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要約

JP-4/LOX、JP-4/AIRの燃焼生成物について 平衛組成と燃焼特性値の検討を行った。パラメタとして、 燃焼生成物の化学種の数、及び、JP-4 の組成と生成 熱、LOX の生成熱をとった。

熱焼生成物の熱力学データは、多種の炭火水素熱分解物を含めたG.S.Bahnの熱化学近似テーブル(C-H-N-O系 158化学種)と、JANAF(Joint Arm-Nary-Airforce)熱化学テーブル(46化学種)を用いた。両テーブルの全ての化学種を考慮した平衛組成の比較を行なうと、燃料過剰の混合比で、特に微量成分の濃度ブロフィルに差が大きい。これらの差異は、平衛緩和反応過程等で、微量成分の反応速度を考慮した解析に用いるには無視し得ないオーダである。燃焼生成物の混合物としての比熱、比熱比等の特性値は、温度を断熱火炎温度以下に限定すれば、両テーブルによる差は、最大で約2%である。JP-4の組成・生成熱等の差異にもとづく比熱、比熱比等の差も約2%である。巻末に、G.S.Bahnの熱化学近似テーブルを、多項係数で近似した場合の多項係数と、近似度合を示すグラフをまとめた。

記 号

$A_1 \sim$	A_7	…(1)式で定象	美した熱力	学	データ定数
c_{o}		定圧比熱(標準状態),	cal/mole deg
$H_{\mathrm{T}}^{\mathrm{O}}$		・・・・・エンタルピ	(").	cal/mole
$S_{\mathbf{T}}^{\mathbf{O}}$		エントロピ	(").	cal/mole deg
$F_{\mathrm{T}}^{\mathrm{O}}$		ギブスの自日	由エネルギ		
		(標準状態),	cal/mole
T		ケルビン怎	腹	,	K

1. まえがき

石油系燃料の燃焼ガスの平衡組成については、すでに ジェットエンジンの排ガス中のNO 濃度の解析に用いる ため、JANAF 1)の平衡定数を用いた広範囲な、数値表が 相波 2) によって報告されている。しかしながら、燃焼生 成物の選択に関する検討は、必ずしも充分ではなかった。 著者等は、各種のロケットプロペラントについて理論性 能値,及び,平衡物性値,輸送特性値等を,S. Gordon³⁾ 等の多項係数化した、JANAF熱力学テーブルを主とす る熱力学データを用いて,各種の条件下で計算し,結果 を報告,及び,提供してきた^{4),5),8),7)},。今回,輸送特性 値の推定に関連して、熱力学データの再検討を行った。 石 油系燃料の燃焼生成物については、JP-4/LOX等のガス 発生器燃焼領域での、ガス分析結果等からも、 JANAFの 熱力学データは、考慮すべき燃焼ガス成分が一部欠けて いるのではないかと判断される。また、熱力学データを 調査した結果、従来、JP-4、LOX 等の生成熱につい ても文献によって異なった値が用いられてきた。また。 G. S. Bahn 8)は、炭化水素燃焼生成物について、JANAF 熱力学データは、反応速度を考慮した解析に用いるには、 炭化水素熱分解物に関する熱力学データが不足している 事を指摘し、これらの近似的な熱力学データを与えた。 著者等は、当所において、実験的研究が行なわれている。 JP-4/LOX, JP-4/AIR等について平衡計算値の再 検討が必要であると判断した。 JP-4 等の 組成と生成 熱値の断熱火炎特性値への影響を調べるとともに、燃焼 生成物として,できるだけ多くの化学種を考慮した場合 の平衡組成への影響をみるため、C-H-N-O系化学 種 (156 種) を考慮した G. S. Bahn の近似熱力学データ と、46種を考慮したJANAF熱力学データを用いて平 衡組成を計算し比較するとともに、JP-4/AIRでの16 化学種を考慮した相波の報告との比較も併せて行った。 G. S. Bahn の熱化学近似テーブルは、多項式で近似して 用いた。今回、著者等が行った、多項係数化の精度につ いては、満足すべきものであり、巻末に多項係数ととも に近似の度合を示すグラフを付録とした。

2. 計算方法とパラメタ

断熱火炎温度,及び,平衡組成等の計算方法は、 S. Gordon 等の CEC プログラム 3)に準じた。付録 A に使用した関係式を簡単に示す。平衡組成,及び,断熱火炎温

^{*} 昭和53年4月24日 受付

^{**}角田支所

度等に影響するパラメタは、圧力とJP-4, LOX, AIR 等の反応物質の組成、及び、生成熱に関するものと、燃 焼生成物の熱力学データである。

2-1 JP-4等の組成と生成熱

JP-4等の石油系炭化水素燃料は、多成分からなる混合物のため、表1に示すような組成・生成熱が各種燃焼計算のデータとして用いられてきた。生成熱のこのよう

な差異は、同表に示した発熱量の評価に起因する。表 2 に石油系炭化水素燃料の規格で示す発熱量と同種燃料の 発熱量の文献値の例を記した。

規格では,一定値以上の発熱量を要求しているのみで, 表1,2 に示した発熱量の差異はありうる。

ここでは、JP-4 の組成・生成熱として、 $CH_{1.9423}$ $AHf_{288.15 \cdot K}=-5430 cal/mole を基準とし、表 <math>1$ の他の

表 1.	石油系炭	化水素燃料の	組成と生成熱
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物質名	化学式	ΔHf cal/mole	AHc keal/kg	データ・リース
炭 化 水 素	CH_2	-6060.	* 10393.5	(A)
R P - 1	$CH_{1.953}$	-5900.	* 10343.0	(B)
"	$CH_{1.97}$	-5764.	* 10375.2	(C)
"	$CH_{1.953}$	-5597.	* 10364.7	(D)
炭 化 水 素	CH_2	-8352.	10250.	(E)
JP-4, RP-1	$CH_{1.9423}$	-5430.	10362.5	(F)
JP-5, ASTMA-1	$CH_{1.9185}$	-5300.	10340.2	(F)

注・ 4日 f 値より逆算

データ・リース

- (A) S.F. Sarner; Propellant Chemistry (1966) pp 398, Reinhold pub
- (B) B Siegel他; Energetics of Propellant Chemistry (1964) pp 176.
 John Wiley & Sons Inc
- (C) G. P. Sutton; Rocket Propulsion Elements (1963) pp 209, John Wiley & Sons Inc
- (D) S.S.Penner他ed; The Chemistry of Propellants (1960) pp 68, Pergamon Press
- (E) 相波哲郎;航空用ガスタービン燃焼器における排気制御の研究(II) 燃焼ガスの化学平衡計算とNO 濃度の計算 - (1975) pp 14. 航空宇宙技術研究所資料 TM - 273
- (F) R. A. Svehla 他; NASA-TND-7056 (1973) pp 158

表 2. ジェット燃料の発熱量 [kcal/kg]

J P - 1	J P – 2	J P - 3	JP-4	JP-5	RP-1
*> 1 0 1 7 0.		* >10270.	* >1 0 2 2 0.	* >10170.	
A) 10300.		A) 1 0 2 7 0.	A) 10400.	A) 1 0 2 5 3.	
B) 10280.	B) 10390.	B) 10400.	B) 10390.	B) 1 0 3 0 0.	B) 10380.

注* 規格値

A) … DADIEU 他:Raketentreibstoffe (1968) pp. 543 Springer-Ver Lag

B) S. F. Sarner; Propellant Chemistry (1966) pp. 203 Reinhold Pub

値を採用した場合の断熱火炎温度、平衡特性値等の比較を各プロペラントについて後で論ずる。文献を調査するとLOXの生成熱についても表3に示すようにいくつかの値が用いられてきた。本報告では、LOXの生成熱として、AHf_{90.18K}=-3102 cal/moleを基準とし、他の値を採用した場合との比較も同様に論ずる。

2-2 燃焼生成物の熱力学データ

JP-4/LOX, JP-4/AIRの燃焼生成物は、多種の化学種が考えられる。表 4-1 は、相波が平衡計算に際して考慮した化学種であり、表 4-2 は、S. Gordon³⁾等がJANAF¹⁾熱力学テーブルを基にC-H-N-O系化学種の熱力学データを多項係数で表わしたもので、本報告では比較の基準として採用した。表 4-3 は、G. S. Bahn⁸⁾の近似熱化学テーブルのイオン種を除く、C-H-N-O系化学種である。

との化学種等に関して、B. J. Mcbride⁹⁾等の熱力学 関数計算コード"PAC-1"と同様な方法で多項係数化 を行なった。図-1に多項係数と、各熱力学関数の近似 熱化学テーブルからの偏差の例を示す。

表4-3の化学種の多項係数、及び偏差値のグラフは、 巻末に付録Dとして、図-1と同様な表示でまとめた。 同図に示すように、多項係数は1ケの化学種について14

表 3. LOXの生成熱 cal/male

化学式	∆Hf cal/mole	データ・リース
02	- 2257.	(A)
02	-3180 .	(B)
02	- 3 0 0 2 .	(C)

- (A) G. P. Sutton; Rocket Propulsion Elements (1963) pp. 208, John Wiley & Sons Inc
- (B) S.F. Sarner; Propellant Chemistry (1966) pp. 394. Reinhold Pub
- (C) R. A. Svehla ; NASA TN D-7056 (1973) pp. 158

表 4-1 相波の考慮した化学種

化学種	化学種	化学種
CH ₄	N	0
co	N H ₃	ОН
CO2	NO	02
Н	N O ₂	(A_r)
H 2	N ₂	
H ₂ O	N ₂ O	

表 4 - 2 S. Gordon 等か熟力学データを与えた化学種

化学種	データ・リース	化学種	データ・リース	化学種	データ・リース
C (s)	J3/61	C 2 N2	J3/61	N	J 3 / 61
c	J3 / 61	C_2O	J9/66	N H	J 12 / 65
СН	J12/67	C 3	J12/69	NH ₂	J 12 / 65
C H 2	J6/69	$C_3 O_2$	J6/68	NH ₃	J12/65
C H 2 O	J3/61	C 4	J12/ 69	NO	J 6 / 63
С И з	J6/69	C 5	J12/69	NO ₂	J 9 / 64
C H4	J3 / 61	H	J9/65	N ₂ C	J 9 / 65
C N	J6/69	H CN		N_2H_4	J 6 / 66
CN ₂	J6/66	н со	J3/61	$N_2 O$	J12/65
co	J9/65	H NO	J3/63	$N_2 O_4$	J12/64
C O 2	J9/65	H O 2	J3/64	N ₂	J9/64
C 2	J12/69	H_2	J3/61	0	J 6 / 62
C_2H	J3/67	$H_2O(s)$	L11/65	ОН	J3/63
C_2H_2	J3/61	H ₂ O(e)	L11/65	O ₂	J 9 / 65
C_2H_4	J9/65	H_2O	J3/61	(A_r)	L5/66
C_2N	J3/67	H_2O_2	L2/69		

注: J… JANANF テープル値を多項係数化したもの

L…NASA. Lewis Reseach Carterの数値を多項係数化したものまた、3/61 等は 1961 年 3 月の選定値を示している。

化学種	化学種	化学種	化学種	化学 種	化学種
C (s)	H ₂	$C_2 O_2 H_3$	$C_4 H_4$	C 6 H4	C ₈ H ₁₇
C	$H_2O(1)$	$C_2 H_4 O^{-1}$	C_4H_5	$C_6 O_2 H_4$	$C_8 H_{18}$
C H	H_2O	СН 3 СНО	$C_{4}H_{6}$	C_6H_{5-1}	C ₉ H
C H ₂	H_2O_2	$C_2H_4O_2$	$C_{4}H_{7}$	C_6H_{5-2}	C ₉ H ₂
CH_2O	N	$C_2 O_2 H_4$	$C_4H_7O_4$	C_6H_{6-1}	C_9 H_{18}
C H 3	NH	$C_2 H_5$	$C_{4}H_{8}$	C_6H_{6-2}	C_9 H_{19}
C H 4	NH ₂	C_2H_4OH	C_4H_9	$C_{6} O_{3} H_{6}$	C ₉ H ₂₀
C N	NH ₃	C_2H_6	C_4H_{10}	C 6 H 7	C ₁₀ H
CH_2OH	NO	$C_2 H_5 O H$	C_5 (s)	C 6 H 8	C ₁₀ H ₂
co	NO ₂	$C_2 O_2$	C_5H	$C_6 O_4 H_8$	$C_{12} H_{20} O_{10}$
C O 2	N ₂	C ₃ (s)	C_5H_2	$C_{6}H_{9}$	$C_2 H_4 O^{-2}$
C_2	HCNO	C_3H	C_5H_3	$C_{6}H_{10}$	$HNO_2 - C$
C_2H	$N_2 H_4$	C_3H_2	C_5H_4	$C_6 H_{10}O_5$	$HNO_2 - T$
$C_2 H_2$	N ₂ O	C_3H_3	C_5H_5	$C_6 O_5 H_{10}$	HNO ₃
$C_2 H_4$	N ₂ O ₄	C_3H_4	C_5H_6	$H_{10}O_5C_6$	NO ₃
CH_3OH	О	C_3H_5	C_5H_7	$C_{6}H_{11}$	N ₂ O ₃
$C_2 N_2$	OH	$C_2 H_5 CO$	C_5H_8	$C_{6}H_{12}$	N_2O_5
C ₂ O	02	C_3H_6	C_5H_9	C_6H_{13}	НСООН
C ₃	C_2 (s)	C_2H_6CO	C_5H_{10}	$C_{6}H_{14}$	CH4 COO
$C_3 O_{.2}$	C ₂ HO	C_3H_7	C_5H_{11}	$C_{7}H$	03
C ₄	C 2 HO2	C_3H_6OH	C 5 H 12	$C_7 H_2$	NH_3 (1)
C ₅	$C_2 H_2 O$	C_3H_8	C ₆ (s)	$C_7 H_{14}$	N_2H_2
H	$C_2 H_2 O_2$	$C_3 H_7 OH$	C 6	$C_{7}H_{15}$	$N_2 H_3$
HCN	$C_2 H_3$	C_4 (s)	$C_{6}H$	$C_7 H_{16}$	(A_r)
HCO	$C_2 H_3 O$	C_4 H	$C_{6}H_{2}$	C_8 H	
HNO	CH ₃ CO	$C_4 H_2$	$C_{6}H_{2}$	$C_8 H_2$	
HO ₂	$C_2 H_3 O_2$	C ₄ H ₃	C 6 H 3	C 8 H 16	

表 4 - 3 G. S. Bahn 近似熱化学テーブル化学種

ケから成る。最初の 7 ケは、温度範囲 $1000 \sim 5000 \, \mathrm{K} \, \mathrm{K}$ 適用し、後の 7 ケは、 $300 \sim 1000 \, \mathrm{K} \, \mathrm{K}$ 適用する。 これ らの係数を $A_1 \sim A_2$ で示すと、熱力学関数は以下の式で示される。

$$C_{P}^{\circ}/R = A_{1} + A_{2} \cdot T + A_{3} \cdot T^{2} + A_{4} \cdot T^{3} + A_{5} \cdot T^{4}$$

$$H_{T}^{\circ}/RT = A_{1} + \frac{A_{2}}{2} \cdot T + \frac{A_{3}}{3} \cdot T^{2} + \frac{A_{4}}{4} \cdot T^{3} + \frac{A_{5}}{5} \cdot T^{4} + \frac{A_{5}}{T}$$

$$S_{T}^{0}/R = A_{1} \ln T + A_{2} \cdot T + \frac{A_{3}}{2} \cdot T^{2} + \frac{A_{4}}{3} \cdot T^{3} +$$

$$\frac{A_5}{4} \cdot T^4 + A_7$$

$$- (F_T^0 / RT) = (S_T^0 / R) - (H_T^0 / RT)$$
.....(1)

図-1の偏差値のクラフは,上式で計算した熱力学関数値とG. S. B ahm の熱化学近似テーブル値の偏差を<math>%で示す。

G. S. Bahnの近似熱化学テープルは、若干の化学種について、特に 1000 K以下の温度で比熱等に納得しかねる数値があるが、今回はそのまま用いた。表 4 - 3 に示した化学種の大部分は多原子分子で熱力学関数値は、単原

子分子,2原子分子等のように精密には推定できない。¹⁰⁾ これらの多原子分子の熱力学関数値は、今後とも改訂されていくので、その都度検討が必要である。表 5 は RP - 1/LOXのガス発生器の燃焼生成物のガス分析結果¹¹⁾ の一例であり、表 4 - 1,表 4 - 2 に示されていない化学種が相当数ある。

表4-3と比較すれば、同表には、エチルペンゼンが ないのを除き殆ど全ての化学種が含まれている。

よって,比較対象の熱力学データとしては,適当なものと判断した。

3. 計算結果と検討

JP-4/LOX, JP-4/AIRの両者について,順次論ずる。ロケットプロペラント燃焼ガスの熱物性,及び,理論性能等の計算では,熱力学データに関しては最新の選定値を採用すればよいが,従来の文献値との差異を検

G.S.BAHN

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討しておく事も必要である。

以下, JP-4/LOX, JP-4/AIRの組成, 生成熱値, 及び, 燃焼ガスの熱力学データの差異が, 平衡組成と燃 焼特性値等にどのように影響するかを検討する。

3-1 JP-4/LOX プロペラント 断熱火炎温度:

309 - 5000

断熱火炎状態は、ロケットモータの燃焼室の状態モデルのひとつとして、プロペラントの理論性能計算等に用いられている。燃焼生成物の熱力学データが同一であるならば、JP-4の組成、及び、JP-4、LOXの生成熱値が火炎温度の推定値に影響する。

表6は、表4-2のS. Gordon 等の熱力学データを採用した場合に、JP-4の組成、生成熱により断熱火炎温度がどのようになるかを示している。燃焼圧力は、latmで、この場合平均値に対して、0.5~0.8%の差がある。同様に、LOXの生成熱による差異を みるためのもの

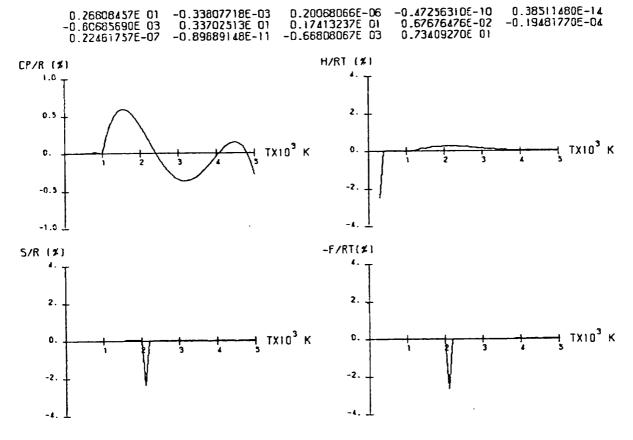


図-1 …AR(G) の熱力学データの多項係数と、表値からの比熱、エンタルビ、 エントロビ、ギブスの自由エネルギの偏差

	O/F	= 0.366	
化学種	分析值重量 (%)	* 気相種等 m ole (%)	** 計算値 mole(%)
СО	3 7. 9 3	3 4.5 6	1 2.3
C O 2	9.96	5. 7 8	2.0
H_2O	0.85	1.20	7. 8
H_2	2.34	2 9.8 5	3 9.9
C H ₄	4.40	7.02	1 3.4
C_2H_2	4.27	4.19	0.5×10 ⁵ 以下
C_2H_4	7.70	7.02	0.001
C_2H_6		_	0.003
C 3 H4	0.41	0.26	0.5×10 ⁵ 以下
C_3H_6	3.96	2.40	"
C 4 H 4	0.21	0.10	"
C_4H_6	1.52	0.72	"
C_4H_8	1.16	0.53	"
C 4 H 8	0.54	0.24	11.
C 6 H 10	1.77	0.54	"
C 6 H 14	0.57	0.17	"
$C_{5}H_{10}$	0.99	0.36	"
C 8 H 16	0.97	0. 2 2	"
C 6 H 6	1.20	0.39	"
C 8 H 10	0.36	0.10	"
C(s)	2.06	4.3 7	4 9.0
RP-1(1)	1 7. 1 4		

表 5. RP・1-LOX ガス発生器 燃焼室ガス分析値の例 ¹¹⁾

- * 液状のRP1(I)を除いた部分についてのモル分率
- ** RP1(I)を除いた O/F で計算した平衡計算値、熱力データは(表4-3)を使用

が表 7 である。酸素の割合が増加するに従い、ブロベラントとしてのエンタルピの差が大きくなり、断熱火炎温度に対する影響も大きくなる。燃焼圧力 1 atmで、平均値に対して、0.3~1.0%の差がある。

表6,表7で最高,最低の断熱火炎温度を示す組成,及び,生成熱を組み合せた場合の断熱火炎温度を表8に示す。すなわち,表1,表3の組成,及び,生成熱を用いると最大で32 K程度,断熱火炎温度間に,差がでてくる。これは,表4-3のG.S.Bahnの熱力学データを用いた場合も同様である。また,熱力学データ,表4-2.及び,表4-3による差は,表7に示したように殆どない。JP-4の組成と生成熱に関しては,H/Cの比が実測に近く,且つ,発熱量のデータがある場合には,これ

を採用し、生成熱値を算出すればよい。 $\mathrm{CH}_{1.9423}$ を CH_2 、 $\mathit{AHf}_{298.15}$ $_{\mathrm{K}}=-5430$ cal/mole を $\mathit{AHf}_{298.15}$ $_{\mathrm{K}}=-8352$ cal/mole としても、断熱火炎温度が、1%以上変わる事はない。

特性排気速度, 比推力等:

ケース3は、ケース2と同様が組み合せで、表4-3の熱力学データを用いたものである。ケース2、3の私み合せは、JP-4、LOX 等の生成熱値に対する最近の推奨値として採用した $\frac{3}{6}$

以下、プロペラントの組成、及び生成熱の典型例として、3つのケースを選び、ロケットプロペラントとしての特性値(特性排気速度、比推力等)に対する影響について述べる。ケース1は、表1の(B)と表3の(B)を組み合

当量比 0.6 0.8 1.0 1.2 1.4 CH_2 $\Delta H f = -6060$ 3 0 4 0. 3 0 8 6. 3 0 9 8. 3 0 7 6. 2 9 4 3. L O X $\Delta H f = -3102$ $CH_{1.953}$ $\Delta H_f = -5900$ 3 0 8 7. 3 1 0 0. 3 0 7 9. 2944. 3 0 4 1. AHf = -3102LOX $CH_{1.97}$ $\Delta Hf = -5764$ 3 0 4 2. 3 0 8 8. 3 1 0 0. 3 0 7 9. 2 9 4 5. LOX $\Delta H f = -3102$ $CH_{1.953}$ $\Delta Hf = -5597$ 2 9 4 6. 3 0 4 3. 3 0 8 9. 3 1 0 1. 3 0 8 1. LOX $\Delta H f = -3102$ CH_2 $\Delta H f = -8352$ 2 9 3 1. 3 0 2 8. 3 0 7 3. 3 0 8 3. 3 0 5 8. LOX $\Delta H f = -3102$ $CH_{1.9423} \Delta Hf = -5430$ 2 9 4 7. 3 0 4 3. 3 0 9 0. 3 1 0 3. 3 0 8 2. LOX $\Delta H f = -3102$

表 6. ジェット燃料/液体酸素の断熱火炎温度 (I) [K] P=1 atm

表 7. ジェット燃料 - 液体酸素の断熱火炎温度(II)〔K〕 P= latm

	混合比	1. 6	1.8	2.4	2. 6	3. 0
CH _{1.9423} LOX	$\Delta H f = -5430.$ $\Delta H f = -2257.$	2757.	3 1 1 3.	3 6 4 3.	3 6 9 3.	3 7 2 1.
CH _{1.9423} LOX	$\Delta H f = -5430.$ $\Delta H f = -3080.$	2 7 3 0.	3 0 8 9.	3 6 2 9.	3 6 8 1.	3 7 1 0.
CH _{1.9423} LOX	$\Delta H f = -5430.$ $\Delta H f = -3102.$	2 7 3 0.	3 0 8 9.	3 6 2 9.	3 6 8 1.	3 7 0 9.
*C H 1,9423 L O X	$\Delta H f = -5430.$ $\Delta H f = -3102.$	2734.	3 0 9 7.	3 6 3 5.	3 6 8 4.	3 7 0 9.

