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Kevlar・Beta Clothの微小デブリ貫通限界重量と厚さ

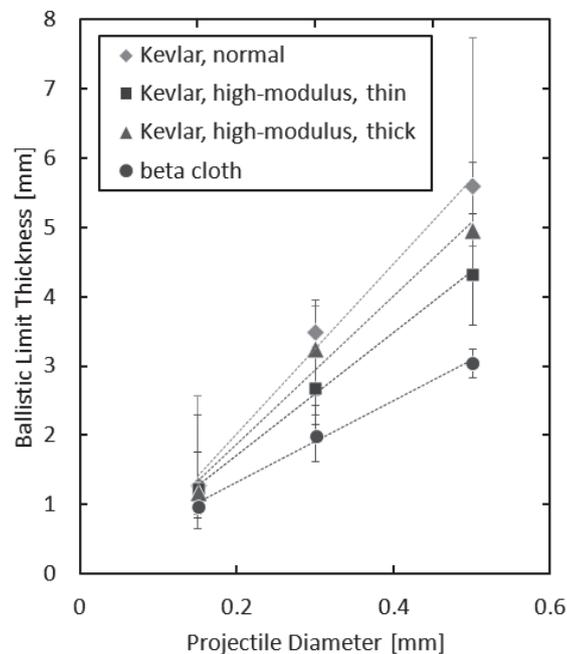
Ballistic Limit Weight and Thickness of Kevlar and Beta Cloth for Sub-millimeter Debris Impact

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デブリ衝突頻度の高いコンポーネントには防護性能の高い材料を採用することが望ましい。しかし、進展部やハーネス等の柔軟な構造は防護性能の高い材料を適用することが困難で、衝突に対して脆弱である。これらを防護するために、形状に柔軟性のあるバンパ材料が必要とされている。本研究では高強度繊維織布に着目をした。高強度繊維のうち、アラミド繊維は超高速衝突に対しても優れた防御性能を持つことが知られており、国際宇宙ステーションに搭載されているデブリバンパ材料として使用されている。デブリ環境モデルによると、低高度軌道の人工衛星は1mm以下のデブリ衝突頻度が高い。従って、本研究では高強度繊維織布に1mm以下の微小デブリが衝突した時の貫通限界について調べた。Kevlar織布とBeta Clothの貫通限界について報告する。

To protect a satellite from space debris impact threat, a satellite designer should employ structure material which has enough protection capability against debris impact. However, for some flexible components, it is impossible to use such strong materials, for example, expandable structures and wire harnesses. To protect these flexible components, a flexible debris bumper is needed. High strength fiber fabric is one of flexible debris bumper material. Since the alamido fiber has high tensile and shear strength, the alamido fiber fabric is known to be also useful for high velocity impact protection. The alamido fiber fabric was used as a part of the Staffed Whipple Bumper installed on the International Space Station. A satellite on the low earth orbit needs to pay attention to impacts on debris smaller than 1 mm, because debris environment models show such small debris will impact on the satellite during its operation lifetime. Therefore, to employ the alamido fiber fabric as a debris bumper, it is necessary to know their sub-millimeter debris impact damage. The purpose of this study is to investigate sub-millimeter debris impact damage of the fiber fabric.





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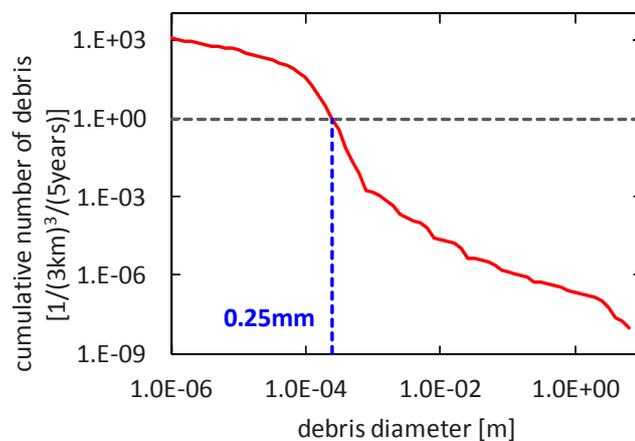


Background

Sub-millimeter debris impact is threat of mission failure for LEO satellites.

Important components, their failure means critical damage for the satellite, should be installed inside of satellite structure.

However, it is impossible for some components. (expandable structure, harnesses, etc.)



debris flux in LEO calculated by MASTER2009

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Purpose

To protect components installed on the outside of the satellite structure, flexible debris bumper is needed.

