.60GHz	28	19h30m	85G
J ●	HexaGrid	SST	Intel Xeon E5-2695 v4 2.10GHz	144	54m	65.4G
	Custom (polyhedra)				1h12m	76.3G

144

Computational Information



ID	Grid	Turbulence Model	Spec	Core	Time	Memory	
K ●	UPACS	SA-fv3(Cmat)	Intel E5 - 2697 V2 - 2.60 GHz	96	1h50m		
		SST-2003(Cmat)			39m		
		SSC-EARSM(Cmat)			2h38m		
	MEGG3D	SA-fv3(Cscal)		Intel E5 - 2697 V2 - 2.60 GHz	72	15h28m	
		SA-fv3(Cmat)				4h28m	
		SST-2003(Cscal)				13h18m	
		SST-2003(Cmat)				4h47m	
		SSC-EARSM(Cscal)				15h17m	
		SSC-EARSM(Cmat)				11h38m	
		KE-YS-1993(Cscal)				13h17m	
		KE-YS-1993(Cmat)				11h37m	
		S-BSL-EARSM(Cscal)				11h29m	
		L ●				HexaGrid	SST