^{*} G. S. Bahn: 熱力学データ使用

表 8. ジェット燃料 - 液体酸素断熱火炎温度 (II) 〔K〕 P= latm

	当量比	0. 6	0. 8	1.0	1. 2	1. 4
CH ₂ LOX	$\Delta H f = -8352$ $\Delta H f = -3102$	2931.	3 0 2 8.	3 0 7 3.	3 0 8 3.	3 0 5 8.
CH _{1.9423} LOX	AHf = -5430 AHf = -2257	2 9 5 8.	3 0 5 2.	3 0 9 7.	3 1 0 9.	3 0 9 0.
CH _{1.593} LOX	AHf = -5900 $AHf = -3080$	2 9 4 5.	3 0 4 1.	3 0 8 7.	3 1 0 0.	3 0 7 9.
CH _{1.9423} LOX	$\Delta H f = -5430$ $\Delta H f = -3102$	2 9 4 7.	3 0 4 3.	3 0 9 0.	3 1 0 3.	3 0 8 2.

せ、表4-2の熱力学データを用いたもので、従来、実験データの整理等に採用してきたものである。ケース2は、表1の(P)表2の(C)を組み合せたもので、表4-2の熱力学データを用いた。

表9は,特性排気速度の例である。燃焼室圧力は,70 atmである。O/Fが小さくなるK従い,ケース1とケース2,3間の差が大きくなる。しかしながら,この差は,O/F=0.3で0.9%であり,ロケットモータの通常の作動領域O/F=2.0~2.3では,0.5%以下である。燃焼生成物の熱力学データによる差はない。

表 10は、比推力の例である。燃焼室圧力は70 atmで、ノズル出口圧力/atm である。同様にO/F が小になるに従い、ケース1とケース2、3間の差が大きくなる。O/Fが0.3で1.6 sec、すなわち、0.9%程度の差がある。ロケットモータの通常の作動領域では、0.5%以下である。燃焼生成物の熱力学データによる差はない。

以下,表11,12,13 にそれぞれ比熱,比熱比,平均 分子量を示す。ほぼ同様な傾向があり、0/F が小さく ならない限り、0.5%以下の差異である。

熱力学データ,表 4-2,表 4-3 による差をはっき りさせるため,定温・定圧の平衡物性等を計算し比較し た。巻末付録 B に燃焼生成物の平均分子量、比熱、比熱 比の比較表を示す。 $O/F = 0.3 \sim 3.0$ 、温度= 500 ~ 6000 K, 圧力= 1 atm、 10 atm、 100 atm である。

同表によると、断熱火炎温度よりも高い温度で、比熱が 10%程度異っている。これは、いくつかの化学種の組成ピーク値の発生温度のずれに起因する。断熱火炎温度以下に温度を限定すれば、約2%の差があるにすぎない。 実験値との比較:

平衡計算値は、ロケットモータのスラストチャンパー で使用する混合比領域について、多数の文献で基準値と して用いられ、実験値の整理に用いられている。

ここでは、ロケットモータのガス発生器で使用する混合比領域での比較を簡単に行う。この領域で平衡計算結果と実測値を比較する事は、炭化水素燃料であるから、特に妥当性に問題もあるが、ここではS. Greenfieldのガス分析結果⁽¹⁾との比較を行った。先に示した表5は、ガス分析結果に相当する状態での平衡計算結果を示しているが、表4-3の熱力学データを用いた結果との間にも差が大きい。また、ガス温度についての比較を行った図-2では、やはり相当程度の差がある。炭化水素燃料では、ガス発生器の長

ケース	プロベラント組成と生成熱	O/F = 0.3	O/F = 0.6	O/F = 1.0	O/F = 2.0	O/F = 3.0
1	$CH_{1,953}$ $\Delta Hf = -5900$. LOX $\Delta Hf = -3080$.	1 0 7 2.	1 2 4 1.	1 3 8 5.	1 7 9 3.	1 7 6 1.
2	$CH_{1.9423}$ $\Delta Hf = -5430.$ LOX $\Delta Hf = -3102.$	1 0 8 2.	1 2 4 8.	1 3 9 2.	1 7 9 6.	1 7 6 2.
3*	* $CH_{1.9423}$ $\Delta Hf = -5430$. LOX $\Delta Hf = -3102$.	1 0 8 2.	1 2 4 8.	1 3 9 2.	1 7 9 6.	1 7 6 2.

表 9. ジェット燃料 ~ 液体酸素の特性排気速度(平衡流を仮定) (m/sec) Pc = 70atm

表 10. ジェット燃料 - 液体酸素の比推力(平衡流, 海面上)(Kg - sec/kg) Pc = 70atm

ケース	プロペラント組成と生成熱	O/F = 0.3	O/F = 0.6	O/F = 1.0	O/F = 2.0	O/F = 3.0
1	$C H_{1.953}$ $\Delta H f = -5930.$ $L O X$ $\Delta H f = -3080.$	1 8 0.7	2 0 8.2	2 2 9.9	2 9 0.9	2 9 7. 3
2	$CH_{1.9423}$ $\Delta Hf = -5430.$ LOX $\Delta Hf = -3102.$	1 1823	2 0 9.3	2 3 0.8	2 9 1.6	2 9 7.4
3*	$CH_{1.9423}$ $\Delta Hf = -5430.$ LOX $\Delta Hf = -3102.$	1 1 8 2 3	2 0 9.3	2 3 0.9	2 9 1.6	2 9 7. 5

^{*} G. S. Bahn 熱力学データ使用

^{*} G. S. Bahn 熱力学データ使用

ケース	プロペラント組成と	生成熱 O/F=0	0.3 $O/F = 0.6$	0/F = 1.0	O/F = 2.0	O/F = 3.0
1		- 5 9 0 0. - 3 0 8 0.	7 2.0 5 7	1.017	0.8324	1.716
2	1.01-0	- 5430. - 3102.	1.996	0.9705	0.8436	1.720
3*	1.0420	- 5 4 3 0. - 3 1 0 2.	3 2.002	0.9768	0.8425	1.721

表 11. ジェット燃料 - 液体酸素,断熱火炎の定圧比熱 〔 cal/mole 〕 Pc=70 atm

表 1 2. ジェット燃料 - 液体酸素, 断熱火炎の比熱比 Pc = 70 atm

ケース	プロペラント組成と生成	O/F = 0.3	O/F = 0.6	O/F = 1.0	O/F = 2.0	O/F = 3.0
1	$CH_{1.953}$ $\Delta Hf = -590$ O_2 $\Delta Hf = -300$	1.125	1.1 6 2	1.238	1.1 7 7	1.1 3 2
2	$CH_{1,9423}$ $\Delta Hf = -543$ O_2 $\Delta Hf = -310$	I —	1.1 6 5	1.243	1.1 7 6	1.1 3 2
3	$CH_{1.9423}$ $\Delta Hf = -543$ O_2 $\Delta Hf = -310$	1 1126	1.1 6 4	1.242	1.1 7 6	1.1 3 2

表13. ジェット燃料-液体酸素,断熱火炎の平均分子量

ケース	プロペラント組成と生成熱	O/F = 0.3	O/F = 0.6	O/F = 1.0	O/F = 2.0	O/F = 3.0
1	$CH_{1.953}$ $\Delta Hf = -5900.$ O_2 $\Delta Hf = -3080.$	2 1.1 2	1 7.7 3	1 5.9 0	2 0.8 2	2 4.7 0
2	$CH_{1.9423}$ $\Delta Hf = -5400.$ O_2 $\Delta Hf = -3102.$		1 7. 6 3	1 5.8 7	2 0.8 5	2 4.7 0
3*	$CH_{1.9423}$ $\Delta Hf = -5400.$ O_2 $\Delta Hf = -3102.$	2 0.9 2	1 7. 6 4	1 5.8 8	2 0.8 5	2 4.7 1

さを長くした場合に排気ガス温度が、上昇したという報告¹³⁾もあり、非平衡性が大きいようである。水素/酸素プロペラントのガス発生器では、平衡計算結果を設計に使用している例もあるが、炭化水素燃料のように分解過程の複雑なものの場合には、適用に問題が多い。

3-2 JP-4/AIR プロペラント

ジェット燃料と空気の燃焼ガスについては、相波の広範囲を平衡計算結果が報告されている。ここでは、表4-1(相波の報告に相当)、表4-2、表4-3の各熱力学データにより、平衡組成、及び、特性値がどのよう

に変わるかを検討する。

断熱火炎温度:

表4-2,表4-3の熱力学データによる断熱火炎温度の差はない。JP-4の生成熱による差は,表14に示すように本計算の範囲内では、4%程度である。

平衡特性值:

定温,定圧下での平衡特性値を表4-2,表4-3の 各熱力学データを用いて計算し比較を行った。当量比 ¢ = 0.6, 1.0, 1.4の3点,温度 500~6000 K で 100K 間隔,圧力 1 atm, 10 atm, 30 atmの3点を選んだ。平

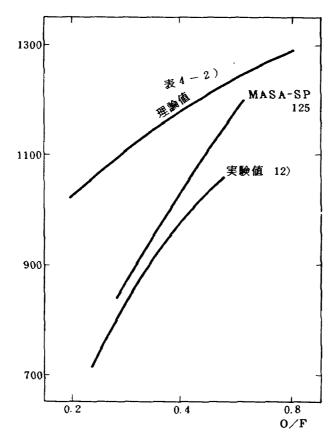


図-2 (JP-4/LOXの燃焼ガス濃度)

表14. ジェット燃料,空気,断熱火炎温度〔K〕

ブロベラント組成と生品	当量比	φ = 0.5	$\phi = 1.0$	$\phi = 2.0$	$\phi = 2.5$	ø = 3.0
C H 1.953 A I R (I)	$\Delta H f = -5900.$ $\Delta H f = -28.2$	1 5 0 8.	2 2 7 4.	1 6 1 9.	1 3 0 4.	1 0 9 0.
CH ₂ AIR (II)	$\Delta H f = -8312.$ $\Delta H f = 0$	1 5 0 0.	2 2 6 1.	1 5 7 5.	1 2 4 9.	1 0 5 4.
CH ₂ AIR (II)	$\Delta H f = -5300.$ $\Delta H f = 0$	1 5 2 3.	2 2 8 7.	1 6 4 6.	1 3 3 5.	1 1 0 3.
C H _{1.9423} A I R (I)	$\Delta H f = -5430.$ $\Delta H f = -28.2$	1511.	2 2 7 7.	1 6 3 0.		
*CH _{1.9423} AIR (I)	$\Delta H f = -5430.$ $\Delta H f = -28.2$	1511.	2 2 7 8.	1 6 2 9.		

AIR(I) ····· N 1.5618 O 0.4196 Ar0.0098 C 0.0030

AIR(II) $\cdots\cdots$ N 1.5618 . O 0.4196

均分子量,比熱,比熱比に対する比較表を巻末付録に示す。同表によると, $\phi=1.4$,T=900 K,P=30 atm の 1 点を除き差は 1 %以内である。

粗成差が小さいため、混合ガスの物性には影響が少ない。

平衡組成の検討:

表4-1(相波),表4-2(S. Gordon),表4-3(G. S. Bahn)の熱力学データを用いた場合の平衡組成を比較する。圧力1atmで,空気加剰の当量比 φ=0.5,及び,量論比と等しい当量比 φ=1.0,燃料過濃の当量比 φ=3.0の各条件で,定温,定圧下での平衡組成を計算し,温度を横軸として,各化学種のモル分率をグラフ化して比較を行う。図3-a,図3-b及び,図3-cは,それぞれ表4-3,表4-2,表4-1の熱力学データによるφ=0.5,圧力1atmでの平衡組成を示している。3つの図を比較することにより,以下の事がわかる。

j) 図3-aと,図3-bを比較すると、モル分率が、 10^{-7} 以下の化学種に差が顕著である。G.S. Balmの熱力学データを用いた場合、表4-2 で考慮していない HNO_2-T , HNO_2-C . O_3 ,HCOOH,HCNO 等が現われる。また、S. Gordon の熱力学データを用いた場合、高温では、表4-3 で考慮していない N_2C , CN_2 等が現われる。他の化学種について、両者の差は小さい。

ii) 図 3-a , 3-b と相波の計算結果(図 3-c)を比較すると,図 3-a , 3-b では, 10^{-5} レベル以上で,高温になると,NH, C_1 (G) 等が生成している。また, 10^{-7} レベルでは,HNO, HCO, H_2O_2 , NH_2 等が生成している。また, 10^{-8} では, HNO_2-C , HNO_2-T , NH_2 , HCN, O_3 , 10^{-9} では,HCOOH, HCNO 等が生成している。

しかし、これらの生成によって、図 3-a、3-bと図 3-cの共通する化学種のモル分率分布の形は、余り影響を受けていない。量論比 $\phi=1.0$ の場合について、同様に比較してみる。図 4-a、4-b 及び、図 4-cは、それぞれ、表 4-3、表 4-2、表 4-1 の各熱力学データによる $\phi=1.0$ 、圧力 1 atmでの、平衡組成を示している。

iii)図4-aと図4-bの平衡組成を比較すると、先の場合と同様にモル分率が 10^{-7} 以下の化学種に差が顕著である。G. S. Bahn の熱力学データを用いた場合、表4-2で考慮していない HNO_2-C 、 HNO_2-T 、 O_3 、HCOOH、HCNO 等が現われ、その濃度レベルは、 $\phi=0.5$ の場合よりも若干高い。

S. Gordon の熱力学データを用いた場合、高温では、

先の場合と同様 KN_2C , CN_2 等が現われる。他の化学種について、差は小さい。

iV) 図 2 と相波の計算結果(図 2')を比較すると、図 2 では、 10^{-5} レベル以上で、高温になると、 $NH.C_1$ (G)、CN等の生成がみられる。また、 10^{-6} レベルでは、 HO_2 、HNO、HCO、CH等の生成、 10^{-7} では、 NH_2 、 H_2O_2 等、また、 10^{-8} では、 NH_2 、 H_2O_2 等、また、 10^{-8} では、HCNO、 CH_2O 等が生成している。

図 2 と図 2 'でも, 共通する化学種のモル分率分布の 形は,ほぼ同様である。表 4-2 ,表 4-3 化基づく平 衡組成の差は,先の $\phi=0.5$ の場合に比較して若干大き くなっているが,存在する化学種は,ほぼ同様である。

図5-a, 5-b及び図5-cは, 燃料過濃の $\phi=3.0$ 圧力1atmでの, 平衡組成を示している。

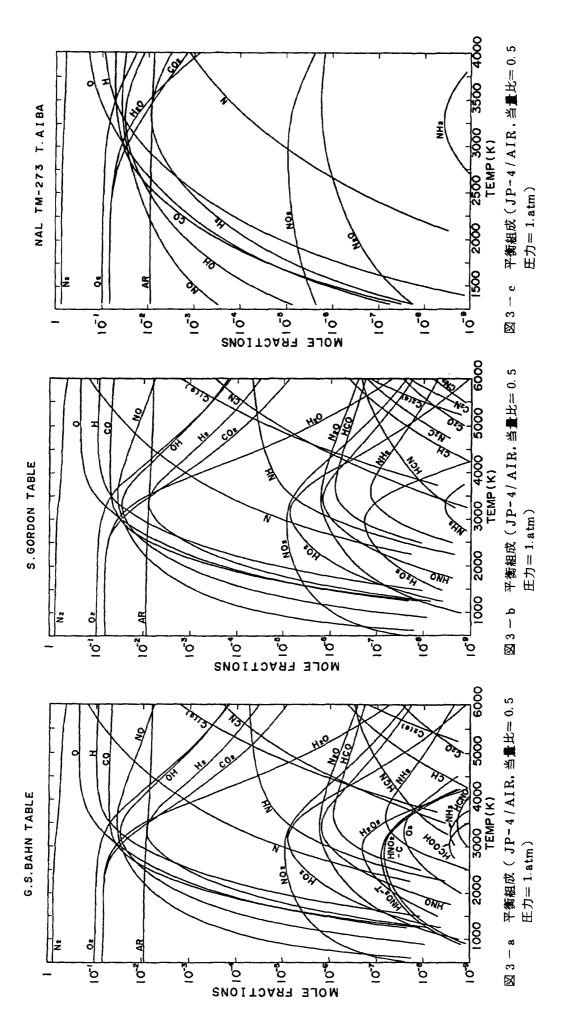
V)図5-b, 5-aのS. Gordon, G. S. Bahnの比較では、 10^{-3} レベルで、固体炭素を $C_1(S)$ とみるか、 $C_2(S)$ とみるかということに相違がみられる。 10^{-5} レベルでは、 C_2H_2 の生成量に差がある。S. Gordon の平衡組成では、 10^{-6} で高温になると、 C_2N が生成している。 10^{-7} では、差が少なく、G. S. Bahnの平衡組成では、 10^{-8} でHCNO が生成する。 10^{-9} では、表4-3 で多数考慮した炭化水素熱分解物の一部、 C_2H_3 、 C_3H_2 、 C_4H 等が生成している。

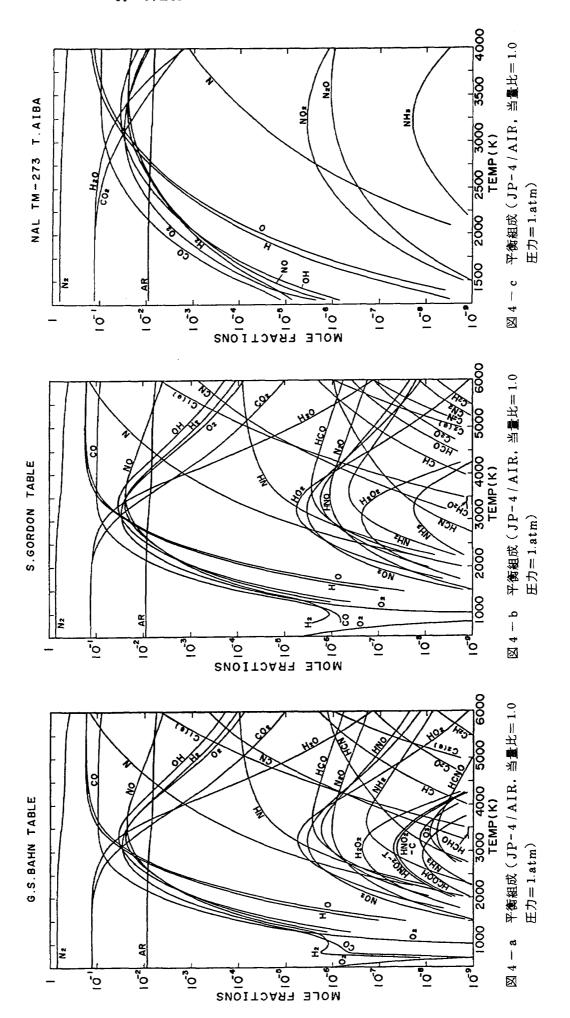
Vi)図5-a,5-bと相波の計算結果(図5-c)の比較から、図5-a,5-bでは、 10^{-3} レベルでのHCN,及び、 C_1 (S)、又は、 C_2 (S)の生成、また、 10^{-4} レベルでのCN等、 10^{-5} レベルでの C_2H_2 、NH、HCO、 10^{-6} レベルでの C_2H 等、 10^{-7} レベルでの CH_3 、 C_2H_4 等々、多種の化学種が生成している。しかし、この $\phi=3.0$ の相波の計算では、 $\phi=0.5$ 、 $\phi=1.0$ と異って、比較的濃度レベルの高い化学種も無視している。

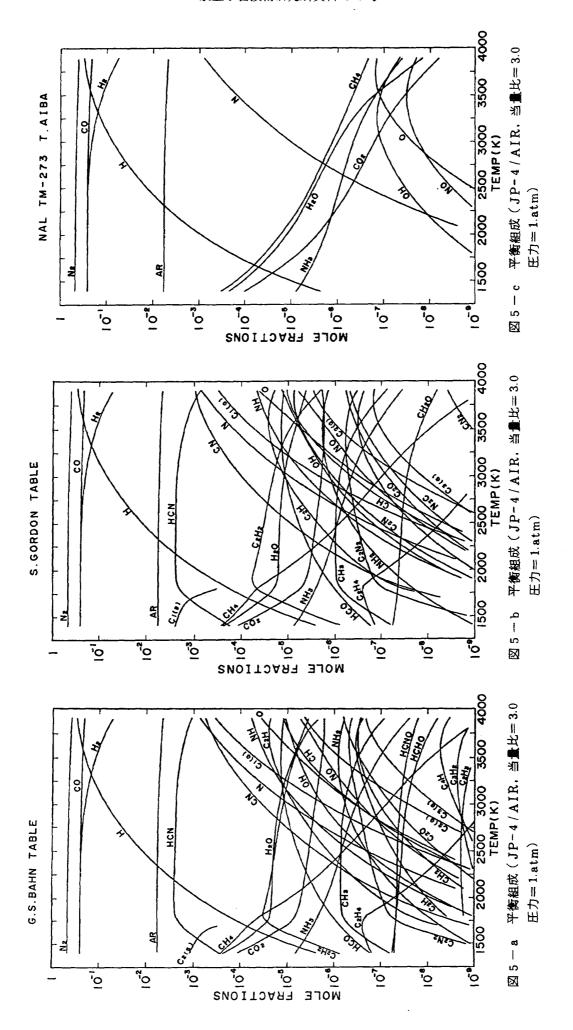
窒素酸化物濃度の推定に当っては、 HO_2 、HCN 等の果たす役割が注目されている。図3-a, 3-b, 図4-a, 4-b, 図5-a, 5-b に示したように HO_2 , HCN 等の濃度は、無視しえない。

これらを無視した相波の平衡組成の使用に当っては、 これらの濃度の推定が必要である。

 10^{-6} レベル以上で、G. S. Bahn と S. Gordon の熱力 学データを用いた平衡組成に比較的大きな差がある化学 種は、 $\phi=3.0$ の C_2 H_2 である。多種の炭化水素熱分解 物を考慮した図 3 の G. S. Bahn の平衡組成では、 C_2 H_2 の濃度が若干低くなり、いくつかの他の炭化水素熱分解 が生成している。以上、当量比 $\phi=0.3$, 1.0 , 3.0 , 圧力 1 atm の典型的な例について比較を行ったが,圧力 が高くなると差は小さくなる。







4. まとめ

JP-4/LOX. JP-4/AIR の平衡計算結果について検討した。

- (i) 断熱火炎温度よりも高温の組成ピーク値のずれがある領域を除くと、燃焼生成物に多種の岸化水素分解生成物を考慮したG.S. Bahn の熱力学データを用いた場合も、S. Gordon の熱力学データを用いた場合も、燃焼生成ガスの平衡物性の差は小さい。
- (ii) 断熱火炎状態の燃焼ガスの平衡物性は,JP-4,LOX の組成・生成熱の差異に基づく変動が若干有り,表4-2,表4-3 の熱力学データに基づく差は無視してよい。ロケット燃料の性能バラメタである特性排気速度では,O/F が小さくなれば差が大となり, $P_c=70$ atm.O/F=0.3 のJP-4/LOX に対しては,10 m/sec 程度の差がでる。これがO/F=1.0 では,特性排気速度の差は7 m/sec で,真空比推力では,1.0 sec の差がでる。量論比近傍では,性能バラメタの差は小さくなる。
- (ii) 大気汚染では、微量生成物が問題になる。JP-4/AIRの燃焼の反応速度論的解析で重要な微量生成物については 10^{-7} 以上の濃度で、表4-2、表4-3の差は殆ど無視できる。
- (V) NAL-TM-273の 相波の広範囲を平衡計算結果は、今回の検討により、空気加剰から量論比近傍での燃焼状態の解析に用いるには、HO₂、NH、HNO 等を追加補正する事、燃料過濃領域で、HCN、CN等を追加補正すべきである事がわかる。