→ **Fabric bumper shield** made of high strength fiber

Investigate ballistic limit weight and thickness of fabric bumper shield

- Alamido fiber fabric (Kevlar cloth)
- Glass fiber fabric coated with aluminum (Beta cloth)



Procedure

1. Perform HVI experiments on a stack of high strength fiber fabrics
2. Count perforated layers in the impacted stack
3. Calculate perforated thickness from the perforated layers
→ **Ballistic limit thickness**
4. From the ballistic limit thickness, calculate areal density of the perforated layers
→ **Ballistic limit weight**



Kevlar Fiber

Kevlar: Alamido fiber

特性	単位	KEVLAR®29	KEVLAR®49
原糸			
緯度(フィラメント数)	dtex (本)	1,670 (1,000)	1,270 (768)
密度	g/cm ³	1.44	1.45
平衡水分率*1	%	4.5	3.5
*1 一度乾燥にした後24℃、55%RHで保持			
機械的性質(原糸)		ASTM D885-85 (参考)JIS L1017	
引張強力	N	338.0	264.0
引張強度	cN/tex (g/d)	203 (23.0)	208 (23.6)
tensile strength	MPa	2,920	3,000
引張弾性率	cN/tex (g/d)	4,900 (555)	7,810 (885)
tensile modulus	GPa	70.5	112.4
破断時伸度	%	3.6	2.4
fracture elongation			

Ref. DuPont

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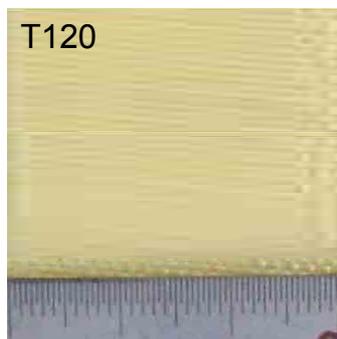
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Kevlar Cloth

	T710	T120	T328
Fiber	K29 (normal)	K49 (high-modulus)	K49 (high-modulus)
Weave	Plain		
Fabric Density [bundle/inch]	24x24	34x34	17x17
Areal Density	319g/m ²	58g/m ²	217g/m ²
Thickness	0.43mm	0.08mm	0.33mm



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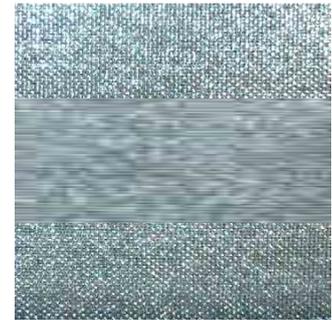
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Beta Cloth

Beta Cloth: Glass fiber fabric coated with aluminum

Parameter (independent of film)	Specified Value	
Cloth type	Beta Cloth	1080
Intermittent temperature range	-151° C to 315° C (-240° F to 600° F)	-199° C to 260° C (-300° F to 500° F)
Continuous temperature range	-151° C to 260° C (-240° F to 500° F)	-185° C to 200° C (-300° F to 400° F)
Fabric side solar absorptance (α_f)	0.45	0.85
Fabric side hemispherical emittance (ϵ_f)	0.80	0.80
Aluminum side absorptance (α_a)	0.22	
Aluminum side hemispherical emittance (ϵ_a)	0.30	
Weight (g/m^2)	274 Typical	170
Thickness	0.008±0.001 in.	
Tensile strength (lb./in. of width)	90 Warp 80 Fill	40 Warp 39 Fill
Tear strength (lb.)	4.0 Warp 4.0 Fill	
Width (in.)	51 (1.30 m)	36 (0.91 m)
Item number	146626	146585
Old part number	G423800	G414500



Ref. Sheldahl

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Glass Fiber Fabric in Beta Cloth

Fiber	ECD450 - Tensile Strength 3200MPa - Tensile Modulus 78GPa
Weave	Plain
Fabric Density	60x46 bundle/inch
Areal Density	47g/m ²
Thickness	0.055mm

