MLI の微小デブリ防護性能評価 Shielding Effect of MLI against Submillimeter Debris

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人工衛星のコンポーネントは、デブリ衝突に対する影響を識別し、衝突リスクが許容されない場合は何らかの 防護材を適用する必要性がある.防護材として搭載実績が高いのは ISS のシールド材として使用されている アルミ合金板であるが、無人宇宙機にとっては重量増加の影響が大きい。新たな軽量防護材の研究開発が 行われているが、耐宇宙環境性能の評価まで完了している材料は極めて少ない.

そこで本研究では MLI の微小デブリ防護性能を評価し, 防護性能を向上させる構成を調べた. 中間層に厚みのあるフィルムを使用して MLI 全体の面密度を向上させれば, MLI でも直径 0.1 mm のデブリ貫通を防ぐ 効果があることがわかった. 最外層に ITO(インジウムすず酸化物)膜を持ったフィルムを使用した場合は模擬デブリがより細かく砕かれた. 最外層はデブリ破砕に対する影響が高いと考えられる. また貫通痕の観察 結果から, 中間層にエンボス加工フィルムを使用すると, 防護性能の向上が示唆された.

Components of JAXA's spacecrafts are identified effects on debris collision before its launch. If the risk is not acceptable, a debris shield is added to the component. An aluminum alloy plate has high reliability since it has been used as a shield of the ISS. For an unmanned spacecraft, however, the effect on the total weight is not ignorable. A lot of light-weight bumpers have been developed before now.

Almost all new bumpers have not finished assessments of protective abilities against space environment. This study investigated shielding effects of MLI blankets. The MLI blanket captured projectiles of 0.1mm in diameter when its areal density was increased by using thick reflectors. If an outer film was covered with ITO (Indium-Tin Oxide), the projectile fractured more. An outer film is considered to influence with fragmentation of debris. Moreover, embossed reflector films seemed to improve shielding effects of a MLI blanket.



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JAXA Spacecraft Design Standards

② ● ★ http://sma.jaxa.jp/TechDoc/ タマ C 図 宇宙航空研究開発機構~ ×
JIMK/JERG
JAXA共通技術又書
TOP > JAXAについて > 組織図 > 安全・信頼性推進部 > JAXA共通技術文書
1. クロシリム自住会示人自 1. 1MB-001 システム安全連進 型 Ø English
- 1MR-002 ロケットペイロード安全標準 型 O English
<u>- 1MR-004</u> 信頼性プログラム標準 型
— JMR-005 品質保証プログラム標準 第 ● English
- JMR-006 コンフィギュレーション管理標準 2 ● English
JMR-012 電気・電子・電気機構部品プログラム標準 🔁
JMR-013 品質プログラム標準(基本要求 JIS Q 9100) 落
→ JERG-0-001 宇宙用高圧ガス機器技術基準 型
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JERG-0-043 宇宙用表面実装はんだ付工程標準 12
— JERG-0-047 再突入機の再突入飛行に係る安全基準 🔁
— JERG-0-049 ソフトウェア開発標準 № ● English
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— JERG-0-051 海外コンポーネント品質確保ハンドブック
— JERG-0-052 宇宙転用可能部品の宇宙適用ハンドブック(共通編)
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ロケット
— JERG-1-008 ロケット搭載ソフトウェア開発標準 24
— JERG-1-009 ロケット機器用鉛フリー部品適用工程標準 🔁
— JERG-1-010 宇宙転用可能部品の宇宙適用ハンドブック(ロケット編) 💈