とれらの補正は、相波の表を用いて、上記化学種の平 衡定数から、簡単に、近似的に求める事ができる。

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付録A

多成分系の平衡組成の数値計算では、最近では平衡関係式を解く方法よりも、自由エネルギ最小法による事が多い。ここでは、S. Gordon³⁾ 等がCECコードで用いた 諸式によって、平衡組成の計算方法を簡単に説明する。

平衡の条件

定圧下では、系のG ibbs の自由エネルギが最小である事が化学平衡の条件である。今 n種の化学種から成る系について考える。状態変数として、P・T・ n_j j=1 ~n をとる。ここで n_j はj 種の系の単位質量当りのモル数である。系のG ibbs の自由エネルギg は、 $\mu_j = (\partial g | \partial n_j) T$ 、P・ n_{i+j} で定義される化学ポテンシャルを用い

て、
$$g = \sum_{j=1}^{n} \mu_{j} n_{j}$$
 で示される。また、 n_{j} は次の質

量保存則を満足しなければならない。

$$\sum_{j=1}^{n} a_{ij} n_{j} - b_{i}^{o} = 0 \quad i = 1, \dots, \ell \dots (A-1)$$

上式が自由エネルギgを最小にするに際しての、拘 条件である。よって、最小とすべき関数Gは、

$$G = g + \sum_{i=1}^{\ell} \lambda_i \left(\sum_{j=1}^{n} a_{ij} n_j - b_i^{\circ} \right)$$

ここで、 λ , はラグランシュ乗数である。平衡では、 $\delta G = 0$ 、すなわち、

$$\sum_{j=1}^{n} \left(\mu_j + \sum_{i=1}^{\ell} \lambda_i \ a_{ij} \right) \delta n_j + \sum_{i=1}^{\ell} \left(\sum_{j=1}^{n} a_{ij} n_j - b_i^{\circ} \right)$$

$$\delta \lambda_i = 0$$

ここで、 δn_j と $\delta \lambda_i$ は独立であるから、係数は、零と等しくなければからない。

$$\mu_j + \sum_{i=1}^{\mathcal{L}} \lambda_i \, \alpha_{ij} = 0 \quad j = 1, \dots, n \dots (A-2)$$

δλ; の係数からは、(A-1)式が得られる。

ここで、系を具体的に記述するため、状態方程式、及び、化学ボテンシャル等の諸式を定める。燃焼生成物は、j=1, ……、m なる気相種と、j=m+1, …n なる 凝縮種の混合物からなると考える。気相種を理想気体で近似し、全圧をPとすると、

$$PV = P/\rho = \eta RT$$
 (A-3)

$$n = \sum_{j=1}^{m} n_j \qquad \cdots \qquad (A-4)$$

混合物の分子量Mは、次式で示される。

$$M = \left(\sum_{j=1}^{n} n_{j} M_{j}\right) / \sum_{j=1}^{m} n_{j} \quad \cdots \quad (A-5)$$

化学ポテンシャルルiは,気・凝縮相の理想化によって,

$$\mu_{j} = \begin{cases} \mu_{j}^{o} + RT \ln(n_{j}/n) + RT \ln P & j = 1, \dots, m \\ \mu_{j}^{o} & j = m+1, \dots, n \end{cases}$$
(A-6)

で示される。エンタルピルは、次式で示される。

$$h = \sum_{j=1}^{n} (H_T^o) j \cdot nj \qquad \cdots (A-7)$$

また、エントロピSは、同様に、

$$S = \sum_{j=1}^{n} S_j n_j \qquad \cdots \qquad (A-8)$$

であり、 S_i は、次式で示される。

$$S_{j} = \begin{cases} (S_{T}^{o}) - R \ln(n_{j}/n) - R \ln P & j = 1, \dots, m \\ (S_{T}^{o}) & j = m+1, \dots, n \end{cases}$$

$$(A-9)$$

ここで、 μ_j^o 、 $(H_T^o)_j$ 、 $(S_T^o)_j$ は標準状態での化学ポテンシャル、エンタルビ、エントロビである。

P. Tを定めると、(A-1), 及び(A-2)式で平 衡組成が定まる。よって、

$$P = P_o$$
 (A-10 a)

$$T = T_o$$
 (A-10 b)

なる式が加わる。熱力学的状態は、任意の2つの状態変 数で定まるから、定圧・断熱燃焼では、

$$h = h_0$$
 (A-11a)

$$P = P_o$$
 (A-11b)

定圧・定エントロピ状態では、

$$S = S_o$$
 (A-12 a)

$$P = P_o \qquad \qquad \cdots \cdots (A-12b)$$

なる式を用いる。とれらの連立方程式を解くには、組成に関する非線型式を含むため、繰返し計算が一般に必要である。式の取扱いを簡単化するため、nも独立変数とみかす。Newton-Raphson 法で、初期推定値 n_j 、ラクランジェ乗数 λ_i 、モル数 n、温度 T (必要な場合)に対する修整を行かう。修整項に関するNewton-Raphonの式を得るため、各式を Taylor 級数 で展開して、1次よりも高次の項を無視する。修整変数としては、 $\Delta C n_j(j=1,\dots,m)$ 、 $\Delta n_j(j=m+1,\dots,n)$ 、 $\pi_i=\lambda_i/RT$ 、 $\Delta C n$ Tをとる。熱力学関数の無次元化を行なうと、(A-1)、(A-2)、(A-4)、(A-11a)、(A-12a)等の諸式から、次のNewton-Raphsonの修整項に関する諸式が得られる。

熱力学的状態をどのように指定するかによって、(T,P)、(H,P)、(S,P)により、(A-13)~(A-18)の諸式が組み合せて用いられる。このままでは、多種の化学種を含む系では、大きな連立方程式を解かなければならない。(A-14)式から得られる Alnnj を他の式に代入する事によって、連立方程式の数は、減少できる。すなわち、

定温・定圧の系では、(A-19)、(A-15)、(A-20)式で AL_nT の項を削除した連立方程式を解くことによって修整値が得られる。

定エンタルピ・定圧の系では、(A-19)、(A-15)、(A-20)、及び、(A-21)式から成る連立方程式を解くと、修整値が得られる。

定エントロピ・定圧の系では、(A-19)、(A-15)、(A-20)、及び、(A-22)式が、修整値を得るための連立方程式である。これらの方程式を解くことにより、 π_i 、 Δn_j 、 $\Delta \ell_n n_i$ 、 $\Delta \ell_n T$ 等が得られる。 $\Delta \ell_n n_j$ は、(A-14)からこれらの値を用いる事によって得られる。すなわち、新しい推定値は、

··········· (A-22)

$$\ell_n n_j^{(i+1)} = \ell_n n_j^{(i)} + \lambda^{(i)} (\mathcal{A}\ell_n n_j)^{(i)} (j=1,\dots,m)$$
 $n_j^{(i+1)} = n_j^{(i)} + \lambda^{(i)} (\mathcal{A}n_j)^{(i)} (j=m+1,\dots,n)$
 $\ell_n n^{(i+1)} = \ell_n n^{(i)} + \lambda^{(i)} (\mathcal{A}\ell_n n)^{(i)}$
 $\ell_n T^{(i+1)} = \ell_n T^{(i)} + \lambda^{(i)} (\mathcal{A}\ell_n T)^{(i)}$
で与えられる。ここで、 $\lambda^{(i)}$ は、収束を早めるための係

で与えられる。ことで、 $\lambda^{(i)}$ は、収束を早めるための係数である。

繰返し計算は、今回は次の条件を満足するまで行った。

$$\frac{n_{j} | \Delta \ell_{n} n_{j} |}{\sum_{j=1}^{m} n_{j}} \leq 0.5 \times 10^{-9} \quad j = 1, \dots, m$$

$$\frac{|\Delta n_{j}|}{\sum_{j=1}^{m} n_{j}} \leq 0.5 \times 10^{-9} \quad j = m+1, \dots, n$$

$$| \Delta \mathcal{L}_n n | \leq 0.5 \times 10^{-9}$$

······ (A- 24)

基本的には、以上の諸式で、定圧・定温の平衡組成、 及び、定圧・定エンタルビ(断熱火炎)での平衡組成を 計算し、比推力等の計算では、定圧・定エントロビの式 を用いている。

以上

記 号

- aij 量論係数 (kg-atom)i/(kg-mole)j
- b_i^o 反応物質 kg 当りの元素 i の kg-atom (kg-atom)/kg
- $(C_p^o)_j$ 種jの標準状態での定圧比熱

 $J/(kg-mole)j\cdot K$

$$(\mathit{H}_{T}^{o})_{j}$$
 " $\mathtt{I} \mathtt{V} \mathtt{S} \mathtt{N} \mathtt{C}$

 $J/(kg-mole)_j$

- h 混合物のエンタルピ J/kg
- h。 反応物質のエンタルピ J/kg
- n 混合物のモル数 kg-m ole/kg
- nj 混合物 kg 当りの種jの kg-mole 数 (kg-mole)j ∕kg
- P 圧力 atm
- S_j 種jのエントロピ $J/(kg-mole)_j K$
- $(S_T^o)_j$ 種 $_J$ に対する標準状態のエントロピ $_J$ / $(kg-mole)_j K$
 - S 混合物のエントロピ $J/kg \cdot K$
 - So 反応物質中のエントロピ J/kg·K
- T 温度 K
- $\lambda^{(i)}$ 収束係数
- μ_j 種jの化学ポテンシャル $J/(kg-mole)_j$
- μ_i^o " 標準状態の化学ポテンシャル