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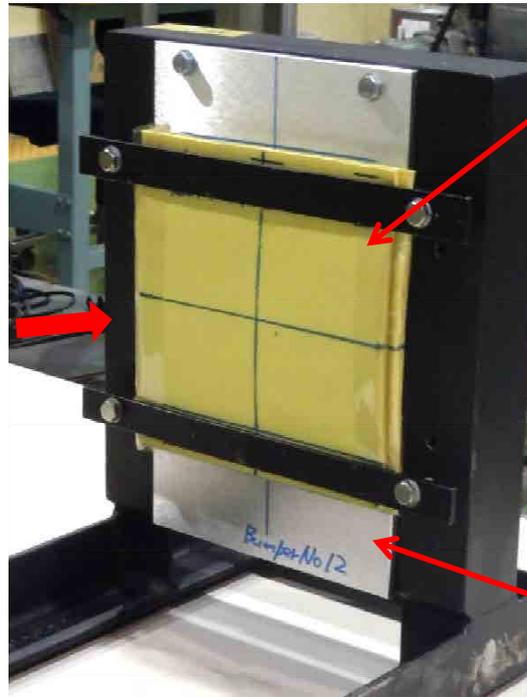


Impact Experiment Condition

Impact velocity
6 km/sec



Projectiles
SUS304, sphere
φ0.15, 0.3, 0.5mm

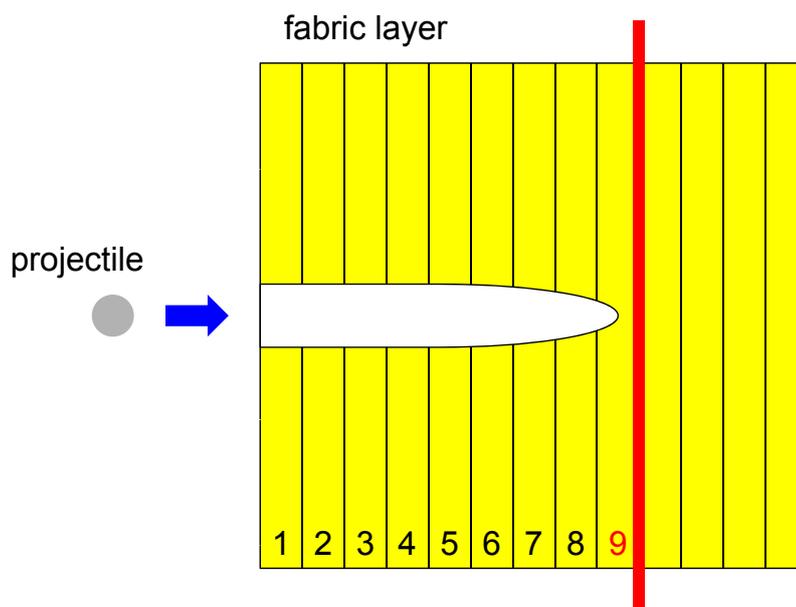


Bumper

Aluminum alloy plate
A2024, t=5mm



Definition of “Perforation”



“Perforated layer + 1 layer” is defined as ballistic limit.

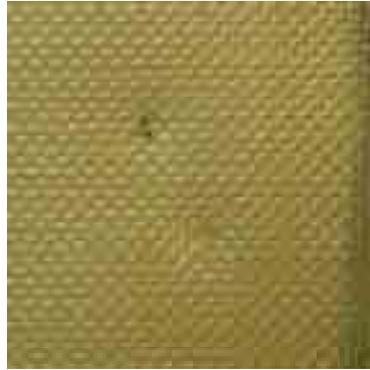


Kevlar T710 ($\phi 0.3\text{mm}$ projectiles)

50mm



Front layer
Impact surface



9th layer
Front surface



9th layer
Back surface



Beta cloth ($\phi 0.3\text{mm}$ projectiles)