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-	JERG-2-000	宇宙機 (人工衛星・探査機) 設計標準 💆 🛛 English
	JERG-2-023	宇宙転用可能部品の宇宙適用ハンドブック(長寿命衛星編)
	JERG-2-024	宇宙転用可能部品の宇宙適用ハンドブック(科学衛星編) 🄁
	JERG-2-100	システム設計標準 12
-	JERG-2-120	単一故障·波及故障防止標準 🔁
	JERG-2-130	宇宙機一般試験標準 🄁
-	JERG-2-141	宇宙環境標準 12
	JERG-2-142	一般環境標準(宇宙機) ங
-	JERG-2-143	耐放射線設計標準 🔁 🛛 English
-	JERG-2-144	微小デブリ衝突耐性評価標準 № ● English
-	JERG-2-151	ミッション・軌道設計標準 四
-	JERG-2-152	擾乱管理標準 🔁 💿 English
-	JERG-2-153	指向管理標準 🔁
	JERG-2-200	電気設計標準 12
-	JERG-2-211	帯電・放電設計標準 № O English
	JERG-2-212	ワイヤディレーティング標準 🔁 🛛 English
-	JERG-2-213	絶縁設計標準 💁 💿 English
-	JERG-2-214	電源系設計標準 🔁 🛛 English
-	JERG-2-215	太陽電池パドル系設計標準 🔁 💿 English
-	JERG-2-241	EMC設計標準 🔽 🛛 English
	JERG-2-310	熱制御系設計標準 🔁 🛛 English
	JERG-2-320	構造設計標準 🔁
	JERG-2-330	機構設計標準 💁 💿 English
-	JERG-2-340	宇宙機用推進系設計標準 🏂
	JERG-2-400	通信設計標準 🔁 💿 English
	JERG-2-420	RF回線設計標準 12
	JERG-2-431	MIL-STD-1553Bオンボードサブネットワーク設計標準 💆
	JERG-2-500	制御系設計標準 🔁 🛛 English
	JERG-2-510	姿勢制御系設計標準 🔁 🛛 English
	JERG-2-600	ソフトウェア開発標準(宇宙機用) 2
-	JERG-2-610	宇宙機ソフトウェア開発標準 🔁 🛛 English
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-	JERG-3-001	地上設備・装置品質プログラム標準 翔

Background



Impact of sub-millimeter debris is a threat of mission failure for LEO satellites.

Sub-millimeter projectile impact data on spacecraft component are not enough to debris protection design for spacecraft.



JAXA is summarizing

examples of hypervelocity

impact experiment and numerical simulation data on the Space Debris Protection Design Manual (JERG-2-144-HB001).

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Vulnerability of Spacecraft Component





Impacts of projectiles larger than 0.3mm in dia. showed negative effects on power harnesses

Spacecraft components are vulnerable against small debris impacts → Critical components are protected if the collision risk is not acceptable



Debris Shielding Material

Bumper shield installed on the ISS

→ Inducing weight increase of spacecraft because its main material is aluminum alloy

Ref. 東出他, 遊星人, 2015.

Bumper shield made of high-strength fiber woven

 \rightarrow Having high protective ability & flexible structure

 \rightarrow Having restrictions for use (temperature, radiation, etc.)

Multi layer insulation (MLI) blankets are normally installed on out-side of spacecraft

→ Can MLI blankets shield spacecraft from sub-millimeter debris impacts?

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Past Research of MLI blankets

Ref. Lambert , Adv. Space Res., 1997.

Lambert conducted the experiments on MLI blankets (22 ply) put on the aluminum plate (2 mm in thickness).

Ballistic limit energies were investigated when aluminum spheres impacted at 6 km/s.

Table 1. Relative performances of MLI in front of aluminium plates

Configuration	Surface density (g/cm ²)	Ballis energ	tic limit y at 6 km/s (J)	Surface density of aluminium to defeat same energy (g/cm ²)	koo (Eq. 1)
Aluminium Aluminium + MLI Aluminium + 2 MLI Aluminium + 3 MLI Aluminium + MLI + 10 mm spacing	0.56 0.62 0.68 0.73 0.62	9 25 85 125 45	0.71 0.99 1.49 1.70 1.21	0.56 0.81 1.26 1.43 1.01	0.42 0.32 0.23 0.21 0.26

↑Projectile diameter (mm)

Energy absorption by MLI blanket was confirmed against impacts of approximately 1 mm projectiles.

→ Shielding effect of MLI is also expected against sub-millimeter debris impact.

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Objective

Investigate shielding effects of MLI blankets against sub-millimeter debris impacts

Tested specimens: Typical MLI blankets installed on LEO satellites MLI blanket consisting of embossed films

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Example of MLI Stracture

Outer layer: Aluminized polyimide film (with radiation coating)

Reflector layer: Aluminized polyester film, Aluminized polyimide film (several layers)

Separator: Plastic mesh

Inner layer: Aluminized polyimide

App.

2mm



Tested MLI Blankets

ID	MLI - I	MLI - II	MLI - III	MLI - IV	MLI - V	
Weight	268 g/m ²	229 g/m ²	315 g/m ²	154 g/m²	268 g/m ²	
Outer	Single Aluminized Polyimide, 50µm	Double Aluminized Polyimide, 25µm	Single Aluminized Polyimide, 25µm	Double Aluminized Polyimide, 25µm	ITO Coated Aluminized Polyimide, 50µm	
	Double Aluminized Polyester					
Reflector	6µm, 10ply	6µm, 10ply	12μm , 10ply	6µm , <mark>6ply</mark>	6µm, 10ply	
Separator	Polyester Mesh					
Inner	Double Aluminized Polyimide, 25µm					