 $J/(kg-mole)_i$

- $\pi_i = -\lambda_i/RT$. 元素 i に対するラグランジェ乗数
- ρ 混合物の密度 kg/m³

付録 - B -

G. S. Bahn, S. Gordon の熱力学データを使用した場合の, JP-4 / LOX燃焼生成物の定温・定圧下における平均分子量, 比熱, 比熱比の比較

Colon	JP-4/LOX	0/	F= 1.8	ATH=		IS OVER T	HAN ONE PERCI		ME3 -2:	
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1000			19.844							0.0846
1866		19,843	19.843	0	0.4977	0.4985	-0.1607	1,2520	1,2514	0.0479
2000. 11.84 1.948 0. 0.518 0.186 -0.186 1.286 1.282 1.282 1.282 0.086 2.086 2.086 2.086 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.286 1.							-0.1813 -0.1794			0.0479
2400. 18.748 14.748 0. 0. 0.4444 1.0777 1.2095 1.2091 0.018 2400. 18.719 14.7173 0.0093 1.2092 1.2093 1.2091 1.2091 1.2091 1.2091 2400. 18.719 14.7173 0.0093 1.2092 1.2093 1.2091 1.2091 1.2091 1.2091 2400. 18.719 14.7173 0.0093 1.2092 1.2093 1.2091 1.2091 1.2091 1.2091 2400. 18.719 14.7173 0.0093 1.2093 1.2093 1.2091 1.2091 1.2091 1.2091 2400. 18.719 1.2091 0.0093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093 1.2093				0.	0.5182	0.5190	-0.1544	1.2431	1.2427	0.0822
200. 19.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 10.00 1	2400.	19.749	19.749							0.0244
3000. 14.773 14.773 0.0083 1.7287 1.7288 0.0984 1.1397 1.3989 1.008 3000. 15.038 15.040 0.0183 4.2446 4.4281 0.0272 1.1328 1.1328 1.1328 0.0083 15.038 15.040 0.0183 4.2446 4.4281 0.0817 1.1427 1.1427 1.1426 6.008 3000. 15.038 15.040 0.00183 4.2446 4.4281 0.0817 1.1427 1.1428 6.008 3000. 15.038 15.040 0.00183 4.2446 4.4281 0.0817 1.1427 1.1428 6.008 3000. 15.038 15.040 0.00183 4.2446 4.4281 0.0817 1.1427 1.1428 6.008 3000. 15.040 15.040 0.0083 4.2446 4.4281 0.0817 1.1427 1.1428 6.008 3000. 15.040 15.040 0.0083 4.1324 4.1324 0.0817 1.1428 1.1428 1.1038 6.008 4000. 15.041 1.000 0.0083 0.1324 0.0818 1.1288 1.1291 0.0084 4000. 15.041 1.000 0.0083 0.0084 0.0086 1.1488 1.1291 0.0084 4000. 15.041 1.1428 1.1484 1.1484 0.00 0.0083 0.0096 1.1488 1.1319 0.0084 4000. 15.041 1.1428 1.1428 0.00 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 4000. 15.041 1.1428 1.1428 0.00 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 3000. 15.041 1.1428 1.1428 0.00 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 1.1319 0.0096 0.0084 0.0089 0.0096 1.1488 0.0089 0.0089 0.0096 0.0096 1.1488 0.0089 0.0089 0.0096 0.0096 1.1488 0.0089 0.0089 0.0096 0.0096 0.0089 0.0089 0.0096 0.0089 0.0089 0.0096 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0.0089 0						0.8156	-0.0368	1.1815	1.1814	0.0085
300. 1, 14.85 1, 13.86 0, -0.018	3000.	18.772	18,773	-0.0053						0. -0.0088
\$000. 15.083 55.061 -0.0133 4.2946 4.2841 -0.0877 1.1427 1.1427 1.1428 0.003 \$000. 15.070 13.707 -0.0033 4.2946 4.1328 4.1526 1.1526 1.1526 1.1526 1.1526 0.008 \$000. 15.070 13.707 -0.0038 4.1328 4.1526 0.032 1.2028 1.2028 0.008 \$000. 15.070 13.707 -0.0084 1.7350 1.7350 1.7350 1.2360 1.2361 0.008 \$000. 11.335 11.335 0.0 0.0841 1.7350 1.7350 1.3361 1.3381 1.3190 0.008 \$000. 11.335 11.335 0.0 0.0844 1.7350 0.0851 1.3381 1.3190 0.0091 \$000. 11.335 11.335 0.0 0.8441 0.7462 0.0102 1.3381 1.3190 0.0091 \$000. 11.350 11.350 0.0 0.8441 0.7462 0.0102 1.3381 1.3190 0.0091 \$000. 11.350 11.355 0.0 0.8541 0.7462 0.0762 1.3381 1.3190 0.0091 \$000. 11.350 11.355 0.0 0.8541 0.7462 0.0762 1.3381 1.3190 0.0091 \$000. 11.350 11.355 0.0 0.8541 0.7462 0.0762 1.3381 1.3190 0.0091 \$000. 11.350 11.355 0.0 0.8541 0.7464 0.0552 1.2925 1.2926 0.0091 \$000. 11.350 11.355 0.0 0.8541 0.7464 0.0552 1.2925 1.2926 0.0691 \$000. 25.435 22.459 0.0.0930 0.4455 0.4500 0.0091 1.2925 1.2926 0.0691 \$000. 25.435 22.459 0.0 0.9932 0.4657 0.7503 1.2925 1.1489 1.1290 0.0190 \$1200. 25.435 22.459 0.0 0.7227 0.7723 1.2925 1.1489 1.1292 0.0190 \$1200. 1.1444 0.0 0.0000 0.7714 0.0 0.7014 0.1338 1.1292 0.1292 0.0000 \$1200. 1.1444 0.0 0.0000 0.7714 0.0 0.7014 0.1338 1.1292 0.0 0.0000 \$1200. 1.1444 0.0 0.0000 0.7714 0.0 0.7014 0.1338 1.1292 0.0 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.00000 0.00000 0.0000 0.00000 0.0000 0.00000 0.00000 0.0000 0.00000 0.00000 0.							0.0757	1.1828	1.1323	0.
18-00 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-70 13-7	3690.	15.038	15.040	-0.0133		4.2881	-0.0617	1.1427		0.0088
## 400						4.1415_		1.1565	_1.1564	0.0086
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### 480. 11.339 11.337 0. 0.884 0.4853 0.0504 1.3187 1.3180 0.001						1.7304	0.0347	1.2360	1.2361	-0.0081
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ARDD	3690.	19.296	19.297	-0.0052	0.9507	0.9501	0.0631	1.1800	1.1800	n.
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5440. 13.883 13.882 0.0072 2.2295 2.2828 -0.1256 1.2170 1.2177 0.0164 5600. 13.361 0.0075 2.0806 2.0844 -0.1682 1.2315 1.2177 0.0164 600. 30.127 30.132 -0.0166 0.5942 0.5960 -0.3029 1.1627 1.1618 0.0774 800. 26.213 26.235 -0.0839 1.8636 1.8411 1.2073 1.1182 1.1194 -0.1073 1000. 18.796 18.814 -0.0958 1.3114 1.3432 -2.4249 1.1720 1.1790 0.0939 1200. 18.429 18.425 0. 0.5197 -0.1156 1.2645 1.2645 0.0297 1400. 18.425 18.425 0. 0.5071 0.5079 -0.1578 1.2702 1.2697 0.0394 1800. 18.423 18.425 0. 0.5074 0.5165 -0.1773 1.2700 1.2697 0.0394 1800.					2.3410			1.1943	1.1943	0.
13.362 13.361 0.0775 2.0806 2.0841 -r.1682 1.2315 1.2311 0.0325	5490.	13.883	13.882	0.0072	2.2295	2.2323	-0.1256	1.2179		0.0164
800. 30.127 30.132 -0.0166 0.5942 0.5960 -0.3029 1.1627 1.1618 0.0774 800. 26.213 26.235 -0.0839 1.8636 1.8411 1.2073 = 1.1182 1.1194 -0.1073 1000. 18.796 18.814 -0.0958 1.3114 1.3432 -2.4249 = 1.1182 1.1194 -0.1073 1200. 18.429 18.429 0. 0.5191 0.5197 -0.1578 1.2645 1.2642 0.0237 1430. 18.425 18.425 0. 0.5107 0.5079 -0.1578 1.2702 1.2697 0.0334 1690. 18.425 18.425 0. 0.5171 0.5079 -0.1578 1.2702 1.2694 0.0472 18.00. 18.425 18.425 0. 0.5174 0.5187 -0.1578 1.2700 1.2694 0.0472 18.00. 18.425 18.425 0. 0.5174 0.5187 -0.1578 1.2700 1.2694 0.0472 18.00. 18.425 18.425 0. 0.5149 0.5157 -0.1554 1.2606 1.2655 0.0395 20.00. 18.416 18.416 0. 0.5341 0.5348 -0.1311 1.2571 1.2567 0.0338 20.00. 18.436 18.344 0. 0.5783 0.5789 -0.1038 1.2409 1.2406 0.0242 2400. 18.334 18.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2189 0.0082 2600. 18.202 18.202 0. 0.8457 0.8450 -0.0355 1.1897 1.1896 0.0084 2800. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1857 1.1866 0.0086 3000. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1897 1.1986 0.0086 3000. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1897 1.1986 0.0086 3000. 14.380 1.4380 0. 4.0542 4.0549 -0.0641 1.1393 1.1393 0. 3690 13.212 13.212 0. 3.9913 3.9646 -0.0833 1.1594 1.1595 0.0086 4000. 12.327 12.326 0.0081 3.2516 3.2533 -0.0532 1.1864 1.1396 0. 3890 13.212 13.212 0. 3.9913 3.9646 -0.0833 1.1594 1.1595 0.0086 4000. 11.397 11.746 0.0085 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.746 0.0085 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.746 0.0085 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.746 0.0085 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.396 0.0086 1.719 11.191 0.0089 1.2021 1.2613 0.0654 1.2793 1.2994 -0.0078 4800. 11.171 11.071 0.0089 1.2021 1.2613 0.0654 1.2793 1.2994 -0.0078 4800. 11.171 11.071 0.0089 1.2021 1.2613 0.0654 1.2793 1.2994 -0.0078 4800. 11.171 11.071 0.0089 1.2021 1.2613 0.0654 1.2793 1.2994 -0.0078 4800. 11.071 11.071 0.0089 1.2021 1.2613 0.0654 1.2793 1.2994 -0.0078 4800. 11.071 11.071 0.0089 1.2021 1.2613 0.0654 1.2793 1.2399 1.2021 1.3093 0.0078 4.0008 1.2021 1.3020 1.3020 1.3020 1.3020 1	5400.	13.362	13.361	0.0075	2.0806	2.0841	-n.1682			0.0325
800. 26.213 26.235 -0.0839 1.8636 1.8411 1.2073 = 1.182 1.194 -0.1073 1000. 18.796 18.814 -0.0958 1.3114 1.3432 -2.4249 = 1.3720 1.1709 0.0959 1200. 18.429 18.429 0. 0.5191 0.5197 -0.1156 1.2645 1.2642 0.0237 1430. 18.425 18.425 0. 0.5191 0.5197 -0.1156 1.2645 1.2642 0.0327 1430. 18.425 18.425 0. 0.5076 0.5078 -0.1773 1.2700 1.2697 0.0394 1600. 18.425 18.425 0. 0.5076 0.5085 -0.1773 1.2700 1.2697 0.0394 1800. 18.425 18.425 0. 0.5149 0.5157 -0.1554 1.2600 1.2655 0.0395 2000. 18.423 18.423 0. 0.5149 0.5157 -0.1554 1.2600 1.2655 0.0395 2000. 18.416 18.416 0. 0.5541 0.5348 -0.1311 1.2571 1.2567 0.0318 22400. 18.394 18.394 0. 0.5783 0.5789 -0.1031 1.2571 1.2567 0.0318 2400. 18.354 18.394 0. 0.5783 0.5789 -0.1031 1.2571 1.2567 0.0318 2400. 18.202 18.202 0. 0.6707 0.6711 -0.0596 1.2170 1.2189 0.0082 2400. 18.202 18.202 0. 0.6847 0.8460 -0.0355 1.1897 1.1896 0.0084 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1654 0.0086 3000. 17.945 17.475 0. 1.6731 1.6725 0.0356 1.1483 1.1483 0. 3290 16.717 16.717 0. 2.4667 0.0486 1.1396 1.1396 0.3290 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.393 1.1393 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3490. 13.212 13.212 0. 3.9913 3.9646 -0.0833 1.1596 1.1966 0. 4200. 11.377 11.746 0.0085 2.3992 0. 0.0081 1.1967 1.1966 0. 4200. 11.747 11.746 0.0085 2.3992 0. 0.0083 1.1596 1.196 0. 4200. 11.747 11.746 0.0085 2.3992 0. 0.0083 1.1596 1.1986 0. 4200. 11.747 11.746 0.0085 2.3992 0. 0.0083 1.1596 1.1986 0. 4200. 11.397 11.396 0.0088 1.716 1.7108 0.0064 1.1396 1.1396 0. 4200. 11.747 11.746 0.0085 2.3992 0. 0. 0.0083 1.1596 1.1996 0. 0.0886 0. 0.0088 1.716 1.716 1.7108 0.0064 1.1396 1.1396 0. 0. 0.0886 0. 0.0088 1.716 1.1708 0.0088 1.716 1.1786 0. 0.0088 1.716 1.1796 0. 0.0088 1.716 1.1796 0. 0.0088 1.7179 1.1396 0.0088 1.716 1.7108 0.0064 1.1397 1.1397 0.0088 1.716 1.1796 0. 0.0088 1.7179 1.1396 0.0088 1.716 1.1798 0.0088 1.716 1.1798 0.0088 1.716 1.1798 0.0088 1.7179 1.1399 0.0088 1.716 1.1798 0.0088 1.7179 1.1399 0.0088 1.716 1.1798 0.0088 1.7179 1.1399 0.0088 1.716 1.1	4									
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1200. 18.429 18.429 0. 0.5191 0.5197 -0.1156 1.2645 1.2642 0.0237 1400. 18.425 18.425 0. 0.5071 0.5079 -0.1578 1.2702 1.2697 0.0394 1600. 18.425 18.425 0. 0.5071 0.5076 0.5085 -0.1778 1.2702 1.2697 0.0394 1600. 18.427 18.423 0. 0.5149 0.5157 -0.1554 1.2660 1.2655 0.0395 2000. 18.426 18.426 0. 0.5341 0.5348 -0.1311 1.2571 1.2567 0.0318 2200. 18.394 18.394 0. 0.5341 0.5348 -0.1311 1.2571 1.2567 0.0318 2200. 18.394 18.394 0. 0.5783 0.5789 -0.1038 1.2409 1.2406 0.0242 2400. 18.334 18.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2169 0.0082 2400. 18.202 18.202 0. 0.8457 0.8460 -0.0355 1.1897 1.1896 0.0084 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1654 0.0086 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1654 0.0086 2800. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1483 1.1483 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3490. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1966 0. 3890. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1966 0. 4200. 17.747 1.746 0.0085 2.3952 0. 0.0641 1.1464 1.1464 0. 4400. 11.397 11.396 0.0088 1.716 1.7108 0.0467 1.2089 1.2089 0.0078 4000. 11.397 11.396 0.0088 1.716 1.7108 0.0467 1.2089 1.2099 1.2099 1.0089 1.0089 1.2099 1.0089 1.0099 1.0089 1.0089 1.0089 1.0099 1.0089 1.0099 1.0089 1.0099 1.0089 1.0099 1.0089 1.0099 1.0089 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099 1.0099	1000.	18.796	18.814	-0.0958	1.3114	1.3432	-2.4249 •	1.1720	1.1709	n.0989
1600. 18.425 18.425 0. 0.5076 0.5085 -0.1773 1.2700 1.2694 0.0472 1800. 18.423 18.423 0. 0.5149 0.5157 -0.1554 1.2660 1.2655 0.0395 2000. 18.416 18.416 0. 0.5341 0.5348 -0.1311 1.2571 1.2577 0.0338 2200. 18.394 18.394 0. 0.5783 0.5789 -0.1038 1.2409 1.2406 0.0242 2400. 18.334 18.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2169 0.0082 2400. 18.202 18.202 0. 0.6857 0.8460 -0.0355 1.1897 1.1896 0.0084 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1654 0.0086 2800. 17.941 17.941 0. 1.547 1.1547 0. 1.6725 0.0359 1.1483 1.1483 0. 20086 0. 17.941 17.941 0. 1.6731 1.6725 0.0359 1.1483 1.1483 0. 20086 0. 2009 0. 24679 2.4667 0.0486 1.1396 1.1396 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3690. 14.380 14.380 0. 4.350 0. 4.552 4.0588 -0.0641 1.1464 1.1464 0. 3800. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1996 0. 3900. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1996 0. 4200. 11.747 11.746 0.0085 2.3952 0. 9.0641 1.1464 1.1684 0. 4200. 11.747 11.746 0.0085 2.3952 0. 9.0641 1.1464 1.1684 0. 4200. 11.747 11.746 0.0085 2.3952 0. 9.0641 1.1796 1.1786 0. 4400. 11.397 11.396 0.0088 1.716 1.7108 0.0467 1.2390 1.2391 -0.0086 4200. 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2084 1.2048 0. 4400. 11.397 11.396 0.0088 1.716 1.7108 0.0467 1.2390 1.2391 -0.0081 4000. 11.192 11.191 0.0088 1.716 1.7108 0.0467 1.2390 1.2391 -0.0078 4000. 11.071 11.071 0. 0.0989 1.2621 1.2613 0.0634 1.2793 1.2794 -0.0078 4000. 11.071 11.071 0. 0.9896 0.08578 0.9859 -0.0502 1.3192 1.3193 0.0074 0.0078 5000 10.999 10.998 0.0091 0.8578 0.8579 -0.01017 1.3476 1.3500 0.0444 0.0085 0.0990 0.0502 1.3192 1.3193 0.0074 0.0088 0.0091 1.0991 10.991 0.0091 0.8578 0.8579 -0.01017 1.3506 1.3500 0.0444 0.0085 0.0991 10.991 10.991 0.0088 0.0091 0.8839 -0.2381 1.3598 1.3598 0.0044								1.2645	1.2642	0.0237
1800. 18.423 18.423 0. 0.5149 0.5157 -0.1554 1.2660 1.2655 0.0395 2000. 18.416 18.416 0. 0.5341 0.5348 -0.1311 1.2571 1.2567 0.0318 2000. 18.394 18.394 0. 0.5783 0.5789 -0.1038 1.2409 1.2406 0.0318 2400. 18.334 18.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2169 0.0082 2400. 18.202 18.202 0. 0.68460 -0.0355 1.1897 1.1896 0.0082 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1655 1.1655 0.0084 2800. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1463 1.1463 0.0084 2800. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1463 1.1463 0. 0.0084 2800. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3690. 14.380 14.380 0. 4.0542 4.0568 -0.0641 1.1464 1.1664 0. 3990. 13.212 13.212 0. 3.9913 3.9066 -0.0833 1.1596 1.1596 0. 3990. 13.212 13.212 0. 3.9913 3.9066 -0.0833 1.1596 1.1596 0. 4200. 17.747 11.746 0.0085 2.3952 0. 0.0359 1.1746 1.1786 0. 4200. 17.747 11.746 0.0085 2.3952 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.396 0.0088 1.716 1.716 1.7108 0.0467 1.2390 1.2391 -0.0081 4000. 11.192 11.191 0.0088 1.716 1.7108 0.0467 1.2390 1.2391 -0.0081 4000. 11.071 11.071 0. 0.0989 1.2621 1.2613 0.0634 1.2793 1.2994 0.0078 4000. 11.071 11.071 0. 0.0989 1.2621 1.2613 0.0634 1.2793 1.2391 -0.0081 5000. 10.999 17.998 0.0091 0.8578 0.8579 -0.0101 1.3506 1.3500 0.0444 0.0985 10.991 10.991 0.0996 0.08578 0.8579 -0.0101 1.3506 1.3500 0.0444 0.0981 10.991 10.991 0.0881 0.8839 -0.2381 1.3598 1.3598 1.3598 0.0758	1600.	18,425	18.425	n.	0.5076	0.5085	-0.1773			0.0394
2200. 18.394 18.394 0. 0.5783 0.5789 -0.1036 1.2400 1.2406 0.0242 2400. 18.334 18.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2169 0.0082 2600. 18.202 18.202 0. 0.8457 0.8440 -0.0355 1.1897 1.1897 0.0082 2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.6751 1.6755 1.1483 1.1483 0.0086 300. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1483 1.1483 0. 3290. 16.717 16.717 0. 2.4679 2.4667 0.0486 1.1396 1.1393 0. 3490. 15.638 15.639 -0.0064 3.4157 0. 1.1393 0. 0. 3690. 14.380 0. 3.9513 3.9646 -0.0641 1.1464 1.1464 0. 4000. 17.327 12.326 0.0081 3.2516 3.2533 -0.0523 1.1786 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-0.1554</td> <td>1.2660</td> <td>1.2655</td> <td>0.0395</td>							-0.1554	1.2660	1.2655	0.0395
2600. 18.03 16.334 0. 0.6707 0.6711 -0.0596 1.2170 1.2169 0.0082 2600. 18.202 18.202 0. 0.8457 0.8460 -0.0355 1.1897 1.1896 0.0084 2830. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1655 1.1654 0.0086 2700. 16.717 16.717 0. 1.6731 1.6725 0.0359 1.1483 1.1483 1.1483 0. 2700. 16.717 16.717 0. 2.4679 2.4667 0.0486 1.1396 1.1396 0. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 2700. 27	2200.	18.394	18.394					1.2409	1.2406	0.0318
2800. 17.941 17.941 0. 1.1547 1.1547 0. 1.1655 1.1654 0.0086 3000. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1483 1.1483 0. 3200. 16.717 16.717 0. 2.4679 2.4667 0.0486 1.1396 1.1396 1.1396 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3590. 14.380 14.380 0. 4.0542 4.0568 -0.0641 1.1464 1.1464 0. 3590. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1595 0.0086 4000. 12.327 12.326 0.0081 3.2516 3.2533 -0.0523 1.1786 1.1786 0. 4200. 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2086 0. 4400. 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0084 4400. 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0086 4500. 11.071 11.071 0. 0.0989 1.2621 1.2613 0.0634 1.2793 1.2794 0.0078 4500. 11.071 11.071 0. 0.9965 0.9960 0.0502 1.3192 1.3193 70.0078 4500. 10.999 17.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3504 0.0448 5400. 10.991 10.9950 0.0991 0.8578 0.8579 -0.0117 1.3506 1.3500 0.0444			18.334		0.6707	0.6711	-0.0596	1.2170	1.2169	0.0082
3000. 17.475 17.475 0. 1.6731 1.6725 0.0359 1.1483 1.1483 0. 3290. 16.717 16.717 0. 2.4679 2.4667 0.0486 1.1396 1.1396 0. 3490. 15.638 15.639 -0.0064 3.4157 3.4157 0. 1.1393 1.1393 0. 3690. 14.380 14.380 0. 4.0542 4.0568 -0.0641 1.1464 1.1464 1. 3890. 3890. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1596 0. 4000. 12.327 12.326 0.0081 3.2516 3.2533 -0.0583 1.1786 1.1786 0. 4200. 11.747 11.746 0.0855 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2048 0. 4400. 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2091 -0.0081 4600. 11.192 11.191 0.0089 1.2021 1.2613 0.0634 1.2793 1.2794 -0.0078 4800. 11.071 11.071 0. 0.9965 0.9960 0.0502 1.3192 1.3193 7.00076 5000. 10.999 10.998 0.0091 0.8578 0.8579 -0.0117 1.3506 1.3500 0.0484 5000 10.991 10.998 0.0091 0.8578 0.8579 -0.0117 1.3506 1.3500 0.0484 5000 10.991 10.991 0.0950 0.0818 0.8899 -0.2381 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 1.3598 0.0758										0.0084 0.0086
3490. 15.638 15.639 -0.0064 3.4157 8.4157 0. 1.1393 1.1393 0. 3690. 14.380 14.380 0. 4.0542 4.0568 -0.0641 1.1464 1.1664 0. 3690. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1595 0.0086 4000. 12.327 12.326 0.0081 3.2516 3.2533 -0.9523 1.1786 1.1786 0. 4200. 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0084 4000. 11.192 11.191 0.0088 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0084 4000. 11.192 11.191 0.0089 1.2021 1.2013 0.0034 1.2793 1.2994 0.0078 4800. 11.071 11.071 0. 0.0965 0.0965 0.0960 0.0502 1.3192 1.3193 -0.0078 5000. 10.999 17.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0188 5000 10.950 10.950 10.950 0.08578 0.8579 -0.0117 1.3506 1.3500 0.0444 5400. 10.951 10.951 0.0950 0.0818 0.8889 -0.7381 1.3198 1.3198 1.3188 0.0758	3000.	17.475	17.475	0 •-	1.6731	1.6725	0.0359	1.1483	1.1483	0.
3690. 14.380 14.380 0. 4.0542 4.0568 -0.0641 1.1464 1.1664 0. 38900. 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1595 0.0866 4000. 12.327 12.326 0.086 3.2516 3.2533 -0.9523 1.1786 1.1595 0.0866 4200. 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2048 1.2048 0. 4400. 11.397 11.396 0.0888 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0814 4600. 11.192 11.191 0.0089 1.2021 1.2613 0.0634 1.2793 1.2794 -0.0078 4800. 11.071 11.071 0. 0.089 1.2021 1.2613 0.0654 1.2793 1.2794 -0.0078 4800. 11.071 11.071 0. 0.9965 0.9960 0.0502 1.3192 1.3193 -0.0076 5000. 10.999 10.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5200. 10.950 10.950 0.0950 0.08178 0.8839 -0.2381 1.3198 1.3500 0.0444									1.1396	0.
3890 13.212 13.212 0. 3.9613 3.9646 -0.0833 1.1596 1.1595 0.0086 4000 12.327 12.326 0.0081 3.2516 3.2533 -0.0523 1.1786 1.1786 0. 4200 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2048 1.2048 0. 4400 11.397 11.396 0.0088 1.7116 1.7108 0.0467 1.2390 1.2391 -0.0081 400 11.192 11.191 0.0089 1.2021 1.2613 0.0467 1.2390 1.2391 -0.0081 4800 11.192 11.191 0.0089 1.2021 1.2613 0.0634 1.2793 1.2794 -0.0078 4800 11.071 11.071 0. 0.9085 0.9960 0.0502 1.3192 1.3192 1.3193 -0.0078 5000 10.999 10.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5200 10.950 10.950 0.0550 0.0634 1.2793 1.3593 -0.0078 5200 10.950 10.950 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5400 10.950 10.950 10.950 0.08578 0.8579 -0.0117 1.3506 1.3500 0.0444 5400 10.951 10.951 0.0950 0.08589 -0.2381 1.3198 1.3198 1.3188 0.0758	3690.	14.380	14.380	n.	4.0542	4.0568	-0.0641	1.1464	1.1464	
4200- 11.747 11.746 0.0085 2.3952 2.3952 0. 1.2048 1.2048 0. 4400- 11.397 11.396 0.0088 1.716 1.7108 0.0467 1.2390 1.2391 -0.0081 4600- 11.192 11.191 0.0089 1.2611 1.2613 0.0654 1.2793 1.2391 -0.0081 4800- 11.071 11.071 9. 0.9865 0.9960 0.0502 1.3192 1.3193 -0.0076 5000- 10.999 12.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5200- 10.950 10.950 0. 0.5578 0.8579 -0.1011 1.3506 1.3500 0.0444 5400- 10.951 10.951 0. 0.85889 -0.2381 1.3198 1.3188 1.3188 0.0758								1.1596	1.1595	0.0086
4400. 11.397 11.396 0.0088 1.7316 1.7108 0.0467 1.2390 1.2391 -0.0081 4600. 11.192 11.191 0.0089 1.2621 1.2613 0.0634 1.2793 1.2794 -0.0078 4800. 11.071 11.071 0. 0.9965 0.9960 0.0502 1.3192 1.3193 -0.0078 5000. 10.999 10.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5200. 10.950 10.950 0.0050 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5400. 10.950 10.950 0.0550 0.8578 0.8579 -0.0110 1.3506 1.3500 0.0444 5400. 10.911 10.911 0. 0.8839 -0.2381 1.3198 1.3188 0.0758	4200.	11.747	11.746	0.0085	2.3952	2.3952	0.			
4800. 11.071 11.07: 0. 0.9965 0.9960 0.0502 11.3192 1.3193 -0.0076 5000. 10.999 10.998 0.0091 0.8578 0.8579 -0.0117 1.3476 1.3474 0.0148 5200. 10.950 10.950 0.950 0.05178 0.8187 -0.1101 1.3506 1.3500 0.0444 5400. 10.911 10.911 0. 0.8818 0.8839 -0.2381 1.3198 1.3188 0.0738			11.396	0.00A8	1.7116	1.7108	0.0467	1.2390	1.2391	-0.0081
5000 10.999 10.998 0.00°1 0.8578 0.8579 -0.0117 1.3474 1.3474 0.0148 5200 10.950 10.950 0. 0.8178 0.8187 -0.1101 1.3506 1.3500 0.0444 5400 10.911 10.911 0. 0.8818 0.8889 -0.7381 1.3198 1.3188 0.0758	4800.	11.071	11.071	9.	0.9965					
5400. 10.911 10.911 0. 0.8810 0.8839 -0.2381 1.3198 1.3188 0.0758		10.999	10.998	0.0001	0.8578	0.8579	-0.0117	1.3476	1.3474	0.0148
# / A / A / A / A / A / A / A / A / A /					0.8818					
56NC. 10.866 19.866 N. 1.0859 1.8894 -0.3223 1.2660 1.2649 0.0869										