50mm



Front layer
Impact surface

Sabot fragment impact



7th layer
Front surface



7th layer
Back surface

Fragment was captured



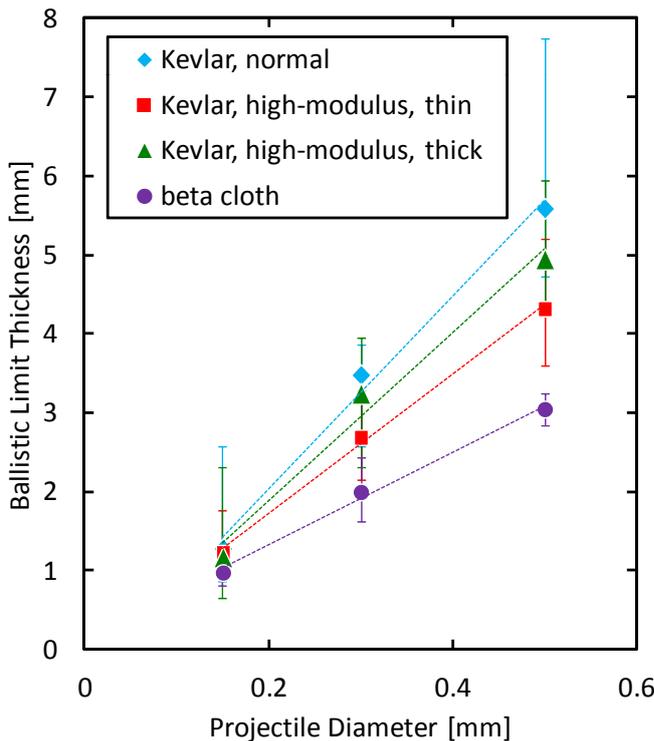
Experiment Results

Impact velocity: 5.61~6.30 km/sec

projectile dia.		Kevlar, normal	Kevlar, high-modulus, thin	Kevlar, high-modulus, thick	Beta Cloth
0.15mm	data	51	53	131	42
	BL	2-6ply	12-22ply	2-7ply	4-6ply
0.3mm	data	10	22	31	12
	BL	6-9ply	27-41ply	7-12ply	8-12ply
0.5mm	data	9	11	14	3
	BL	11-18ply	45-65ply	13-18ply	14-16ply



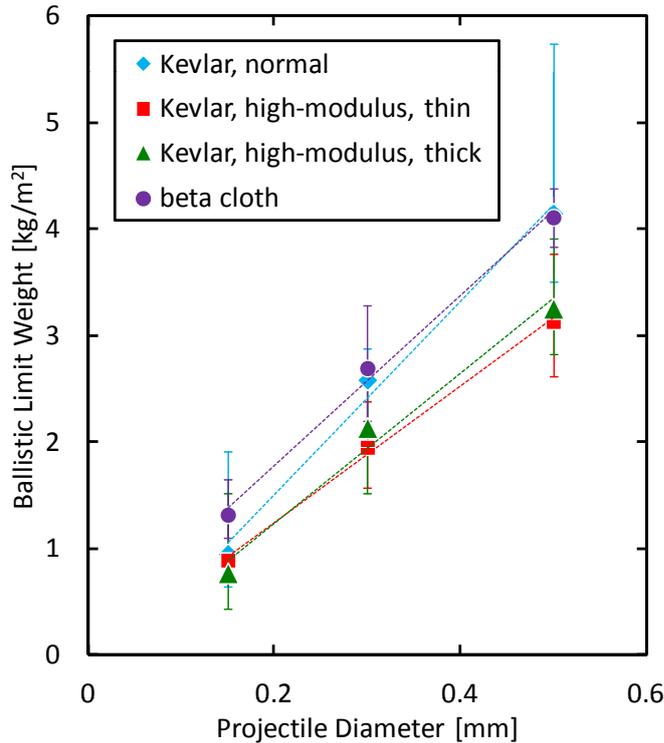
Ballistic Limit Thickness



- Beta Cloth was the thinnest bumper.
- Kevlar cloth made of high modulus fiber showed better protection capability than normal fiber.
- To stack thinner clothes was effective to decrease the ballistic limit thickness.



Ballistic Limit Weight



- High modulus Kevlar cloth was the lightest weight bumper.

- Beta Cloth was the heaviest bumper.

→ To increase areal density contributes to decrease the ballistic limit thickness.

- Kevlar cloth made of high modulus fiber showed better protection capability than normal fiber.

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Comparison with Aluminum Bumper

E.Christiansen, Meteoroid/debris shielding, NASA TP 2003-210788, 2003.

$$\text{when } \frac{\rho_p}{\rho_t} < 1.5 \quad t_w = 1.8 \times 5.24 d^{19/18} H^{-0.25} \left(\frac{\rho_p}{\rho_t} \right)^{1/2} \left(\frac{V_n}{C} \right)^{2/3}$$

$$\text{when } \frac{\rho_p}{\rho_t} \geq 1.5 \quad t_w = 1.8 \times 5.24 d^{19/18} H^{-0.25} \left(\frac{\rho_p}{\rho_t} \right)^{2/3} \left(\frac{V_n}{C} \right)^{2/3}$$

ρ_p : Projectile Density (g/cm³)

ρ_t : Target Density (g/cm³)

t_w : Target Perforation Thickness (cm)

d : Projectile Diameter (cm)