ITO: Indium-Tin Oxide, Use for holding lower surface potential

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Experimental Conditions

Impact velocity 6 km/sec

Projectiles SUS304, Sphere d_p=0.1mm, 0.3mm



4 corners of a blankets were fixed on an aluminum alloy plate

Inner layer roughly contacted on surface of an aluminum alloy plate

Aluminum alloy plate A2024-T3, t=5mm



Results

ID	MLI - I	MLI - II	MLI - III	MLI - IV	MLI - V
Mark	Thick outer film	Standard	Thick reflectors	Half layers	ITO outer film
Weight	268 g/m ²	229 g/m²	315 g/m²	154 g/m²	268 g/m ²
Outer	Single Aluminized Polyimide, <mark>50µm</mark>	Double Aluminized Polyimide, 25µm	Single Aluminized Polyimide, 25µm	Double Aluminized Polyimide, 25µm	ITO Coated Aluminized Polyimide, 50µm
Reflector	6μm, 10ply	6μm, 10ply	<mark>12μm</mark> , 10ply	6µm, <mark>6ply</mark>	6μm, 10ply
0.3mm	Perforation				
0.1mm	Perforation	Perforation	Non Perforation	Perforation	Perforation
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Damage of Outer Films (0.1mm)

ID	MLI - I	MLI - II	MLI - III	MLI - IV	MLI - V
Mark	Thick outer film	Standard	Thick reflectors	Half layers	ITO outer film
Outer film	Single Aluminized Polyimide, 50µm	Double Aluminized Polyimide, 25µm	Single Aluminized Polyimide, 25µm	Double Aluminized Polyimide, 25µm	ITO Coated Aluminized Polyimide, 50µm
Front surface	• <u>100</u> µт »	100µm	100jum	ОО́; 100µт	100µт

Aluminized surfaces were observed around perforated holes in the cases of single aluminized outer films. \rightarrow Back surface or 2nd layer (reflector surface) $\frac{12}{200}$ $\frac{12}{200}$



Damage of Inner Films (0.1mm)

ID	MLI - I	MLI - II	MLI - III	MLI - IV	MLI - V		
Mark	Thick outer film	Standard	Thick reflectors	Half layers	ITO outer film		
Inner	Double Aluminized Polyimide, 25µm						
Back surface	200µm	200µm	Non Perforation	200µm	200 um		

Perforated holes were larger than outer layers. On the film of MLI-V, groups of smaller holes were observed. \rightarrow ITO coating seems to contribute fragmentation of a projectile.

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Crater Volume (0.3mm)

All MLI blankets were perforated by impacts of 0.3 mm projectiles → Measure volumes of craters on aluminum plates behind the blankets



MLI blankets seem to have effects to reduce by about 20% of impact energies.



Embossed Refrector

Embossing: Method for making concavo-convex pattern



Merits:

Separators are not used because contacting area between layers is quite small due to embossed pattern

 \rightarrow Acceptable temperature does not depend on separator material

 \rightarrow Workability is improved

Demerits:

Cost is higher

Total thickness of the blanket becomes thick due to embossed pattern

→ Can it induce higher shielding effects?

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Structure of Embossed MLI blankets



Outer layer: Aluminized polyimide film (with radiation coating)

Reflector layer:

Embossed Aluminized polyester film, Embossed Aluminized polyimide film (several layers)



Inner layer: Aluminized polyimide



Tested MLI

ID	MLI - II	MLI-E	
Weight	229 g/m ²	239 g/m ²	
Outer	Double Aluminized Polyimide, 25µm		
Reflector	Double Aluminized Polyester Film, 6μm, 10ply	Embossed Double Aluminized Polyester Film, 350-400μm, 10ply	
Separator	Polyester Mesh	None	
Inner	Double Aluminized Polyimide, 25µm		

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Impact Test Result

0.1 mm projectiles did not perforate the embossed MLI blanket \rightarrow Showed high shielding effect

Measurement of crater volumes on the aluminum plate is ongoing







Summary

As a result of hypervelocity impact experiments for 6 kinds of MLI blankets, shielding effect of the MLI blankets were found against sub-millimeter projectile impacts.

Projectiles of 0.1 mm in diameter were captured in the MLI blanket made from thick reflectors (12 μ m) and one from embossed reflectors.

ITO coating of outer layer seemed to improve shielding effects because projectiles were fractured to smaller fragments.

MLI blankets can reduce 20% of projectile impact energies.

Use of embossed films as reflector material can improve shielding effects against sub-millimeter debris impact.

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