JP-4/LOX -		MOL WT	ATME	CP C	AL/(MOL)(HAN ONE PERCI Ki	84	MMA (S)	
(K)	GORDON	BAHN		BORDON	BAHN		GORDON	BAHN	<u> </u>
600.	30,495 28,916	30,497 28,926	-0.0066 -0.0346	0.9468	0.4664	1,0984 *	1.1800	1,1788	0.1017 -0.1317
1000.	23.437	23,494	-0.2432	2.8013	2.7690	1.1530 *	1.1187	1,1191	-0.0358
1200.	18.697 18.485	18.708 18.435	-0.0588 0.	0.9241 0.5189	0.9407	-1.7963 • -0.2505	1.2087	1.2073	0.1158
1600.	18.426	18.426	0.	0.5076	0.5085	-0.1773	1.2702	1.2696	0.0472
2000.	18,425	18.425	0.	0.5114	0.5210	-0.1369 -0.1345	1.2676	1.2671	0.0394
2200.	18,416	18,416	0.	0.5375	0.5381	-0.1116	1.2551	1.2547	0.0319
2400. 2600.	18.397 18.355	18.397 18,355	0. 0.	0.5698	0.5702	-n.0702 -0.0478	1.2434	1.2432	0.0161
2800.	18,272	18,272	0.	0.7235	0.7237	-0.0276	1.2091	1.2090	0.0083
3000. 3200.	18.122	18.122 17.873	0	1.1059	0.8758	0.0161	1.1749	1,1906	<u> </u>
3400.	17.487	17.467		1.4377	1.4372	0.0348	1.1637	1.1637	
3600. 3800.	16.929 16,190	16.930 16.191	-0.0059 -0.0062	1.8786	1.8779	0.0373 0.0042	1.1578 1.1574	1,1578 1,1574	0.
4000.	15.314	15.315	-0.0065	2.8717	2.8227	-n.n354	1.1619	1.1619	0. n.
4200. 4400.	14,397	14,397 13.543	0.0074	3.0633 3.0327	3.0653 3.0348	-0.0653 -0.0692	1.1706	1.1706	0.
4600.	12,826	12.826	0 •	2.7636	2.7650	-0.0507	1.1978	1.1978	0.
4800. 5000.	12.269 	12.268 11.859	n.0982 n.0084	2.8641 1.947A	2.3646	-0.0211 -0.0103	1.2161	1.2161	0.
5200.	11.570	11.569	0.0086	1.5882	1.5888	-n.n378	1.2616	1.2614	0.0159
5400. 5600.	11.367	11.366	0.0089	1.1312	1.3163	-0.1141 -0.2652	1.2861	1.2856	0.0389
		= 1.6	ATM=					,	
600.	30.617	30.617	.0•	D-4211	0.4236	-0.5937	1.1882	1.1869	0.1094
800.	30.073	30.078	-0.0166	0.5997	0.5930	1.1172 *	1-1577	1.1596	-0.1641
1000. 1200.	27.721 22.363	27.749	-0.2907	1.2906 2.5826	2.5692	1.1932 *	1.1298	1.1305	0.0264
1490.	19.n72	19.091	-0.0996	1.0754	1.0906	-1.4134 *	1.2101	1.2089	0.0992
1600. 1800.	18.493 18.435	18.495 18.436	-8-01NB -8-0054	0.5688 0.5172	0.5718 0.5182	-0.5274 -0.1933	1.2604	1.2595	0.0714 0.0395
2000.	18.427	18.427	0.	0.5172	0.5179	-n.1353	1.2644	1.2639	0.0395
2400.	18.424	18.424 18.41R		0.5250	0.5256	-0.1143	1.259A 1.2538	_1.2595 _1.2585	0.0238
2600.	18.405	18.405	0.	0.5593	0.5596	-0.0536	1.2460	1.2458	0.0161
2800. 3000.	18.379 18.331	18.379 18.332	0. -0.0055	0.5921 0.6412	0.5923 0.6414	-0.0338 -0.0312	1.2362	1.2361	0.0081
3200.	18.253	18.253	n.	0.7120	0.7121	-0.0140	1.2129	1.2128	0.0082
3400	18.130	18.130_	0.	0.8102	0.9415	0.0123	1.2013	1.1913	0.
3600. 3800.	17.948 17.692	17.949 17.693	-0.0056 -0.0057	0.9417 1.1112	1.1109	0.0212 0.0270	1.1837	1.1837	n.
4000.	17.349	17.350	-0.0058	1.3188	1.3184	0.0303	1.1789	1.1789	n.
4200. 4400.	16.912 16.386	16.913 16.387	-0.0059 -0.0061	1.5546 1.7957	1.5543	0.0193 0.	1.1773	1.1773	0. 0.
4600.	15.792	15.793	-0.0063	2.0105	2.0110_	-0.0249	1.1832	1.1832	. 0.
4630.	15.164	15.164	n.	2.1683	2.1693	-0.0461 -0.0711	1.1900	1.1900	0. 0.
		14.536	0.	2.2489	2,2305		1.1788	1.1900	
5000. 5200.	14.536 13.942	14.536	0. 0.	2.2489 2.2467	2.2505	-0.0890	1.1988 1.2093	1.1988	0.0083
5000. 5200. 5400.	14.536 13.942 13.405	13.942 13.404	0. 0.0075	2.2467 2.1698	2.2487 2.1723	-0.0890 -0.1152		1.2092	
5000. 5200. 5400. 5600.	14.536 13.942 13.405 12.938	13.942 13.404 12.937	0. 0.0075 0.0077	2.2467 2.1698 2.0368	2.2487 2.1723 2.0402	-0.0890 -0.1152 -0.1669	1.2093 1.2212 1.2343	1.2092	0.0083 0.0164
5000. 5200. 5400.	14.536 13.942 13.405 12.938	13.942 13.404	0. 0.0075	2.2467 2.1698 2.0368	2.2487 2.1723 2.0402	-0.0890 -0.1152 -0.1669 HAN ONE PERCI	1.2093 1.2212 1.2343	1.2092	0.0083 0.0164
5000. 5200. 5400. 5600. JP-4/LOX	14.536 13.942 13.405 12.938	13.942 13.404 12.937	0. 0.0075 0.0077	2.2467 2.1698 2.0368	2.2487 2.1723 2.0402 IS OVER TO	-0.0890 -0.1152 -0.1669 HAN ONE PERCI	1.2093 1.2212 1.2343	1.2092 1.2210 1.2339	0.0083 0.0164
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975	13.942 13.404 12.937 F= 1.4 MOL WT RAHN 29.980	0. 0.0075 0.0077 ATH= 5	2.2467 2.1698 2.0368 1. CP C GORDON 0.6214	2.2487 2.1723 2.0402 IS OVER TI AL/(MOL)(I RAHN 0.6231	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) *	1.2093 1.2212 1.2343 NT GORDON 1.1579	1.2092 1.2210 1.2339 ANNA (S) BAHN _ 1.1572	0.0083 0.0164 0.0324 1
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891	13.942 13.404 12.937 F= 1.4 HOL HT RAHN 29.980 25.914	0. 0.0075 0.0077 ATH= 5. -0.0167 -0.0888	2.2467 2.1698 2.0368 1. CP C GORDON 0.6218 1.9096	2.2487 2.1723 2.0492 IS OVER TI AL/(MOL)(I RAHN 0.6231 1.8886	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) \$ -0.2091 1.0997 *	1.2093 1.2212 1.2843 NT GORDON 1.1579 1.1181	1.2092 1.2210 1.2339 ANMA (S) BAHN = 1.1572 1.1191	0.0083 0.0164 0.0324 7 0.0605 -0.0894
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K) 600. 800. 1000.	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 18.006 17.016	13.942 13.404 12.937 F= 1.4 HOL WT RAHN 29.980 25.914 18.061 17.016	0. 0.0075 0.0077 ATM= 5 -0.0167 -0.0888 -0.3055	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5325	2.2487 2.1723 2.0402 IS OVER TO AL/(HOL)(I) RAHN 0.6231 1.8886 3.9107 0.5336	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) \$ -0.2091 1.0997 * -0.3902	1.2093 1.2212 1.2343 NT GORDON 1.1579 1.1181 1.1235 1.2877	1.2092 1.2210 1.2339 IRMA (S) BAHN _ 1.1572 1.1191 1.1231 1.2873	0.0063 0.0164 0.0324 1 0.0605 -0.0894 0.0356 0.0311
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K) 	14.536 13.942 13.405 12.938 0/4 GORDON 29.975 25.891 18.006 17.016 17.016	13.942 13.404 12.937 F= 1.4 MOL WT PAHN 29.980 25.914 18.061 17.016 17.008	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.6218 1.9096 3.8955 0.5325 0.5158	2.2487 2.1723 2.0402 IS OVER TI AL/(MOL)(I RAHN 0.6231 1.8886 3.9107 0.5336 0.5164	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 -0.3902 -0.2066 -0.1163	1.209% 1.2212 1.2543 NT GORDON 1.1579 1.1181 1.1235 1.2877 1.2931	1.2092 1.2210 1.2339 NRMA (S) BAHN _ 1.1572 J.1191 1.1231 1.2873 1.2926	0.0083 0.0164 0.0324 1 1 0.0605 -0.0894 0.0356 0.0311 0.0387
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K) 	14.536 13.942 13.405 12.938 0/1 GORDON 29.975 25.891 18.006 17.016 17.008 17.008	13.942 13.404 12.937 F= 1.4 HOL WT RAHN 29.980 25.914 18.061 17.006 17.008 17.008	0. 0.0075 0.0077 ATM= 5 -0.0167 -0.0888 -0.3055	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5325	2.2487 2.1723 2.0402 IS OVER TO AL/(HOL)(I) RAHN 0.6231 1.8886 3.9107 0.5336	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) \$ -0.2091 1.0997 * -0.3902	1.2093 1.2212 1.2343 NT GORDON 1.1579 1.1181 1.1235 1.2877	1.2092 1.2210 1.2339 IRMA (S) BAHN _ 1.1572 1.1191 1.1231 1.2873	0.0083 0.0164 0.0324 7 0.0605 -0.0894 0.0356 0.0317 0.0387
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K) 600. 800. 1000. 1270. 1400. 1600. 2000.	14.536 13.942 13.405 12.938 0/1 GORDON 29.975 25.891 16.006 17.006 17.006 17.006 17.006	13.942 13.404 12.937 F= 1.4 MDL WT RAHN 29.980 25.914 18.061 17.016 17.008 17.008 17.008	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.909A 3.8955 0.5325 0.5198 0.5300 0.5300	2.2487 2.1723 2.0402 IS OVER TI AL/(MOL)((PAHN) 0.6231 1.8886 3.9107 0.5336 0.5164 0.5306 0.5306	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 1.0997 * -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905	1.2093 1.2212 1.2743 NT GORDON 1.1579 1.1181 1.1235 1.2877 1.2931 1.2902 1.2840	1.2092 1.2210 1.2339 INMA (5) BAHN 1.1572 1.1191 1.1231 1.2873 1.2926 1.2897 1.2836 1.2724	0.0083 0.0164 0.0324 7 0.0605 -0.0894 0.0356 0.0311 0.0387 0.0312 0.0312
5000. 5200. 5400. 5400. 5600. JP-4/LOX - TEMP (K) 600. 800. 1000. 1200. 1400. 1600. 2000. 2200. 2400.	14.536 13.942 13.405 12.938 	13.942 13.404 12.937 F= 1.4 MOL WT RAHN 29.980 25.914 18.061 17.008 17.008 17.008 17.008 16.999 16.977	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.6214 1.9096 3.8955 0.5325 0.5158 0.5198 0.5300 0.5527 0.6028 0.7040	2.2487 2.1723 2.1402 IS OVER TI AL/(MOL)(I PAHN 0.6286 3.9107 0.5336 0.5306 0.5532 0.6032 0.7043	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 1.0997 * -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0664 -0.1426	1.2093 1.2212 1.2743 NT GGORDON 1.1579 1.1181 1.2355 1.2877 1.2902 1.2840 1.2727 1.2535 1.2264	1.2092 1.2210 1.2339 INMA (S) BAHN - 1.1572 1.1191 1.1231 1.2873 1.2926 1.2897 1.2836	0.0605 -0.0605 -0.0894 0.0356 0.0351 0.0387 0.0387 0.0387 0.0387
5000. 5200. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 18.006 17.016 17.008 17.006 16.979 16.977 14.920	13.942 13.404 12.937 F= 1.4 MOL NT RAHN 29.980 25.914 18.061 17.016 17.008 17.008 17.008 16.977 16.920 16.775	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.6218 1.9096 3.8955 0.5325 0.5158 0.5198 0.5300 0.5527 0.6028 0.7040 0.8887	2.2487 2.1723 2.0402 IS OVER TI AL/(MOL)(I RAHN 0.6231 1.8886 7.9107 0.5336 0.5306 0.5302 0.6932 0.6932 0.8889	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 1.0997 • -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0664 -0.0426	1.2093 1.2212 1.2343 NT GORDON 1.1579 1.1181 1.1235 1.2877 1.2931 1.2902 1.2840 1.2727 1.2535 1.2536 1.1976	1.2092 1.2210 1.2339 NMA (S) BAHN 1.1572 1.1231 1.2873 1.2926 1.2897 1.2836 1.2724 1.2533 1.2953 1.2754 1.2754	0.0083 0.0164 0.0324 7 0.0605 -0.0894 0.0317 0.0317 0.0317 0.0317 0.0317 0.0317 0.0082
5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 18.006 17.016 17.006 17.006 17.006 17.006 17.006 16.979 16.977 16.920 16.775 16.556	13.942 13.404 12.937 F= 1.4 HOL HT RAHN 29.980 25.981 18.061 17.008 17.008 17.008 17.006 16.999 16.977 16.920 16.795 16.556	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5325 0.5198 0.5300 0.5527 0.6028 0.7040 0.8887 1.1960 1.6705	2.2487 2.1723 2.0402 IS OVER T. AL/(MOL)(I PAHN 0.6236 3.9107 0.5336 0.5306 0.5320 0.6032 0.6032 0.6032 0.8889 1.16706	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0666 -0.0225	1.2093 1.2212 1.2743 NT GORDON 1.1579 1.1181 1.2931 1.2902 1.2840 1.2727 1.2535 1.27264 1.1732 1.1736	1.2092 1.2210 1.2339 1.2339 1.2339 1.2339 1.1591 1.1591 1.1231 1.2873 1.2893 1.2893 1.2893 1.2893 1.2893 1.2724 1.2533 1.2724 1.2733 1.1750 1.1751	0.0083 0.0164 0.0324 7 -0.0892 0.0356 0.0311 0.0387 0.0387 0.0382 0.0312 0.0302 0.0084
5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K) .600. 800. 1000. 1200. 1400. 1800. 2000. 2400. 2400. 2400. 2400. 3200.	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 16.006 17.016 17.008 17.008 16.999 16.977 16.920 16.775 16.556 16.147	13.942 13.404 12.937 F= 1.4 HOL WT RAHN 25.914 18.061 17.006 17.008 17.008 17.008 17.006 16.999 16.977 16.920 16.556 16.556	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.6218 1.9096 3.8955 0.5158 0.5198 0.5309 0.5309 0.7040 0.8887 1.1960 1.6705 2.3454	2.2487 2.1723 2.0402 IS OVER TI AL/(MOL)((FAHN) 0.6231 1.8886 3.9107 0.5336 0.5164 0.5336 0.6032 0.7043 0.8889 0.8032 0.4032 0.4032 0.4032 0.4032 0.4032 0.4032 0.4032	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) \$ -0.2091 1.0997 * -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0905 -0.0905 -0.0905 -0.0060 -0.025 -0.0060 -0.0043	1.2093 1.2212 1.27843 NT GORDON 1.1579 1.1181 1.1235 1.2877 1.2931 1.2902 1.2840 1.2727 1.2535 1.2640 1.1732 1.1566	1.2092 1.2210 1.2339 IRMA (S) BAHN 1.1572 1.1231 1.2873 1.2897 1.2836 1.2724 1.2533 1.2725 1.1731 1.1566 1.1480	0.0605 -0.0894 0.0324 0.0605 -0.0894 0.0356 0.0311 0.0374 0.0326 0.0085 0.0085
5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K) 600. 800. 1200. 1400. 1600. 1800. 2200. 2400. 2400. 2400. 2400. 3000.	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 18.006 17.016 17.006 17.006 17.006 17.006 17.006 16.979 16.977 16.920 16.775 16.556	13.942 13.404 12.937 F= 1.4 HOL HT RAHN 29.980 25.981 18.061 17.008 17.008 17.008 17.006 16.999 16.977 16.920 16.795 16.556	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5325 0.5198 0.5300 0.5527 0.6028 0.7040 0.8887 1.1960 1.6705	2.2487 2.1723 2.0402 IS OVER T. AL/(MOL)(I PAHN 0.6236 3.9107 0.5336 0.5306 0.5320 0.6032 0.6032 0.6032 0.8889 1.16706	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0666 -0.0225	1.2093 1.2212 1.2743 NT GORDON 1.1579 1.1181 1.2931 1.2902 1.2840 1.2727 1.2535 1.27264 1.1732 1.1736	1.2092 1.2210 1.2339 1.2339 1.2339 1.2339 1.1591 1.1591 1.1231 1.2873 1.2893 1.2893 1.2893 1.2893 1.2893 1.2724 1.2533 1.2724 1.2733 1.1750 1.1751	0.0083 0.0164 0.0324 7 -0.0892 0.0356 0.0311 0.0387 0.0387 0.0382 0.0312 0.0302 0.0084
5000. 5200. 5400. 5400. 5600. JP-4/LOX - TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 16.006 17.006 17.006 17.006 16.999 16.977 16.920 16.755 16.147 15.515 14.646 13.629 12.657	13.942 13.404 12.937 F= 1.4 MDL WT PAHN 29.980 25.914 18.061 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 18.556 16.556 16.556 16.147 15.515 14.646 13.628 12.657	0.0075 0.0077 ATM= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5158 0.5158 0.5158 0.5300 0.5300 0.5300 0.620 0.620 0.8857 1.960 1.6705 2.3454 3.1450 3.7260 3.6887	2.2487 2.1723 2.1723 2.1402 IS OVER TI AL/(MOL)((RAHN) 0.6281 0.5336 0.5336 0.5336 0.5532 0.7043 0.6332 0.7043 0.6332 0.7043 0.6332 0.7043 0.6332 0.7043 0.5336 0.7043	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 1.0997 -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0664 -0.0225 -0.0664 -0.0225 -0.0664 -0.0225 -0.0664 -0.0225 -0.0664 -0.0225 -0.0664 -0.0225 -0.0664 -0.0225	1.2093 1.2212 1.2743 NT GGRDON 1.1579 1.1181 1.1235 1.2247 1.2931 1.2902 1.2840 1.2727 1.2535 1.2264 1.1732 1.1566 1.1466 1.1523 1.1645	1.2092 1.2210 1.2339 1.2339 1.2319 1.2319 1.1191 1.1231 1.28973 1.28973 1.28973 1.28973 1.28973 1.2724 1.25733 1.1975 1.1731 1.1566 1.1480 1.1466 1.1523 1.1644	0.0045 0.0324 7 0.0605 -0.0894 0.0356 0.03147 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0387 0.0085
5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K) 600. 800. 1000. 1200. 1400. 1600. 2400. 2400. 2400. 2400. 3200. 3400. 3500. 3600. 3600. 3600.	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 16.006 17.016 17.006 16.999 16.977 16.920 16.775 16.556 16.147 15.515 14.646 13.629 12.657 11.387	13.942 13.404 12.937 F= 1.4 HOL HT RAHN 29.980 25.914 18.061 17.016 17.008 17.008 17.008 17.008 16.999 16.977 16.920 16.795 16.556 16.147 15.515 14.646 13.628	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.621A 1.9096 3.8955 0.5325 0.5158 0.5198 0.5327 0.6028 0.7040 0.8887 1.1960 1.6705 2.3454 3.1450	2.2487 2.1723 2.0402 IS OVER TO RAHN 0.6281 1.88867 0.5336 0.5332 0.6032 0.6032 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033 0.6033	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) * -0.2091 -1.0997 -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0167 -0.0265 -0.0257 -0.0060 -0.043 -0.0127 -0.0167	1.2093 1.2212 1.2743 NT GORDON 1.1579 1.181 1.1235 1.2877 1.2931 1.2902 1.2840 1.2727 1.2535 1.2727 1.1732 1.1736 1.1736 1.1746 1.1466 1.1466	1.2092 1.2210 1.2339 1MMA (S) BAHN - 1.1572 1.12873 1.2873 1.2926 1.2897 1.2833 1.29265 1.1751 1.17566 1.1751 1.1566 1.1480 1.1460 1.1523	0.0045 0.0164 0.0324 7 0.0605 -0.0316 0.0317 0.0382 0.0312 0.0312 0.0362 0.0045 0.0045 0.0045
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5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938 0/6 GORDON 29.975 25.891 16.006 17.016 17.006 16.999 16.977 16.920 16.775 16.556 16.147 15.515 14.646 13.629 12.657 11.387	13.942 13.404 12.937 F= 1.4 HOL WT RAHN 25.914 18.061 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.008 17.0	0. 0.0075 0.0077 ATM= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. 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CP C GORDON 0.6218 1.9096 3.8955 0.5358 0.5158 0.5158 0.5300 0.5527 0.6028 0.7040 0.8887 1.6705 2.3454 3.1450 3.7269 3.6887 3.0824 2.7926 1.6846 1.2632 0.9015 1.6705 1.0520 1.3779 10.4819 0.9764 1.3260 0.5511 0.5521 0.5521 0.55260 0.5521	2.2487 2.1723 2.1723 2.1402 IS OVER TO MOLIVE FARM OF THE PROOF TO THE	-0.0890 -0.1152 -0.1669 HAN ONE PERCI K) -0.2091 1.9997 -0.3902 -0.2066 -0.1163 -0.1154 -0.1132 -0.0905 -0.0167 -0.0060 -0.0225 -0.0167 -0.0060 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0256 -0.0356	1.2093 1.2212 1.2743 NT GGRDON 1.1579 1.1181 1.1235 1.2877 1.2931 1.2902 1.2840 1.1976 1.1976 1.1976 1.1566 1.1523 1.1645 1.1831 1.2089 1.2426 1.18371 1.2089 1.2266 1.13371 1.3371 1.3371 1.3371 1.3371 1.3371 1.3566 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.2907 1.2866 1.2796 1.2796 1.2796 1.2796 1.2796	1.2092 1.2210 1.2339 1.2339 1.2319 1.1501 1.1501 1.1231 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.2826 1.1975 1.1975 1.1975 1.1976 1.1466 1.1466 1.1466 1.1466 1.1466 1.1466 1.1460 1.2090 1.2427 1.3179 1.3281 1.2785 1.2785 1.1732 1.2836 1.2785 1.2785 1.2785 1.2785 1.2785 1.2785 1.2785 1.28397 1.28397 1.28397 1.28397 1.28399 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26999 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.26899 1.2	0.0834 0.0164 0.0324 7 0.0605 -0.0894 0.0356 0.0317 0.0387 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085 0.0085
5000. 5200. 5400. 5400. 5600. JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938	13.942 13.404 12.937 F=1.4 HOL NT RAHN 29.914 18.061 17.008 17.008 17.008 17.008 17.006 16.997 16.920 16.556 16.555 14.646 13.657 11.386 12.657 11.386 12.657 11.386 12.657 11.071 10.885 10.774 10.705 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.550 10.55	0. 0.0075 0.0077 ATH= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. CP C GORDON 0.6218 1.9096 3.8955 0.5158 0.5198 0.5300 0.5527 0.6028 0.7040 0.8887 1.1960 1.67028 2.3454 3.1450 3.7269 3.6887 3.1450 3.7269 3.6887 3.1450 3.7269 3.6887 3.1769 1.6846 1.2631 1.0162 0.90157 1.0520 0.90157 1.0520 0.9511 0.9764 0.5511 0.55260 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 0.55370 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CP C GORDON 0.621A 1.9096 3.8955 0.5325 0.5158 0.5300 0.5300 0.5300 0.5300 0.7040 0.620 0.7040 0.8887 3.1450 3.7269 3.6887 3.1450 3.7269 3.6887 3.1062 0.9012 0.9012 0.9015 1.0379 1.0379 1.0520 1.3779 10.5370 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 0.5567 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JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938	13.942 13.404 12.937 F= 1.4 MDL NT PAHN 29.981 18.061 17.006 17.006 17.006 17.006 16.999 16.977 16.5515 16.5515 14.646 13.6627 11.386 11.071 10.885 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 10.705 1	0. 0.0075 0.0077 ATM= \$ -0.0167 -0.0888 -0.3055 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	2.2467 2.1698 2.0368 1. 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JP-4/LOX TEMP (K)	14.536 13.942 13.405 12.938	13.942 13.404 12.937 F= 1.4 MDL WT PAHN 29.9914 18.061 17.008 17.008 17.008 17.008 17.006 16.999 16.997 16.920 16.795 16.556 16.147 15.515 14.646 13.657 11.386 11.071 10.885 11.071 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 10.750 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1.2727 1.2535 1.1732 1.1566 1.1732 1.1566 1.1742 1.1831 1.2089 1.2426 1.1831 1.2089 1.2264 1.1732 1.1366 1.1831 1.2793 1.2816 1.1831 1.2946 1.2946 1.2946 1.2946 1.2946 1.2816 1.3178 1.3371 1.2846 1.1831 1.2946 1.2946 1.2946 1.2946 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.1988 1.2846 1.2907 1.2860 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 1.2796 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Color Colo	TEMP		HOL HT	ATH# :	CP CA	L/(MOL)(K		GA	HHA (S)	
1000	(K)	GORDON	BAHN	<u> </u>	GORDON	BAHN		GURDON		
1000										0.1015
1000										-0.1300 -0.0620
1400							0.4900			0.0176
1000				-0-1431	1.3984	1.4142	-1.1299 *	1.2059		0.0829
2000. 17.015 17.015 -0.0549 0.5384 0.5384 0.1320 1.2818 1.2809 2200. 17.001 17.006 -0.0519 0.5420 0.1440 -0.0738 1.2717 1.2252 2200. 10.488 10.499 -0.0519 0.5950 0.5800 -0.0517 1.2258 1.2258 2200. 10.488 10.499 -0.0519 0.5950 0.5800 -0.0517 1.2258 1.2258 2200. 10.488 10.499 -0.0519 0.5950 0.5800 -0.0517 1.2258 1.2258 2200. 10.488 10.499 -0.0519 0.7303 0.7304 -0.0517 1.2268 1.2268 2200. 10.488 10.499 -0.0519 0.7303 0.7304 -0.0517 1.2261 1.2263 2200. 10.488 10.499 -0.0519 0.7303 0.7304 -0.0512 1.2262 1.2263 2200. 10.489 10.489 -0.0518 -0.0518 1.2267 1.2262 2200. 10.489 10.489 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518 -0.0518				-0.0291						0.0791