H : Brinell Hardness of Target

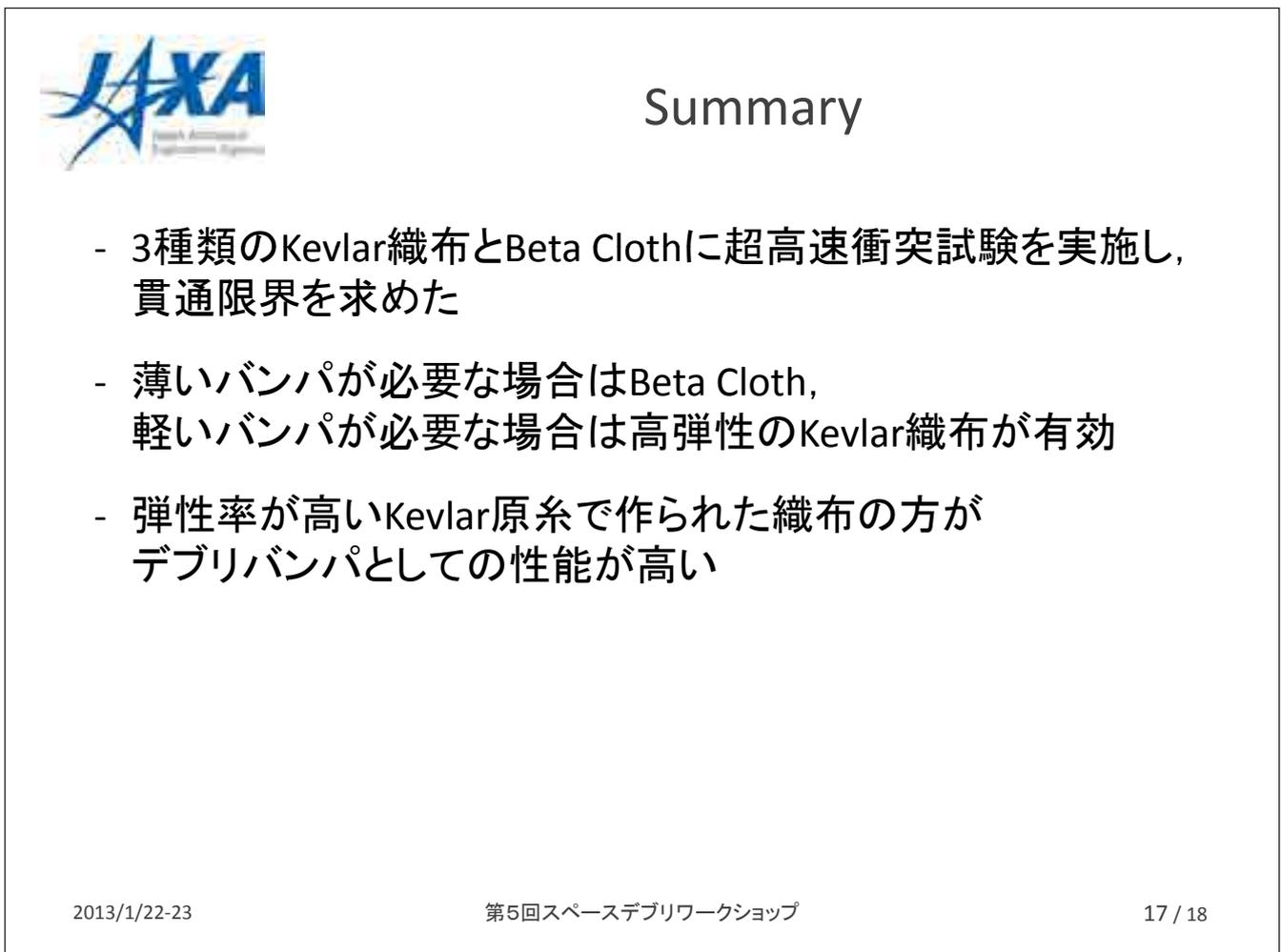
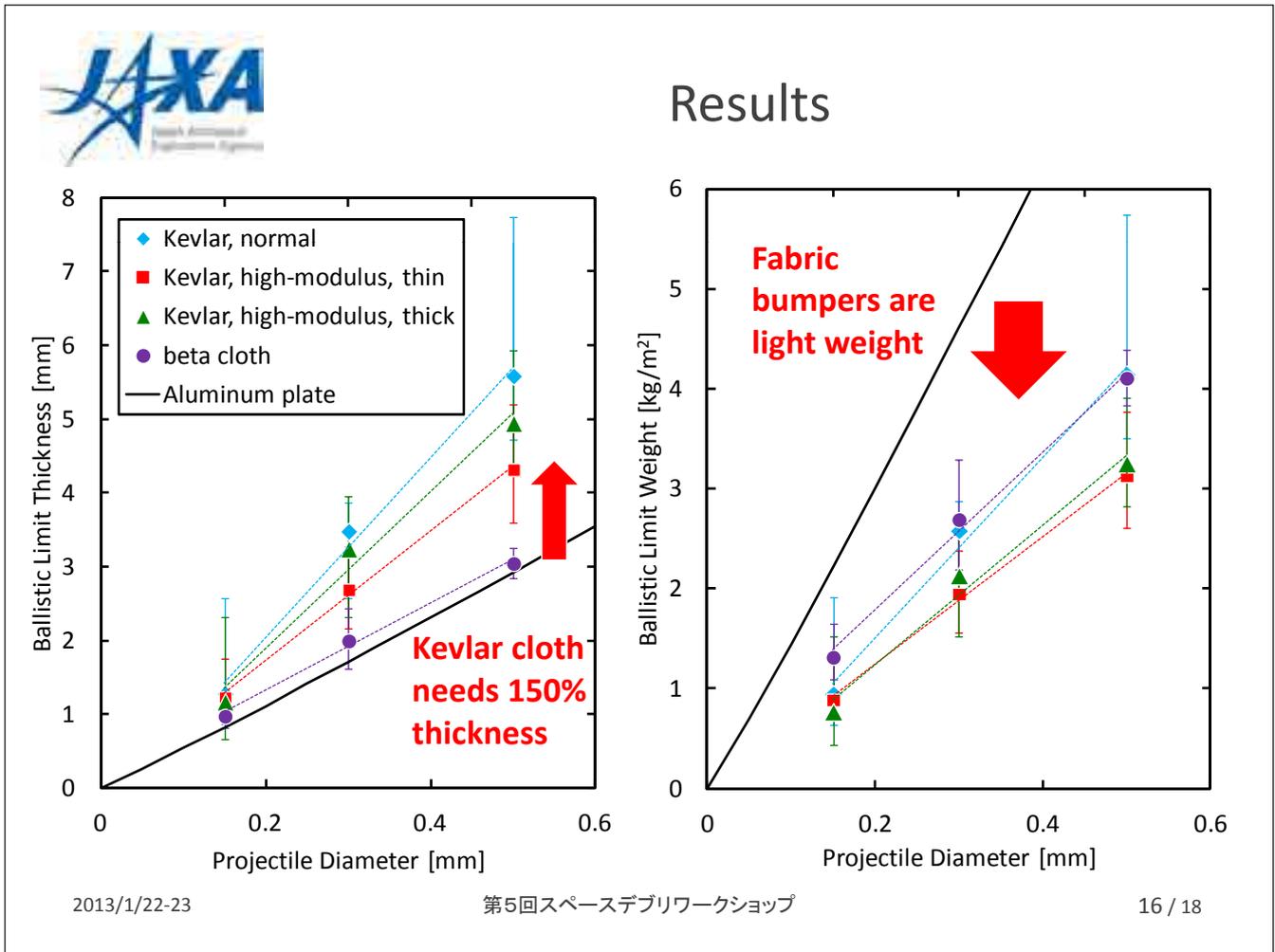
C : Speed of Sound in Target (km/s)

V_n : Normal Component of Impact Velocity (km/s)

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Handbook

材料名	Kevlar T710	Kevlar T120	...	
材料構成	Kevlar(アラミド繊維) 織布 原糸:K29(通常タイプ) 織り方:平織り 密度:24×24本/inch	Kevlar(アラミド繊維) 織布 原糸:K49(高弾性タイプ) 織り方:平織り 密度:34×34本/inch	...	セラミック繊維織布と ガラス繊維織布について 同様の評価を実施予定
1層の厚さ	0.43mm	0.08mm		
1層の重さ	319g/m ²	58g/m ²		
貫通限界式	n=28d-0.97	n=110d-0.46		
入手性	数日	数週間		
作業性	- 切断面から繊維がほつれる	- 切断面から繊維がほつれる - 張力をかけると織目が崩れる		
コメント	- 紫外線に弱い	- 紫外線に弱い		