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Shoro	600.	10.542								-0.0156
S200. 10.299 10.290 0. 1.295 0. 1.295 0. 1.295 0. 1.245 1.246 1.229 1.2125 5600. 10.130 10.130 0. 1.9364 1.9406 -0.2109 1.1855 1.1850										n. n.0078
10.130										0.0320
10.130				-	1.5437	1.5463	-0.1684	1.2129	1.2125	0.0330
TENP						1.9406	-0.2169	1.1855	1.1850	8.0422
TEMP	.4/1 OY	04	/Fz 1.9	ATM-	10. = 1	IS OVER T	MAN ONE PERCE	NT		
CK1 GORDON BANN B. GORDON			MOL WT	A I II I	CP C	AL/(HOL)	K)	G		
800. 28.481 28.483 -0.0421 1.0110 1.0022 0.8704 1.1345 1.3387 1.000 17.038 17.071 -0.1937 2.3926 2.4211 -1.1912 1.1164 1.1181 1.200. 17.038 17.071 -0.1937 2.3926 2.4211 -1.1912 1.11608 1.1599 1.400 15.724 15.728 -0.0254 0.7112 0.7168 -0.7874 1.2788 1.2787 1.600 15.603 15.604 -0.0064 0.5464 0.5492 -0.1459 1.3110 1.3107 1.800 15.529 15.559 0. 0.5447 0.5451 -0.0734 1.3069 1.3067 2.000 15.589 15.569 0. 0.5572 0.5575 -0.0334 1.3069 1.3067 2.000 15.589 15.569 0. 0.5572 0.5575 -0.0348 1.2985 1.2983 2.000 15.589 15.559 0. 0.5800 0.5670 -0.0580 0.5572 1.2869 1.2867 2.200 15.589 15.569 0. 0.5800 0.5670 -0.0345 1.2869 1.2867 2.200 15.584 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.9680 0.6881 -0.0145 1.2510 1.2500 2.600 15.526 15.526 0. 0.9505 0.9505 0.9508 -0.0344 1.1261 1.2709 2.600 15.526 15.526 0. 0.9505 0.9508 -0.0346 1.2098 1.2098 3.000 15.454 15.455 0. 0.9505 0.9508 -0.0316 1.2098 1.2098 3.000 15.454 15.455 0. 0.9505 0.9508 -0.0316 1.2098 1.2098 3.000 15.454 15.453 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 3.400 1.461 14.461 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 3.600 1.461 14.461 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 1.1944 3.600 1.461 14.461 0. 1.1628 1.768 3.600 1.461 1.461 14.461 0. 1.1628 1.768 3.600 1.161 1.178 1.1778 4.000 13.483 13.433 0.0072 2.0772 2.0783 -0.0535 1.1817 1.178 1.1778 4.000 13.483 13.433 0.0072 2.0772 2.0783 -0.0535 1.1817 1.1871 1.1871 4.000 12.299 12.290 0.0061 2.5864 2.5809 -0.0351 1.1817 1.1871 1.1974 4.000 12.299 12.290 0.0061 2.5864 2.5809 -0.0351 1.1817 1.1871 1.1975 3.000 1.1.081 1.080 1.097 1.097 3.0078 2.3500 -0.0322 1.2295 1.2295 3.000 1.1.084 11.080 0.0090 1.8586 2.5809 -0.0351 1.1871 1.2991 1.2995 3.000 1.1.081 1.080 1.080 0.0090 1.8586 0.6830 -0.4204 1.1998 1.1298 3.000 1.0577 3.0378 -0.0097 1.0097 3.0378 1.0098 1.1499 1.2998 3.000 1.5.736 15.738 -0.0097 1.0979 2.5192 2.5000 0.4538 1.1395 1.2299 1.2295 3.000 1.5.500 15.500 0.0090 1.5897		GORDON			SORDON	BAHN	<u> </u>	CORDON	BAHN	<u>s</u>
800. 28.481 28.483 -0.0421 1.0110 1.0022 0.8704 1.1345 1.3387 1.000 17.038 17.071 -0.1937 2.3926 2.4211 -1.1912 1.1164 1.1181 1.200. 17.038 17.071 -0.1937 2.3926 2.4211 -1.1912 1.11608 1.1599 1.400 15.724 15.728 -0.0254 0.7112 0.7168 -0.7874 1.2788 1.2787 1.600 15.603 15.604 -0.0064 0.5464 0.5492 -0.1459 1.3110 1.3107 1.800 15.529 15.559 0. 0.5447 0.5451 -0.0734 1.3069 1.3067 2.000 15.589 15.569 0. 0.5572 0.5575 -0.0334 1.3069 1.3067 2.000 15.589 15.569 0. 0.5572 0.5575 -0.0348 1.2985 1.2983 2.000 15.589 15.559 0. 0.5800 0.5670 -0.0580 0.5572 1.2869 1.2867 2.200 15.589 15.569 0. 0.5800 0.5670 -0.0345 1.2869 1.2867 2.200 15.584 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.6201 0.6203 -0.0323 1.2710 1.2709 2.600 15.564 15.564 0. 0.9680 0.6881 -0.0145 1.2510 1.2500 2.600 15.526 15.526 0. 0.9505 0.9505 0.9508 -0.0344 1.1261 1.2709 2.600 15.526 15.526 0. 0.9505 0.9508 -0.0346 1.2098 1.2098 3.000 15.454 15.455 0. 0.9505 0.9508 -0.0316 1.2098 1.2098 3.000 15.454 15.455 0. 0.9505 0.9508 -0.0316 1.2098 1.2098 3.000 15.454 15.453 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 3.400 1.461 14.461 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 3.600 1.461 14.461 0. 1.1624 1.1628 -0.0344 1.1944 1.1944 1.1944 3.600 1.461 14.461 0. 1.1628 1.768 3.600 1.461 1.461 14.461 0. 1.1628 1.768 3.600 1.161 1.178 1.1778 4.000 13.483 13.433 0.0072 2.0772 2.0783 -0.0535 1.1817 1.178 1.1778 4.000 13.483 13.433 0.0072 2.0772 2.0783 -0.0535 1.1817 1.1871 1.1871 4.000 12.299 12.290 0.0061 2.5864 2.5809 -0.0351 1.1817 1.1871 1.1974 4.000 12.299 12.290 0.0061 2.5864 2.5809 -0.0351 1.1817 1.1871 1.1975 3.000 1.1.081 1.080 1.097 1.097 3.0078 2.3500 -0.0322 1.2295 1.2295 3.000 1.1.084 11.080 0.0090 1.8586 2.5809 -0.0351 1.1871 1.2991 1.2995 3.000 1.1.081 1.080 1.080 0.0090 1.8586 0.6830 -0.4204 1.1998 1.1298 3.000 1.0577 3.0378 -0.0097 1.0097 3.0378 1.0098 1.1499 1.2998 3.000 1.5.736 15.738 -0.0097 1.0979 2.5192 2.5000 0.4538 1.1395 1.2299 1.2295 3.000 1.5.500 15.500 0.0090 1.5897	600.	30.232	30.234	-0.0066	0.5020	0.5036	-0.3187	1,1683	1,1675	0.0685
1200		28,481	28.493	-0.0421	1.0110	1.0022	0.8704	1.1345	1.1355	-0.0881
1400										0.0775
1600. 15,603 15,604 -0.0064 0.5484 0.5492 -0.1459 1.3110 1.3107 2000. 15,589 15,589 0.								1,2798		0.0860
2000. 15,589 15,589 0. 0.5572 0.5572 -0.0538 1.2985 1.2983 2000. 15,582 15,582 0. 0.5800 0.5802 -0.0345 1.2869 1.2867 2400. 15,584 15,564 0. 0.6201 0.6203 -0.0323 1.210 1.2709 2600. 15,526 15,252 0. 0.6880 0.6880 0.6881 -0.0145 1.2210 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.2510 1.251		15.603	15.604		0.5484		-0.1459	1.3110	1.8107	0.0229
2200	1800.	15.592	15.592	0.	0,5447				1,3067	0.0153
2400, 15,564 15,564 0. 0.6201 0.6203 -0.0328 1.2710 1.2709 2600. 15,454 15,456 0. 0.7947 0.7949 -0.0252 1.2295 1.2295 3800. 15,454 15,456 0. 0.7947 0.7949 -0.0252 1.2295 1.2295 3800. 15,331 15,131 0. 1.1624 1.1628 -0.0316 1.2098 1.2098 3200. 15,131 15,131 0. 1.1624 1.1628 -0.0316 1.2098 1.2098 3200. 14,845 14,845 0. 1.4306 1.4312 -0.0419 1.1842 1.1841 3400. 14,845 14,845 0. 1.4306 1.4312 -0.0419 1.1842 1.1841 3400. 13,434 13,433 0.0072 2.0772 2.0783 -0.0536 1.1778 1.1778 4000. 13,434 13,433 0.0074 2.3740 2.3751 -0.0458 1.1788 1.1788 3800. 13,984 13,983 0.0074 2.3740 2.3751 -0.0458 1.1871 1.1871 4000. 12,294 12,293 0.0061 2.5804 2.5809 -0.0351 1.1871 1.1871 4400. 12,294 12,293 0.0061 2.5804 2.5809 -0.0194 1.1969 1.1969 1.1969 4800. 11,799 11,797 0.0170 2.4760 2.4260 0. 1.2098 1.2098 4800. 11,394 11,392 0.0176 2.1564 2.1559 0.0282 1.2256 1.2257 5000. 11,084 11,080 0.0090 1.8569 1.8566 0.0162 1.2231 1.2256 5200. 10,849 10,848 0.0092 1.6036 1.6041 -0.0312 1.2285 1.2285 5400. 10,544 10,543 0.0095 1.4004 1.4040 -0.2571 1.2585 1.2582 5400. 10,544 10,543 0.0095 1.4004 1.4040 -0.2571 1.2585 1.2582 600. 30,377 30,378 -0.0038 0.4519 0.4538 -0.4204 1.1756 1.1747 800. 27,375 27,381 -0.0087 1.3174 1.3037 1.0359 1.1492 1.1504 1000. 27,354 27,381 -0.0087 1.3174 1.3037 1.0359 1.1492 1.1504 1000. 15,622 17,726 -0.1092 1.0740 0.4538 -0.4204 1.1756 1.1747 2000. 15,622 17,726 -0.1092 1.0740 0.4538 -0.4204 1.1756 1.1747 2000. 15,627 15,628 -0.0064 0.5754 0.6603 -0.4106 1.2287 1.2284 2600. 15,736 15,738 -0.0027 0.0576 0.6603 -0.4106 1.2287 1.2284 2600. 15,550 15,550 0. 0.064 0.5784 0.5797 -0.0701 1.2930 1.2930 1.2949 2000. 15,627 15,628 -0.0064 0.5784 0.5797 -0.0701 1.2930 1.2940 3000. 15,600 15,600 0. 0. 0.5703 0.5707 -0.0701 1.2930 1.2940 3000. 15,600 15,600 0. 0. 0.5827 0.5829 -0.0343 1.2074 1.2074 2800. 15,750 15,550 0. 0.0647 0.0577 0.0977 -0.0701 1.2930 1.2940 3200. 15,600 15,600 0. 0. 0.6824 0.6826 -0.0353 1.2074 1.2074 3800. 15,750 15,500 0.0667 1.1120 1.1120 1.1125 -0.0450 1.2044 1.2044 3800. 15,750 15,550 0.0067 1.1120 1.11							-0.0538			0.0154
2600		15.564	15.564		0.6201					0.0079
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3400, 14,845 14.845 0. 1.4806 1.4312 -0.0419 1.1842 1.1841 3600. 14.461 14.461 0. 1.7450 1.7458 -0.0458 1.1788 1.1788 3800, 13,984 13.983 0.0072 2.0772 2.0783 -0.0558 1.1778 1.1778 4000. 13,434 13.433 0.0074 2.3740 2.3751 -0.0463 1.1807 1.1807 4200, 12,284 12,283 0.0078 2.5617 2.5626 -0.0463 1.1807 1.1807 4400. 12.294 12.293 0.0081 2.5804 2.5809 -0.0194 1.1969 1.1969 4800. 11,799 11,797 0.0170 2.4960 2.4280 0. 1.2098 1.2098 1.2099 4800. 11,394 11.392 0.0176 2.1564 2.1559 0.0232 1.2256 1.2257 5900. 11.081 11.080 0.0090 1.8569 1.6061 -0.0512 1.2256 1.2257 5900. 10.849 10.848 0.092 1.6036 1.6061 -0.0512 1.2582 1.2255 5900. 10.849 10.848 0.092 1.6036 1.6061 -0.0512 1.2582 1.2258 5000. 10.544 10.543 0.0095 1.4004 1.4040 -0.2571 1.2582 1.2658 1.2688 5600. 10.544 10.543 0.0095 1.4004 1.4040 -0.2571 1.2582 1.2658 1.2668 600. 30.373 -0.0033 0.4519 0.4538 -0.4204 1.1756 1.1747 800. 29.772 29.777 -0.0168 0.4433 0.6380 0.8239 1.1492 1.1504 1000. 27.354 27.381 -0.0987 1.3174 1.3037 1.0399 1.1492 1.1504 1000. 27.354 27.381 -0.0987 1.3174 1.3037 1.0399 1.1268 1.1274 1200. 22.151 22.211 -0.2709 2.5122 2.5008 0.4538 1.1335 1.1335 1400. 17.692 17.726 -0.1922 1.9740 1.9916 -0.8916 1.1733 1.1363 1600. 16.72 16.182 -0.0618 0.9553 0.9626 -0.7642 1.2549 1.2549 2000. 15.627 15.628 -0.0064 0.5784 0.5792 -0.1383 1.2974 1.2982 2000. 15.627 15.628 -0.0064 0.5784 0.5792 -0.1383 1.2974 1.2989 2400. 15.588 15.588 0. 0.5827 0.5829 -0.0343 1.2959 1.2849 2600. 15.574 15.574 0. 0.0669 0.6070 -0.0155 1.2267 1.2263 3400. 15.588 15.588 0. 0.5827 0.5829 -0.0343 1.2950 1.2849 2600. 15.574 15.575 0. 0. 0.6640 0.6973 -0.0155 1.2262 1.2263 3400. 15.586 15.580 0. 0.6841 0.6447 -0.0155 1.2264 1.2973 2400. 15.588 15.580 0. 0.6844 0.6826 -0.0232 1.2243 1.2243 3400. 15.575 15.510 0. 0. 0.6972 0.6973 -0.0155 1.2263 1.2243 3400. 15.576 15.510 0. 0. 0.6972 0.6973 -0.0155 1.2263 1.2243 3400. 15.576 15.510 0. 0. 0.6972 0.6973 -0.0135 1.2263 1.2263 3400. 15.576 15.570 0. 0.0669 1.4277 1.4277 -0.0350 1.2014 1.2017								1,2098	1.2098	0.
\$800. 14.461 14.461 0. 1.7450 1.7458 -0.0458 1.1788 1.1788 \$800. 13.984 13.983 0.0072 2.0772 2.0783 -0.0580 1.1778 1.1778 4000. 13.434 13.433 0.0074 2.3740 2.3751 -0.0463 1.1807 1.1807 4200. 12.854 12.853 0.0078 2.5617 2.9526 -0.0351 1.1817 1.1807 4400. 12.294 12.293 0.0081 2.5604 2.5809 -0.0351 1.1969 1.1969 4500. 11.799 11.797 0.0170 2.4260 2.4260 0. 1.2098 1.2099 4800. 11.394 11.392 0.0176 2.1564 2.1559 0.0232 1.2256 1.2257 5000. 11.081 11.080 0.0090 1.6569 1.8566 0.0162 1.2431 1.2430 5200. 10.849 10.848 0.0092 1.6036 1.6041 -0.0312 1.2555 1.2552 5400. 10.677 10.676 0.0094 1.4455 1.4473 -0.1245 1.2654 1.2654 5600. 10.544 10.543 0.0095 1.4004 1.4040 -0.2571 1.2551 1.2564 5600. 10.544 10.543 0.0095 1.4004 1.4040 -0.2571 1.2591 1.2562 **OF** 1.2** **ATH** 100.** 690. 30.377 30.378 -0.0033 0.4519 0.4538 -0.4204 1.1756 1.1747 800. 27.354 27.381 -0.0987 1.3174 1.3037 1.0399 1.1462 1.1504 1000. 27.354 27.381 -0.0987 1.3174 1.3037 1.0399 1.1268 1.1274 1200. 22.151 22.211 -0.2709 2.5122 2.5008 0.4538 1.1335 1.1335 1400. 17.692 17.726 -0.1922 1.7740 1.9916 -0.8916 1.1793 1.1783 1600. 16.172 16.182 -0.0618 0.9553 0.9026 -0.7642 1.2599 1.2591 2000. 15.627 15.628 -0.0064 0.5784 0.5792 -0.1383 1.2974 1.2991 2000. 15.627 15.628 -0.0064 0.5784 0.5792 -0.1383 1.2974 1.2992 2400. 15.588 55.588 0. 0.5827 0.5929 -0.0333 1.2974 1.2979 2400. 15.588 55.588 0. 0.5827 0.5929 -0.0333 1.2974 1.2930 3200. 15.574 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 2800. 15.574 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 3800. 15.734 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 3800. 15.745 15.510 0. 0.6972 0.6973 -0.0133 1.2493 1.2493 3800. 15.250 15.510 0. 0.6972 0.6973 -0.0133 1.2493 1.2493 3800. 15.262 15.025 0.0067 1.1120 1.12647 -0.0366 1.2350 1.2263 3800. 15.262 15.025 0.0067 1.1120 1.12647 -0.0366 1.2350 1.2263 3800. 15.264 15.025 0.0069 1.4272 1.4277 -0.0350 1.2017 1.2017								1.1542	1.1841	0.0084
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\$200. 10.84\$	4800.	11.394	11.392	0.0176	2.1564	2.1559	0.0232	1.2256		-0.0082
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0/F= 1.2 ATM= 100. 690. 30.377 30.378 -0.0033 0.4519 0.4538 -0.4204 1.1756 1.1747 800. 29.772 29.777 -0.0168 0.6433 0.6380 0.8239 1.1492 1.1504 1000. 27.354 27.381 -0.0987 1.3174 1.3037 1.0399 1.1268 1.1274 1200. 22.151 22.211 -0.2709 2.5122 2.5008 0.4538 1.1335 1.1332 1400. 17.692 17.726 -0.1922 1.9740 1.9916 -0.8916 1.1793 1.1783 1600. 16.172 16.182 -0.0618 0.9553 0.9626 -0.7642 1.2549 1.2540 1800. 15.736 15.738 -0.0127 0.6576 0.6603 -0.4106 1.2897 1.2891 1800. 15.627 15.628 -0.0644 0.5784 0.5797 -0.1383 1.2974 1.2972 2200. 15.600 15.600 0. 0.5703 0.5707 -0.0701 1.2650 1.2929 2400. 15.588 15.588 0. 0.5527 0.5829 -0.0343 1.2891 2400. 15.588 15.588 0. 0.5527 0.5829 -0.0343 1.2850 1.2849 2400. 15.574 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 2800. 15.550 15.550 0. 0.6441 0.6442 -0.0155 1.2626 1.2625 3000. 15.510 15.510 0. 0.6972 0.6973 -0.0134 1.2493 1.2493 3200. 15.445 15.445 0. 0.6641 0.6442 -0.0155 1.2626 1.2625 3400. 15.544 15.455 0. 0.7694 0.7695 -0.0130 1.2849 3400. 15.545 15.455 0. 0.7694 0.7695 -0.0130 1.2849 1.2849 3400. 15.547 15.347 0. 0.6624 0.8626 -0.0232 1.2243 1.2243 3600. 15.210 15.210 0. 0.9770 0.9773 -0.0306 1.2030 1.2030 4200. 14.791 14.791 0. 1.2642 1.2647 -0.0306 1.2030 1.2030 4200. 14.791 14.791 0. 1.2642 1.2647 -0.0306 1.2030 1.2030	5600.	10.544	10.543	0.0095		1.4040	-n.2571	1.2591		0.0715
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1600. 16.172 16.182 -0.0618 0.9553 0.9826 -0.7642 1.2549 1.2549 1.2549 1.2549 1.2891 1.2891 1.2897 1.2891 1.2897 1.2891 1.2897 1.2891 1.2897 1.2891 1.2897 1.2891 1.2897 1.2891 1.2897 1.2897 1.2891 1.2974 1.2972 1.2972 1.2972 1.2972 1.2972 1.2972 1.2972 1.2980 1.2981 1.2980 1.2980 1.2981 1.2849 1.2849 2800 15.550 15.550 0. 0.6069 0.6070 -0.0185 1.2747 1.2746 1.2625 3000 15.510 15.510 0. 0.6441 0.6442 -0.0155 1.2626 1.2625 3260 15.445 15.445 0. 0.6972 0.6973 -0.0135 1.2493 1.2493 3262 1.2362 3490 15.347 15.347 0. 0.6824 0.8624 0.8626 -0.0135 1.2243 1.2243 3800 15.252 1.5025							0.4538	1.1335		0.0265
1800. 15.736 15.738 -0.0127 0.6576 0.6603 -0.4106 1.2897 1.2891 2000. 15.627 15.628 -0.0064 0.5784 0.5797 -0.1383 1.2974 1.2972 2200. 15.600 15.500 0. 0.5703 0.5707 -0.0701 1.2950 1.2929 2400. 15.558 15.588 0. 0.55827 0.5829 -0.0343 1.2950 1.2849 2600. 15.574 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 2800. 15.550 15.550 0. 0.6441 0.6442 -0.0155 1.2626 1.2625 3000. 15.550 15.550 0. 0.6441 0.6442 -0.0155 1.2626 1.2625 3000. 15.510 15.510 0. 0.6972 0.6973 -0.0143 1.2493 1.2493 3270. 15.445 15.445 0. 0.6972 0.6973 -0.0133 1.2626 1.2362 3490. 15.347 15.347 0. 0.6824 0.8626 -0.0232 1.2243 1.2243 3600. 15.220 15.210 0. 0.9770 0.9773 -0.0371 1.2845 1.2493 3800. 15.226 15.025 0.0067 1.1120 1.125 -0.0450 1.2074 1.2074 4000. 14.791 14.791 0. 1.2642 1.2647 -0.0366 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0366 1.2037 1.2017 1.2012			16.482		1.9/40_ n.9553	0.9494	-0.7542			0.0717
2000. 15,627 15,628 -n.0064 0.5784 0.5797 -0.1383 1.2974 1.2972 2200. 15,600 15,600 0. 0.5703 0.5707 -0.0701 1.2980 1.2980 2400. 15,588 15,588 0. 0.5827 0.5829 -0.0333 1.2850 1.2849 2600. 15,574 15,574 0. 0.0049 0.6070 -0.0155 1.2747 1.2746 2800. 15,550 15,550 0. 0.6441 0.6442 -0.0155 1.2026 1.2625 3000. 15,510 15,510 0. 0.6972 0.6973 -0.0143 1.2493 1.2493 3400. 15,347 15,347 0. 0.8624 0.8626 -0.0130 1.2243 1.2243 3800. 15,226 15,025 0.0067 1.1120 1.1125 -0.0372 1.2146 1.2146 1.2146 1.2074 4000. 14.791 14.791 0.0067 1.1120 <td< td=""><td></td><td></td><td></td><td>-0.0127</td><td></td><td>0.6603</td><td></td><td>1.2897</td><td>1.2891</td><td>9.0465</td></td<>				-0.0127		0.6603		1.2897	1.2891	9.0465
2400. 15,588 15,588 0. 0.5827 0.5829 -0.0343 1.2859 1.2849 2600. 15,574 15,574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 2800. 15,550 15,550 0. 0.60441 0.6442 -0.0155 1.2626 1.2625 3000. 15,510 15,510 0. 0.6972 0.6973 -0.0143 1.2493 1.2493 3200. 15,445 15,445 0. 0.7694 0.7695 -0.0130 1.2362 1.2362 3490. 15,347 15,347 0. 0.8624 0.8626 -0.0232 1.2243 1.2243 3600. 15,210 15,210 0. 0.9770 0.9773 -0.0307 1.2146 1.2145 3800. 15,026 15,025 0.0067 1.1120 1.1125 -0.0450 1.2074 1.2074 4000. 14.791 14.791 0. 1.2642 1.2647 -0.0396 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0367 1.2017 1.2012	2000.	15.627	15.628	-n.D064	0.5784	0.5792	-0.1383	1.2974	1.2972	0.0154
2600. 15.574 15.574 0. 0.6069 0.6070 -0.0165 1.2747 1.2746 2800. 15.550 15.550 0. 0.6441 0.6442 -0.0155 1.2626 1.2625 3000. 15.510 15.510 0. 0.6972 0.6973 -0.0155 1.2626 1.2625 3000. 15.415 15.445 0. 0.7694 0.7695 -0.0130 1.2493 1.2493 3200. 15.347 15.347 0. 0.6624 0.8626 -0.0282 1.2243 1.2243 3600. 15.210 15.210 0. 0.9770 0.9773 -0.0307 1.2243 1.2243 3600. 15.226 15.025 0.0067 1.1120 1.1125 -0.0450 1.2074 1.2074 4.000. 14.791 14.791 0. 1.2642 1.2647 -0.0306 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0356 1.2030 1.2030 4400. 14.174 14.173 0.0371 1.5911 1.5917 -0.0377 1.2017 1.2017				0	0.5703_					
2800. 15.550 15.550 0. 0.6441 0.6442 -0.0155 1.2625 1.2625 3000. 15.510 15.510 0. 0.6972 0.6973 -0.0143 1.2493 1.2493 3200. 15.445 15.445 0. 0.7694 0.7695 -0.0130 1.2362 1.2362 3400. 15.347 15.347 0. 0.8624 0.8626 -0.0232 1.2243 1.2243 3800. 15.210 15.210 0. 0.9770 0.9773 -0.0307 1.2146 1.2245 3800. 15.026 15.025 0.0067 1.1120 1.1125 -0.0307 1.2146 1.2074 4.000. 14.791 14.791 0. 1.2649 1.2647 -0.0396 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0356 1.2012 1.2012 4400. 14.174 14.173 0.0371 1.5911 1.5917 -0.0377 1.2017 1.2017					0.5827 0.6040					0.0078
3000. 15.510 15.510 0. 0.6972 0.6973 -0.0143 1.2493 1.2493 3200. 15.445 15.445 0. 0.7694 0.7695 -0.0130 1.2362 1.2362 3490. 15.347 15.347 0. 0.8624 0.8626 -0.0232 1.2243 3600. 15.210 15.210 0. 0.9770 0.9773 -0.0307 1.2146 1.2145 3800. 15.026 15.025 0.0067 1.1120 1.1125 -0.0450 1.2074 1.2074 4000. 14.791 14.791 0. 1.2642 1.2647 -0.0366 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0350 1.2012 1.2012 1400. 14.174 14.173 0.0071 1.5911 1.5917 -0.0377 1.2017 1.2017		15.55n	15.550		0.6441	0.6442				0.0079
3700. 15,445 15,445 0. 0.7694 0.7695 -0.0130 1.2362 1.2362 3490. 15,347 15,347 0. 0.8624 0.8626 -0.0232 1.2243 1.2243 3600. 15,210 15,210 0. 0.9770 0.9773 -0.0307 1.2146 1.2145 3800. 15.026 15.025 0.0067 1.1120 1.1125 -0.0450 1.2074 1.2074 4000. 14.791 14.791 0. 1.2649 1.2647 -0.0396 1.2030 1.2030 4290. 14.506 14.505 0.0069 1.4272 1.4277 -0.0356 1.2012 1.2012 4400. 14.174 14.173 0.0371 1.5911 1.5917 -0.0377 1.2017 1.2017		15.510	15.510	ρ.	0.6972	0.6973	-0.0143	1.2493	1.2493	n ·
3600. 15,210 15,210 0. 0.9770 0.9773 -0.0367 1.2146 1.2145 3600. 15,026 15.025 0.0067 1.1120 1.1275 -0.0450 1.2074 4000. 14.791 14.791 0. 1.2642 1.2647 -0.0366 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0350 1.2012 1.2012 4400. 14.174 14.173 0.0071 1.5911 1.5917 -0.0377 1.2017 1.2017	3200.	15.445	15.445	0.	8.7694	0.7695				n.
3800. 15.026 15.025 0.0067 1.1120 1.1125 -0.0450 1.2074 1.2074 4000. 14.791 14.791 0. 1.2642 1.2647 -0.0396 1.2030 4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0350 1.2012 1.2012 4400. 14.174 14.173 0.0371 1.5911 1.5917 -0.0377 1.2017 1.2017			15.347		0.8624	0.8626	-0.0232			0. n.0082
4000. 14.791 14.791 0. 1.2649 1.2647 -0.0396 1.2030 1.2030 4200. 14.506 14.505 0.0069 1.4972 14.277 -0.0350 1.2012 1.2012 4400. 14.174 14.173 0.0071 1.5911 1.5917 -0.0377 1.2017 1.2017				₽• 0-0047						0.0082
4200. 14.506 14.505 0.0069 1.4272 1.4277 -0.0350 1.2012 1.2012 4400. 14.174 14.173 0.0071 1.5911 1.5917 -0.0377 1.2017 1.2017						1.2647		1.2030	1.2030	0.
4400. 14.174 14.173 0.0371 1.5911 1.5917 -0.0377 1.2017 1.2017			14.505	0.0069	1.4272	1.4277	-0.0350	1.2012	1.2012	0.
	4200.		14.173	0.0371	1.5911					0.
4600. 13.804 13.803 0.0072 1.7425 1.7430 -0.0267 1.2044 1.2044 4800. 13.409 13.408 0.0075 1.8655 1.8661 -0.0322 1.2090 1.2091	4400.		13.603	0.0072	1 - 7425					0.0083
	4400. 4600.	13.804	4 2 4 4 4	0 0075						
5200. 12.613 12.612 0.0079 1.9746 1.9756 -0.0506 1.2229 1.2228	4400. 4600. 4800.	13.409	13.408	0.0075	1.8655					0.
5400. 12.244 12.242 0.0163 1.9539 1.9557 -0.0921 1.2311 1.2309 5600. 11.909 11.907 0.0168 1.8961 1.8991 -0.1582 1.2390 1.2386	4400. 4600. 4800. 5000.	13.804 13.409 13.006 12.613	13.005 12.612	0.0077	1.9456	1.9463 1.9756	-0.0360 -0.0506	1.2158	1.2153	

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JP-4/LOX	0/	F= 1.0 HOL WT	=MTA		(S OVER 1 NL/(MOL){	HAN ONE PERCINI	GAMMA (S)	
(K)	GORDON	BAHN	x	GORDON	BAHN	*	GORDON BAHN	*
600.	29.582	29,588	-0.0203	0.6906_	0.6906		1-1483 1-1479	
800. 1000.	25.075 17.581	25.100 17.626	-0.0997 -0.2560	2.0270 3.6065	2.0095 3.6230	0.8633 -0.4575	1.1180 1.1188	-0.0716 0.0355
1200. 1400.	15.373 15.186	15.378 15.187	-0.0325 -0.0066	0.8749	0.8842	-1.0630 + -0.1532	1.2410 1.2395 1.3018 1.3015	0-1209 9-0230
1600.	15.159	15.159	o.	0.5716	0.5720	-0.0700	1.3013 1.3011	0.0154
2000.	15.151	15.151. 15.142	0• 	0,5857	0.5859	-n.n341 -n.n321	1.2726 1.2725	0.0077
2200. 2400.	15.119	15.119	0. 0.0066	0.7033 0.8669	0.7039	-n.n853 -n.6921	1.2430 1.2428 1.2049 1.2036	0.0161 0.1079
2600.	14.940	14,936	0.0268	1.1689	1.2131	-3.7813 *	1.1671 1.1618	0.4541
2800. 	14.703	14.681	0.1496	1.6939	1.9254	-13.6667 • 0.7907	1.1863 1.1232	1.1529 + -0.0776
3200.	13.752	13.736	n,1163 n,0460	2.4794	2.4520 3.0496	1.1051 *	1.1548 1.1550	-n.06n6 -n.0346
3400. 3600.	13.052 12.277	13.046 12.280	-0.0244	3.0A15 3.5264	3.4953	1.0352 * 0.8819	1.1547 1.1551 1.1593 1.1595	-0.0173
3800. 4000.	11.526	10.896	0.0868 -0.1195	3.654n 3.4428	3.6290 3.4373	n.6842 n.1598	1.1669 1.1670 1.1768 1.1766	-0.0086 0.0170
4200.	10.385	10.396_	-0.1059	2.9921	_3.0164	-0.7886	1.1899 1.1891	n.0672
4400. 4600.	9.807	10.037 9.809	-0.0598 -0.0204	2.3757 1.7315	2.4071	-1.8430 + -1.0511 +	1.2114 1.2099 1.2474 1.2459	0.1238 0.1203
4800. 5000.	9.677	9.67R 9.602	-0.0103	1.2885 1.0942	1.2961	-n.6289 -n.4021	1.2910 1.2897 1.3159 1.3149	0.1007 0.0760
5200.	9.549	9.550	-0.0105	1-1089	1.1123	-0.3066	1.3002 1.2993	0.0692
5400. 5600.	9.499	9.499	0 <u>.</u>	1.7294	1.7343	-0.2873 -0.2833	1.2098 1.2091	0.0638
	0/1	F= 1.0	ATM=	10.				
600.	30.063	30.066	-0,0100	0.5248	0.5259	-0.2096	1.1623 1.1617	0.0516
1000.	28.203 22.652	28.216 22.702	-0.0461 -0.2207	1.0519 2.7622	1.0446 2.7368	0.7510 0.9196	1.1321 1.1329 1.1184 1.1186	-0.0707 -0.0179
1200. 1400.	16.942 15.508	16.973 15.514	-n.1830 -n.0387	2.3303 0.8728	2.3561	-1.1072 * -0.7676	1.1605 1.1597 1.2494 1.2484	0.0689 0.0800
1600.	15.256	15.257	-0.0066	0.6317	0.6326	-n.2218	1.2490 1.2886	0.0310
1800 • 2000 •	15.192 15.168	15.192 15.168	0. 0.	0.5983 0.6095	0.5989	-0.1003 -0.0328	1.2907 1.2900	0.0155 0.0078
2200.	15.152	15.152	0.	0.6495	0.6497	-0.0308	1.2591 1.2590	0.0079
2600.	15.130 15.008	15.130 15.087	D. D.NA66	0.7303 0.8735	0.7320 0.8878	-0.2328 -1.6371 =	1.2298 1.2292 1.1952 1.1922	0.0488 0.2510
2800. 3000.	15.009	15.002 14.85	0.0466 0.1211	1.1096	1.1877	-7.0386 - -0.5952	1.1413 1.1522 1.2004 1.2005	n.7836 -n.0083
3200.	14.657	14.636	0.1483	1.2757	1.2746	0.0862	1.1869 1.1876	-0.0590
3400. 3600.	14.355	14.336	0.1324	1.5648	1.5554	0.6007 0.8655	1.1785 1.1793 1.1746 1.1753	-0.0679 -0.0596
3800. 4000.	13.473 12.922	13.464 12.921	0.0668 0.0077	2.2395 2.558A	2.2189 2.5363	0.9198 0.8716	1.1744 1.1750 1.1770 1.1774	-0.0511 -0.0340
4200.	12.342	12,346	-0.0324	2.8040	2.7821	0.7810	1.1817 1.1821	-0.0338
4400.	11.771 11.246	11.78c 11.256	-0.0765 -0.0889	2.9314 2.9146	2.9143	0.5833 0.1784	1.1882 1.1884 1.1963 1.1962	-0.0168 0.0084
4800. 5000.	10.791 10.422	10.801	-0.0927 -0.0672	2.7458 2.4371	2.7574	-0.4225 -0.9232	1.2068 1.2061 1.2213 1.2201	Ი.0580 Ი.0983
5200.	10.142	10.146	-0.0394	2.0486	2.0694	-1.0153 ·	1.2408 1.2393	0.1209
5400. 5600.	9.942	9.801	0.0101 0.	1.6926	1.7065	-0.6836	1.2628 1.2612 1.2778 1.2760	0.1267
JP-4/LOX -	0/1	F= 1.0	ATH=	100. • 1				
TEMP		F= 1.0 MOL WT		CP CA	S DVER TO	HAN OHE PERCINT	GAMMA (S)	
TEMP (K)	GORDON	HOL WY BAHN	¥		S OVER TO	HAN ONE PERCINT		*
TEMP (K) 690.	GORDON 30.223	HOL WT BAHN 30.224	¥ -0.0988	GP CA GORDON 0.4702	S OVER TO	HAN ONE PERCINT K) \$ -0.2977	GAMMA (S) GORDON BAMN 1.1692 1.1685	0.0599
TEMP (K) 690. 800. 1000.	GORDON 30.223 29.579 27.121	80L WT BAHN 37.224 29.585 27.149	-0.033 -0.0203 -0.1632	GP CA GORDON 0.4702 0.6708 1.3333	S OVER TO HAHN D.4716 0.6663 1.3207	HAN ONE PERDINT K) 5 -0.2977 0.6708 0.9450	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.453 1.1250 1.1254	0.0599 -0.0786 -0.0356
TEMP (K) 690. 800.	GORDON 30.223 29.579	80L WT BAHN 30.224 29.585	-0.033 -0.0203	CP CA GORDON 0.4702 0.6708	S DVER TO PAHN D.4716 0.6663	HAN OHE PERCINT K) 3 -0.2977 0.6708	GAMMA (S) GORDON RAMN 1.1692 1.1685 1.1444 1.1453	0.0599
TEMP (K) 690. 800. 1000. 1200. 1400.	GORDON 30.223 29.579 27.121 22.022 17.683 16.067	MOL WT BAHN 39.224 29.585 27.149 22.079 17.716 16.078	-0.0203 -0.0203 -0.1032 -0.2588 -0.1866 -0.0685	CP CA GORDON 0.4702 0.6708 1.3333 2.4639 1.9523 1.9461	D.4716 0.6663 1.3207 2.4537 1.9681 1.0535	HAN OHE PERCINT K) 3 -0.2977 0.6708 0.9450 0.4140 -0.8098 -0.7074	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1244 1.1453 1.1251 1.1218 1.1762 1.1754 1.2356 1.2356 1.2357	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728
TEMP (K1) 690. 1000. 1200. 1400. 1600. 1800.	GORDON 30.223 29.579 27.121 22.022 17.683 16.067 15.550	MOL WT BAHN 39.224 29.585 27.149 29.079 17.716 16.078 15.555 15.358	-0.033 -0.0203 -0.1032 -0.2588 -0.1866 -0.0685 -0.0322 -0.0130	CP CA GORDON 0.4702 0.670R 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642	D.4716 0.4663 1.3207 2.4537 1.9681 1.0535 0.7474 0.6654	HAN OHE PERCINT X -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807	GAMMA (S) GORDON BAMN 1.1692 J.1685 1.1444 1.1453 1.1250 1.1254 1.1762 1.1754 1.2356 1.2347 1.2686 1.2679 1.2730 1.2731	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552
TEMP (K1) 690. 800. 1000. 1200. 1400. 1600. 1600. 2000. 2200. 2400.	GORDON 30.223 29.579 27.121 22.022 17.683 16.067 15.550 15.269 15.221	MOL WT BAHN 39.224 29.585 27.149 22.079 17.716 16.078 15.555	4 -0.0033 -0.0203 -0.1032 -0.2588 -0.1866 -0.0685 -0.0322	CP CA GORDON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447	D.4716 0.6663 1.3207 2.4537 1.9681 1.0535 0.7474	MAN ONE PERDINT K) * -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1250 1.1254 1.1321 1.3318 1.1762 1.1754 1.2356 1.2347 1.2666 1.2679	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552 0.0471 0.0555
TEMP (K1) 690. 800. 1000. 1200. 1400. 1400. 1400. 2000. 2200. 2400.	GORDON 30.223 29.579 27.121 22.022 17.683 16.067 15.356 15.269 15.221 15.186	#OL WT RAHN 37.224 29.585 27.149 27.079 17.716 16.078 15.555 15.358 15.271 15.224 15.189	-0.0933 -0.0203 -0.1032 -0.12588 -0.1866 -0.0352 -0.0352 -0.0193 -0.0197 -0.0198	GP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 2.6604 0,7019 0.7879	D. 4716 0.6663 1.3207 2.4537 1.9535 0.7474 0.6654 0.6611 0.7939	HAN ONE PERCINT K) 3 -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1251 1.1254 1.1762 1.1754 1.1762 1.1754 1.2356 1.2047 1.2686 1.2679 1.2730 1.2724 1.2609 1.2602 1.2777 1.2655 1.2013 1.2025	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552 0.0471 0.0555
TEMP (K1) 690. 800. 1200. 1200. 1400. 1600. 1600. 2200. 2200. 2400. 2690. 2800. 3000.	GORDON 30,223 29,579 27,121 22,022 17,683 16,067 15,756 15,756 15,269 15,148 15,198	MOL WT RAHN 37.224 29.585 27.149 22.079 17.716 16.078 15.555 15.358 15.271 15.224 15.189 15.190	-0.0933 -0.0203 -0.1632 -0.2588 -0.1866 -0.0685 -0.0382 -0.0382 -0.0197 -0.0198 -0.0198 -0.0199	CP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 0.6604 0.7019 0.7879 0.9263 0.7653	D. 4716 0.6663 1.3207 2.4537 1.9681 1.0535 0.7474 0.6651 0.7030 0.7939 0.7939	HAN OHE PERCINT (x) -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 +1.0453	GAMMA (S) GORDON BAMN 1.1692 J.1685 1.1444 1.1453 1.1250 1.1254 1.1321 1.1318 1.1762 1.1754 1.2356 1.2347 1.2686 1.2679 1.2730 1.2724 1.2609 1.2602 1.2737 1.3655 1.2073 1.2045 1.1752 1.1685 1.2368 1.2347	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552 0.0471 0.0555 0.0970 0.2319 0.5701 0.0647
TEMP (K1) 670. 800. 1000. 1200. 1400. 1600. 1400. 2000. 2200. 2400. 2600. 2800.	GORDON 30.223 29.579 27.121 22.022 17.683 16.067 15.356 15.356 15.356 15.269 15.2186	#OL WT RAHN 37.224 29.585 27.149 22.079 17.716 16.078 15.555 15.271 15.224 15.151	-0.0933 -0.0203 -0.1232 -0.2588 -0.1866 -0.0685 -0.0322 -0.0130 -0.0197 -0.0199	CP CA GORNON D. 4702 Q. 6708 1. 3333 2. 4639 1. 9523 1. 0461 Q. 7447 Q. 6642 2. 6604 Q. 7019 G. 7879 Q. 9263	D. 4716 0.6663 1.3207 2.4537 1.9681 1.0535 0.7474 0.6661 0.7039 0.7939	MAN ONE PERCINT K) 2 -0.2977 -0.6708 -0.9450 -0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1250 1.1254 1.1321 1.3318 1.1762 1.1754 1.2356 1.2347 1.2686 1.2347 1.2686 1.2347 1.2686 1.2347 1.2680 1.2679 1.2730 1.2724 1.2609 1.2602 1.2377 1.2365 1.2073 1.2045 1.1759 1.1685	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552 -0.0471 0.0555 0.0970 0.2319
TEMP (K1) 690. 1000. 1200. 1400. 1600. 1600. 2200. 2200. 2400. 2600. 3000. 3299. 3400.	GORDON 30,223 29,579 27,121 22,022 16,067 15,556 15,269 15,146 15,148 15,013 14,752	MOL WT GAHN 301.224 29.585 27.149 29.079 17.716 16.078 15.358 15.271 15.358 15.274 15.189 15.190 15.090 14.870 14.870	-0.0933 -0.0203 -0.1032 -0.2588 -0.1866 -0.0685 -0.0322 -0.0130 -0.0197 -0.0198 -0.0199 -0.0533 -0.0805	GP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 0.6604 0.7019 0.9263 0.7653 0.8410 0.9423 1.0674	S OVER TILL/(HOL)(I) RAHN D.4716 0.6663 1.3207 2.4537 1.9681 1.0535 0.7474 0.6611 0.7039 U.9562 0.7733 0.8477 0.9466 1.0682	HAN OHE PERCINT X -0.2977	GAMMA (S) GORDON BAMN 1.1692	0.0599 -0.0786 -0.0356 0.0265 0.0680 0.0728 0.0552 0.0471 0.0555 0.0970 0.2319 0.5701 0.0647 0.0327 -0.0382
TEMP (K1) 690. 800. 1200. 1400. 1400. 1600. 2200. 2400. 2600. 2800. 3000. 3100. 3600. 3800.	GORDON 30, 223 29, 579 27, 121 22, 022 17, 683 16, 067 15, 756 15, 756 15, 756 15, 186 15, 188 15, 193 14, 193 14, 193 14, 193 14, 195 14, 309	MOL MT RAHN 30.224 27.149 27.161 16.075 15.358 15.271 15.224 15.189 15.005 14.738 14.738 14.295	-0.0933 -0.1632 -0.1632 -0.1636 -0.0685 -0.0332 -0.0130 -0.0197 -0.0198 -0.0199 -0.0533 -0.0949 -0.0949 -0.0949 -0.0949	CP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 0.6604 0.7019 0.7879 0.9263 0.7653 0.8410 0.9423 1.0674 1.2135	S OVER TILL (HOL) (I RAHN D. 4716 O. 6663 T. 1.9585 O. 74584 O. 6613 O. 7939 U. 9562 O. 7733 C. 8477 O. 9466 1. 0682 1. 2102 1. 3593	HAN OHE PERCINT (x) 3 -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.749 0.2719 0.5375	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1250 1.1254 1.1762 1.1754 1.1762 1.1754 1.2356 1.2347 1.2686 1.2347 1.2686 1.2767 1.2730 1.2724 1.2609 1.2202 1.2737 1.2365 1.2073 1.2045 1.1752 1.1685 1.2747 1.243 1.2140 1.2141 1.2056 1.2060 1.1997 1.2003 1.1902 1.2003	0.0599 -0.0786 -0.0786 0.0265 0.0680 0.0728 0.0552 0.0471 0.0555 0.0970 0.2319 0.5701 0.0647 0.0327 -0.0082 -0.0332 -0.0585
TEMP (K1) 670. 800. 1000. 1200. 1400. 1600. 1400. 2000. 2200. 2400. 2600. 3000. 3229. 3400. 3600.	GORDON 30,223 29,579 27,121 22,022 17,683 16,067 15,356 15,269 15,186 15,186 15,193 14,1902 14,752	MOL WT GAHN 37.224 29.285 27.149 22.716 16.078 15.358 15.271 15.224 15.189 15.189 15.4890 14.738	4 -0,0933 -0.1032 -0.1258 -0.1258 -0.1666 -0.1665 -0.0352 -0.0150 -0.0198 -0.0198 -0.0198 -0.0198 -0.0198 -0.0165 -0.0949 -0.1651	CP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 2.6604 0.7019 0.7879 0.7853 0.8410 0.9423 1.0674	D. 4716 0.6663 1.3207 2.4537 1.0535 0.7474 0.6611 0.7039 0.7939 0.7939 0.7939 0.9562 0.7474 0.6611 0.7939 0.9562 0.7474	HAN OHE PERCINT (x) 3 -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.749 0.2719 0.5375	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1250 1.1254 1.1321 1.1318 1.1762 1.1754 1.2356 1.2347 1.2686 1.247 1.2686 1.2247 1.2686 1.2269 1.2730 1.2724 1.2609 1.2602 1.2777 1.2365 1.1752 1.1685 1.2354 1.2356 1.2354 1.2356 1.2364 1.2356 1.2364 1.2356 1.2364 1.2356 1.2364 1.2356 1.2364 1.2356 1.2365 1.2060 1.1997 1.2063	0.0599 -0.0786 -0.0265 0.0680 0.0728 0.0552 -0.0471 0.0555 0.0970 0.2319 0.5701 0.0647 0.0327 -0.0327 -1.0082
TEMP (K1) 690. 800. 1200. 1200. 1400. 1600. 2200. 2200. 2400. 2600. 2800. 3000. 3299. 3400. 4000. 4400.	GORNON 30,223 29,579 27,121 22,022 16,067 15,550 15,269 15,261 15,148 15,148 15,013 14,002 14,752 14,359 14,013 13,672 13,295	MOL MT RAHN 301.224 27.149 27.716 16.075 15.358 15.271 15.189 15.189 15.005 14.540 14.540 14.541 14.541 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545 14.545	-0.0933 -0.0203 -0.1632 -0.2588 -0.0685 -0.0352 -0.0130 -0.0197 -0.0198 -0.0199 0.0533 -0.0949 0.1531 0.0785 0.0785 0.0785	CP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 0.7019 0.7879 0.9263 0.7653 0.8410 0.9423 1.0674 1.2135 1.3767 1.5510 1.79015	S OVER TO THE TOTAL THE TOTAL TO THE TOTAL TO THE T	HAN ONE PERCINT (x) 3 -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.7750 0.7836	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1251 1.1254 1.1321 1.1318 1.1762 1.1754 1.2356 1.2347 1.2686 1.2347 1.2686 1.2347 1.2686 1.2356 1.2737 1.2365 1.2737 1.2365 1.2737 1.2365 1.2737 1.2365 1.2747 1.243 1.2140 1.2141 1.2036 1.2040 1.1997 1.2033 1.1962 1.1963 1.1950 1.1957 1.1957 1.1963	0.0599 -0.0786 -0.0265 0.0265 0.0680 0.0728 0.0552 0.0477 0.0552 0.0477 0.0327 -0.0082 -0.0586 -0.0586 -0.0586 -0.0586 -0.0586
TEMP (K1) 690. 800. 1200. 1200. 1400. 1600. 1600. 2200. 2400. 2600. 2800. 3000. 3600. 3600. 3600. 4700. 4400. 4600. 4800. 5000.	GORDON 30, 223 29, 579 27, 121 22, 022 17, 683 16, 067 15, 756 15, 756 15, 756 15, 766 15, 186 15, 193 15, 013 14, 752 14, 752 14, 555 14, 013 13, 672 13, 295 12, 479	MOL MT MAHN 4 29.581 221.140 22.716 16.075 15.358 15.271 15.005 15.489 15.495 14.545 14.545 14.605 13.293 12.8484	-0.0933 -0.0203 -0.1632 -0.2588 -0.0685 -0.0332 -0.0130 -0.0197 -0.0198 -0.0199 -0.0533 -0.0949 -0.0785 -0.0785 -0.0785 -0.0785 -0.0150	CP CA GORRON 0.4702 1.3333 2.4639 1.9461 0.7447 0.6642 0.6642 0.7019 0.7879 0.9263 0.7653 0.8410 0.9423 1.0674 1.2135 1.3767 1.5510 1.790 1.9015 2.0577 2.1857	S OVER TO VER TO	HAN OHE PERCINT () 3 -0.2977 0.6708 0.9450 0.4140 -0.8093 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.7967 -0.4563 -0.7750 0.7636 0.7750 0.7636	GAMMA (S) GORDON BAMN 1.1692 J.1685 1.1444 1.1453 1.1251 1.1254 1.1321 1.1318 1.1762 1.1754 1.2356 1.2347 1.2686 1.2679 1.2730 1.2724 1.2609 1.2602 1.277 1.2365 1.2073 1.2045 1.1752 1.1685 1.2347 1.2243 1.2140 1.2141 1.2056 1.2060 1.1997 1.2003 1.1962 1.1969 1.1950 1.1957 1.1957 1.1957 1.1957 1.1968 1.2014 1.2018 1.2014 1.2018	0.0599 -0.0786 -0.0265 0.0680 0.0728 0.0552 -0.0471 0.0555 0.0970 0.2319 0.0647 0.0327 -0.0082 -0.0550 -0.0586 -0.0586 -0.0586 -0.0582 -0.0583 -0.0586
TEMP (K1) 670. 800. 1000. 1200. 1400. 1600. 1400. 2000. 2200. 2400. 2600. 3000. 3100. 3100. 3600. 3400. 3600. 4700. 4400. 4600.	GORDON 30, 223 29, 579 27, 121 22, 022 17, 683 16, 067 15, 356 15, 269 15, 186 15, 198 15, 198 15, 101 14, 1555 14, 309 14, 1555 14, 309 13, 672 13, 295	MOL WT GAHN 429.584 27.149 29.716 16.078 15.358 15.271 15.189 15.191 14.738 14.741 14.295 13.693 12.894 12.075	-0.0933 -0.0203 -0.1632 -0.2588 -0.1866 -0.0685 -0.0322 -0.0130 -0.0197 -0.0199 -0.0533 -0.0949 -0.0533 -0.0949 -0.0785 -0.0778 -0.0778 -0.0778	CP CA GORNON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 2.6604 0.7019 0.7879 0.7853 0.8410 0.9423 1.0674 1.2135 1.3767 1.5510 1.7790 1.9015 2.0577	S OVER TO VER TO	HAN OHE PERCINT () 3 -0.2977 0.6708 0.9450 0.4140 -0.8098 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.7967 -0.4563 -0.7750 0.6963 0.7750 0.7836 0.7338 0.6131 0.3915	GAMMA (S) GORDON BAMN 1.1692 1.1685 1.1444 1.1453 1.1250 1.1254 1.1321 1.1318 1.1752 1.2757 1.2686 1.2247 1.2686 1.2247 1.2686 1.2247 1.2609 1.2002 1.2777 1.2365 1.2777 1.2685 1.2777 1.2685 1.2777 1.243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2140 1.2243 1.2159 1.1967 1.1967 1.1968 1.1957 1.1968 1.1957 1.1968 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018 1.2014 1.2018	0.0599 -0.0786 -0.0786 -0.0265 0.0680 0.0728 0.0552 0.0471 0.0555 0.0970 0.2319 0.5701 0.0647 0.0327 -0.0082 -0.0332 -0.0566 -0.0570 -0.0586 -0.0570 -0.0586 -0.0570 -0.0333 -0.0417 -0.0333
TEMP (K1) 690. 800. 1200. 1200. 1400. 1600. 2200. 2200. 2400. 2600. 3000. 3600. 3800. 4000. 4400. 4600. 4800. 5000.	GORNON 30,223 29,579 27,121 22,022 16,067 15,550 15,550 15,269 15,146 15,148 15,018 14,752 14,555 14,309 14,013 13,672 12,893 12,479	MOL MT MAHN 4 29.581 27.140 27.716 16.075 15.358 15.274 15.189 15.005 14.738 14.545 14.005 13.298 12.8484	-0.0933 -0.0203 -0.1632 -0.2588 -0.0685 -0.0332 -0.0130 -0.0197 -0.0198 -0.0199 -0.0533 -0.0949 -0.0785 -0.0785 -0.0785 -0.0785 -0.0150	CP CA GORRON 0.4702 0.6708 1.3333 2.4639 1.9523 1.0461 0.7447 0.6642 0.6604 0.7879 0.9263 0.8410 0.9423 1.0674 1.2135 1.3767 1.5510 1.7290 1.9015 2.0577 2.1857 2.1857	S OVER TO VER TO	HAN OHE PERCINT () 3 -0.2977 0.6708 0.9450 0.4140 -0.8098 -0.7074 -0.3626 -0.1807 -0.1060 -0.1567 -0.7615 -3.2279 -1.0453 -0.7967 -0.4563 -0.7967 -0.4563 -0.7750 0.6963 0.7750 0.7836 0.7338 0.6131 0.3915	GAMMA (S) GORDON BAMN 1.1692 J.1685 1.1444 1.1453 1.1251 1.1254 1.1321 1.1318 1.1762 1.1754 1.2356 1.2347 1.2686 1.2679 1.2730 1.2724 1.2609 1.2602 1.277 1.2365 1.2073 1.2045 1.1752 1.1685 1.2347 1.2243 1.2140 1.2141 1.2056 1.2060 1.1997 1.2003 1.1962 1.1969 1.1950 1.1957 1.1957 1.1957 1.1957 1.1968 1.2014 1.2018 1.2014 1.2018	0.0599 -0.0786 -0.0265 0.0680 0.0728 0.0552 -0.0471 0.0555 -0.970 0.2319 0.5701 0.0647 9.0327 -0.0082 -0.0585 -0.0586 -0.0586 -0.0586 -0.0582 -0.0417 -0.0333 -0.0166 0.0032
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JP-4/L(/F= 0.8 HOL WT	ATH	10. • 1	S OVER T	HAN ONE PERCI	NT GA	MMA (S)	
(X) GORDON	BAHN		GORDON	BAHN		GORDON	BAHN	<u> </u>
600		29.861	-0.0067	0.5509	0.5512	-0.0545	1.1563	1.1560	0.0259
1000		27.885 22.342	-0.0574 -0.2153	1.1011 2.7352	1.0940 2.7131	0.6448 0.8080	1.1295	1.1301 '	-0.0531 -0.0179
1200	. 16.630	16.859	-0.1723	2.2563	2.2790	-1.0061 -	1.1602	1.1595	0.0403
1400 1600		<u>15.443_</u> 15.179	-0.0389 -0.0132	0.9090	0.9150	-0.6601 -0.1920	1.2872	1.2365	0.0566
1800	15,108	15.109	-0.0066	0.6448	0.6453	-0.0775	1.2661	1.2660	0.0079
2000 2200		15.082 15.065	0.	0.6574 0.7009	0.6576	-n.0304 -0.0285	1.2558	1.2557	0.0080
2400	. 15.041	15.041	0.	0.7884	0.7903	-0.2410	1.2112	1.2107	0.0413
2600 2800		14.996	0.0469	1.1986	0.9588	-1.6216 • -6.9331 •	1.1495	1.1773	0.2288 D.7134
3000			0.2438	2.2247	1.9494	-21.7842 -	1.1240	1.1071	1.5036 +
3200. 3490.		14.421 14.088	0.6202 9.4593	1.7662	1.4220	36.0813 • 2.5422 •	1.1047	1,1761	-6.4633 • -0.2312
3600. 3800.		13.664	0.32A3 ` 0.1594	2.1377 2.5264	2.0703	3.1529 • 3.1349 •	1.1655	1.1677 _1.1681_	+n.1888 -n.1457
4000	. 12.576	12.578	-0.0159	2.8989	2.8168	2.4321 •	1.1694	1.1706	-0.1026
4200 4490		11.369	-0.1758 -0.3179	3,2160 3,4422	3.1376	2.4378 •	1.1789	1.1746	-0.0682 -0.9339
4600	. 10.744	16.786	-ŋ.39n9	3,5545	3.5211	0.9397	1.1846	1.1844	0.0169
4800. 5000		10.264 9.810	-0.4011 -0.3375	3.5324 3.3428	3,5510 3,4118	-0.5266 -2.0641 +	1.1913	1.1902	0.0923 0.1749
5200	. 9,417	9.438	-0.2230	2.9654	3.0508	-2.8799 *	1-2141	1.2113	0.2306
5400. 5600.		9.157 8.959	-0.1312 -0.0670	2.4632 1.9807	2.550 <u>0</u> 2.0223	-2.7119 ·	1.2341	1.2561	0.2512
		/F= 0.8		100.					
600		30.037	-0.0033	0.4907	0.4915	-0.1630	1.1627	1.1624	0.0258
800. 1020.	. 29.346	29.353 26.872	-0.0239 -0.1343	0.7037	0.7000	0.5258 0.8864	1.1392	1.1398	-0.0527
1200	. 21.873	21.926	-0.2423	2.4023	2.3934	0.3705	1.1228	1.1332 1.1301	0.0265
1400. 1600.		17.710 16.067	-n.1753	1.9263	1.9399	-0.7060	1.1724	1.1716	0.0682
1800	. 15.509	15.514	-0.0747 -0.0322	1.0913 0.7988	0.8015	-n.6323 -0.8380	1.2735	1.2227	0.0654
2000. 2200.		15.299 15.201	-0.0196 -0.0132	0.7172	0.7185 0.7149	-0.1813 -0.1120	1.2505	1.2498	0.0560 0.0646
2400	. 15.145	15.148	-0.0198	0.7595	0.7609	-0.1843	1.2387	1.2379	0.1150
2600. 2800.		15.110 15.068	-0.0331 -n.0266	9.8537 1.9050	0.8604 1.0372	-n.7848 -3.2040 *	1.1896	1.1867 1.1540	0.2436 0.5515
3000	. 15.006	15.004	0.0133	1.2236	1.3518	-10.4773 •	1.1343	1.1217	1.1108 .
3200. 3496.		14.88t 14.73n	1.2280 0.3316	1.5210 1.0514	1.9517	-28.3169 • -1.0938 •	1.1139 1.197n	1.0933	1.8494 +
3690	. 14.604	14.549	0.3766	1.1956	1.1918	0.3178	1.1007	1.1923	-0.1680
3890. 4000-		14.323	0.3825 0.3334	1.3629 1.5485	1.3433	1.4381 • 2.1828 •	1.1861 1.1841	1.1885 1.1864	-0.2023 -0.1942
4200	. 13.766	13.732	0.2470	1.7470	1.7021	2.5701 •	1.1840	1.1861	-n.1774
44 ባብ . 46 ፀብ .		13.369	0.1419 0.0308	1.9522 2.1574	1.9000 2.1012	2.6739 = 2.6050 =	1.1854	1.1871	-0.1434 -0.1179
4890.	. 12.531	12.541	-n.0798	2.3548	2.2978	2.4206 •	1.1913	1.1924	-0.0923
5010. 5210.		12.098 11.652	-0.1822 -0.2754	2.5347 2.6859	2.4815 2.6429	2.0989 ● 1.6010 ●	1.1953 1.2000	1.1961	-0.0669 -0.0250
5400.	. 11.176	11.213	-0.3311	2.7945	2.7703	0.8660	1.2055	1.2051	0.0332
5 6 00.	. 1n.755	19.792	-0.3440	2.8449	2.8469	-0.1020	1.2119	1.2107	0-0990
JP-4/L		/F= 0.6	ATH			HAN ONE PERCI		MMA (C)	
JP-4/LI TEM	P	HOL HT	ATH:		IS OVER 1 AL/(MOL)(BAHN			INMA (S) Bahn	<u> </u>
TEH (K	P) GORDON	HOL HT		CP C/ GORDON	AL/(MOL)(BAHN	K)	GORDON	BAHN	
600 600	P GORDON . 29.004 . 23.904	9.012 23.935	-0.0276 -0.1297	0.7867 2.1976	0,7843 2.1843	0.3051 0.6052	GORDON 2.1387	1,1888 1,1191	-0.0088 -0.0358
TEM (K	P GORDON . 29.004 . 23.904 . 16.994 . 15.168	29.012 23.935 17.029	-0,0276	CP C/ GORDON 0,7867	0.7843	(K) % 0.8051	GORDON 1.1387	BAHN 1,1888	-0.0088 -0.0358 0.0354
75M (K 600 800 1000 1200	P GORDON 29.004 23.904 16.994 15.166 14.992	29.012 23.935 17.029 15.172 14.993	-0.0276 -0.1297 -0.2060 -0.0264 -0.0067	CP C/ GORDON 0,7867 2.1976 3.1624 0.9138 0.6812	AL/(MOL)(BAHN 0.7843 2.1843 3.1795 0.9202 0.6819	0.3051 0.6052 -0.5407 -0.7004 -0.1028	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537	BAHN 1,1388 1,1191 1,1293 1,2220 1,2535	-0.0088 -0.0358 0.0354 0.0573 0.0160
TEM (K 600 800 1000 1200 1400 1600	P GORDON . 29.004 . 23.904 . 16.994 . 15.166 . 14.992 . 14.963	29.012 23.935 17.029 15.172 14.993 14.963	-0,0276 -0.1297 -0.2060 -0.0264	CP C/ GORDON 0.7867 2.1976 3.1624 0.9138	0.7843 2.1843 3.1795 0.9202	0.3051 0.6052 -0.9407 -0.7004	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537	1,1388 1,1191 1,1293 1,2220 1,2535 1,2502	-0.0088 -0.0358 0.0354 0.0578
7EM (K 600 800 1000 1200 1400 1600 1800 2000	P GORDON 29.004 23.904 16.994 15.166 14.963 14.963	29.012 23.935 17.029 15.172 14.993 14.963 14.954	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0.	CP C/ GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308	0.7843 2.1843 3.1795 0.9202 0.6819 0.7310	0,3051 0.6052 -0.5407 -0.7004 -9.1028 -0.0448 -0.0436 -0.0274	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2503 1.2416 1.2271	BAHN 1,1388 1,1191 1,1293 1,2220 1,2535 1,2502 1,2415 1,2271	-0,0088 -0.0358 0.0354 0.0578 0.0160 0.0080 0.0081
TEM (K 600 800 1000 1200 1400 1600	P GORDON . 29,004 . 23,904 . 16,994 . 15,168 . 14,992 . 14,963 . 14,953 . 14,954 . 14,954	МОL WT ВАНН 29.012 23.935 17.029 15.172 14.993 14.963 14.954 14.943 14.943 14.956	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0.	CP C/ GORDON 0.7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.6251	0.7843 2.1843 3.1795 0.9202 0.6819 0.6705 0.6881	0,3051 0.6052 -0.5407 -0.7004 -0.1028 -0.0448 -0.0486	QORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2503 1.2416 1.2271 1.2042	BAHN 1,1888 1,1191 1,1293 1,2220 1,2535 1,2502 1,2415 1,2271 1,2041	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.
7EW (K 600 800 1200 1400 1600 1800 2200 2400 2400	P GORDON 29,004 23,904 16,994 15,166 14,992 14,963 14,954 14,943 14,943 14,943 14,943 14,943 14,721	HOL N7 BAHN 29.012 23.935 17.025 15.172 14.993 14.954 14.954 14.954 14.918 14.818 14.856	-0.0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0.	CP C/ GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.8878 0.7308 0.8251 1.0148	0.7843 2.1843 3.1795 0.9202 0.6819 0.6705 0.6881 0.7310 0.0258 1.0217 1.4140	0.3051 0.6052 -0.9407 -0.7004 -0.1028 -0.0436 -0.0274 -0.0848 -0.0779 -3.6635	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2533 1.2416 1.2271 1.2042 1.1746 1.1449	BAHN 1,1888 1,1191 1,1293 1,2220 1,2535 1,2502 1,2415 1,2271 1,2041 1,1736 1,1407	-0,0088 -0.0358 0.0354 0.0578 0.0160 0.0080 0.0081 0.0083 0.0851 0.3668
TEM (K 600 800 1000 1200 1200 1400 1600 2000 2200 2200 2400 2600 3000	P GORDON . 29,004 . 23,904 . 16,994 . 15,166 . 14,962 . 14,963 . 14,954 . 14,914 . 14,914 . 14,166 . 14,1721 . 14,461 . 14,461 . 14,461 . 14,461 . 14,461	MOL N7 BAHN 29,012 23.935 17.029 15.172 14.993 14.994 14.943 14.918 14.856 14.717 14.437	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0. 0. 0. 0. 0. 0. 0. 0.1660 0.7710	CP C. GORDON 0.7867 2.1976 3.1624 0.9138 0.6612 0.6702 0.6878 0.7308 0.8251 1.0148 1.3648 1.9739 3.0071	AL/(NOL) BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.6705 0.6881 0.73310 0.8258 1.0217 1.4148 2.2376	0,3051 0,6052 -0,9407 -0,7004 -9,1028 -0,0436 -0,0436 -0,0274 -0,0848 -0,635 -13,3593 -36,6846	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2503 1.2416 1.271 1.2042 1.1746 1.1449 1.1204	BAHN 1,1388 1.1191 1,1293 1.2220 1,2535 1.2502 1,2415 1.2271 1.1736 1,1407 1.1095	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0083 0.0083
7 EM (K 600 1000 1200 1400 1600 2000 2400 2400 2800 3000 3200	P GORDON 29,004 123,904 16,994 15,166 14,992 14,963 14,953 14,953 14,954 14,918 14,816 14,816 14,461 14,461 14,461 14,461	MOL N7 BAHN 29.012 23.935 17.029 15.172 14.993 14.963 14.963 14.963 14.918 14.943 14.856 14.737 14.437 13.007	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0.710 1.4607	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.67308 0.8878 0.7308 0.8251 1.0148 1.9739 3.0071 4.7613	AL/(MOL) BAHN 0,7843 2,1843 3,1795 0,9202 0,6819 0,6705 0,6881 0,7310 0,0258 1,0217 1,4148 2,2376 4,0922 2,9785	8 0,3051 0.6052 -0.5407 -0.7004 -0.1028 -0.0448 -0.0456 -0.0274 -0.0848 -0.6799 -3.6655 -13.3593 -36.0846 -37.7471	GORDON 1.1387 1.1187 1.1297 1.2227 1.2557 1.2503 1.2416 1.2271 1.2042 1.1746 1.1018 1.0874	BAHN 1,1888 1.1191 1.1293 1.2220 1.2535 1.2525 1.22415 1.2271 1.2041 1.1736 1.1407 1.1095 1.0820 1.1438	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0083 0.0851 0.3668 0.9729 1.7971 -5.1867
TEM (K 600 800 1200 1200 1400 1600 2000 2200 2400 2800 3000 3200 3400	P GORDON 29,004 . 23,904 . 16,994 . 15,166 . 14,962 . 14,963 . 14,954 . 14,914 . 14,918 . 14,216 . 14,461 . 14,461 . 14,461 . 14,168 . 13,281 . 12,329 . 11,434	MOL N7 BAHN 29.029 23.935 17.029 15.172 14.993 14.963 14.954 14.954 14.954 14.954 14.326 14.717 14.437 13.900 13.087 12.326	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0, 0, 0, 0, 0, 0, 1,660 0,7710 1,4607 0,0243	CP C: GORDON 0.7867 2.1976 3.1624 0.9138 0.6612 0.6702 0.6878 0.7308 0.8251 1.0148 1.9739 3.0071 4.7813 3.9632 4.5899	AL/(NOL) BAHN 0.7843 3.1795 0.9202 0.6819 0.6705 0.6881 0.73310 0.8258 1.0217 1.1148 2.2376 2.2376 3.7191 4.3685	0,3051 0,6052 -0,9407 -0,7004 -0,1028 -0,0436 -0,0436 -0,0274 -0,0848 -0,6635 -13,3559 -3,6635 -3,0846 -3,7471 -6,1592 -4,8238	G/RDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2503 1.2416 1.2271 1.2042 1.7746 1.449 1.1018 1.0874 1.1434 1.1435	BAHN 1.1888 1.1191 1.1293 1.2220 1.2535 1.2220 1.2415 1.2271 1.2041 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493	-0,0088 -0.0358 0.0354 0.0578 0.0160 0.0080 0.0081 0.0085 0.0851 0.3668 0.9729 1.7971 • -5.1867 • -0.1574 -0.0697
TEM (K 600 800 1000 1200 1400 1600 2000 2400 2400 2600 3000 3000 3500 3600	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.994 14.994 14.994 14.918 14.931 14.918 14.717 14.437 13.900 13.097 12.326 11.486	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2,1976 3,1624 0,9138 0,6812 0,6702 0,6878 0,7308 0,8251 1,0148 1,3648 1,9739 3,0071 4,7813 3,7632 4,5899 4,9592	AL/(MQL)(BAHN 0.7843 2-1843 2-1843 3-1795 0-9202 0-8819 0-6705 0-6881 0.7310 0-9212 1-5146 2-2376 4-0922 2-9765 3-7191 4-3685 4-7873	0,3051 0.6052 -0.5407 -0.7004 -0.1028 -0.0448 -0.0274 -0.0848 -0.0274 -0.0848 -0.0799 -3.6635 -36.0846 -37.7471 -6.1592 -6.1592 -3.46636	90RDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2537 1.2916 1.2716 1.2716 1.1449 1.1408 1.0087 1.1485 1.1485 1.1485	BAHN 1.1388 1.1191 1.1293 1.2220 1.2535 1.2502 1.2415 1.2271 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493	-0.0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0083 0.0851 0.2668 0.9729 1.7971 -0.1574 -0.0697 -0.0173
TEM (K 600 800 1200 1200 1400 1600 2200 2400 2400 2800 3000 3400 3600 3600 3600	P 29.004 23.904 16.994 15.166 14.992 14.963 14.954 14.963 14.913 14.913 14.913 14.201 14.461 14.008 13.281 12.329 11.434 10.572 9.813	MOL N7 BAHN 29.012 23.935 17.029 15.172 14.993 14.953 14.953 14.918 14.954 14.717 14.437 13.900 13.087 12.326 9.910 9.263	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0, 0, 0, 0, 0, 0, 1,660 0,7710 1,4607 0,0243 -0,435 -0,935	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.67308 0.8251 1.0148 1.3448 1.9739 3.0071 4.7613 3.9632 4.5599 4.9592 5.0774	AL/(MQL)(BAHN 0.7842 2.1843 3.1795 0.9202 0.6819 0.6705 0.6881 0.7310 0.0258 1.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103	0,3051 0,6052 -0,9407 -0,7004 -0,1028 -0,0486 -0,0486 -0,0274 -0,0888 -0,685 -3,685 -3,3598 -3,685 -3,7471 -6,1592 -4,8236 -3,4663 1,3215 -2,0262	G/RDON 1.1887 1.1187 1.1297 1.2227 1.2553 1.2416 1.2271 1.2042 1.7464 1.1016 1.0874 1.1434 1.1455 1.1591 1.1591	BAHN 1.1388 1.1191 1.1293 1.2220 1.2535 1.2502 1.241 1.1736 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493 1.1544 1.1586 1.1614	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0081 0.0081 0.0081 0.0083 0.0851 0.3668 0.9729 1.7971 -5.1867 -0.067 -0.0173 0.0481
TEN (K 600 800 1000 1200 1400 1400 2000 2200 2400 2200 3000 3400 3500 3500 4000 4200 4200	P GORDON 29,004 23,904 16,994 11,954 14,963 14,964 14,963 14,461 14,461 14,008 13,281 11,434 10,572 9,813 9,178 8,650	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.964 14.954 14.954 14.856 14.737 14.437 13.900 13.087 12.326 11.486 0.0558 9.910 9.203 8.716	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0.272 0.660 0.7710 1.6607 0.0243 -0.4548 -0.9135 -0.9261 -0.6583	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.8251 1.0148 1.3648 1.9739 3.0071 4.7813 3.9632 4.5899 4.9592 5.0774 5.0538 4.6357	AL/(MQL)/ BAHN 0.7843 3.1795 0.2026 0.6819 0.6881 0.7310 0.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103 5.1562	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0448 -0,0485 -0,0485 -0,0274 -0,0848 -0,04799 -3,6635 -13,353 e -3,6435 -13,353 e -3,6435 -13,255 e -4,7273 e	QGRDON 1.1387 1.1187 1.1297 1.2227 1.2503 1.2416 1.271 1.024 1.1449 1.1018 1.0874 1.1485 1.1859 1.1591 1.1687	BAHN 1.1388 1.1191 1.1293 1.2220 1.2535 1.2502 1.2415 1.2041 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1458 1.1586 1.1614 1.16063	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0085 0.0851 0.3668 0.9729 1.7971 -5.1867 -0.0697 -0.01574 -0.0697 0.0431 0.1376 0.2054
TEM (K 600 800 1000 1200 1400 1600 2000 2200 2400 2400 3000 3400 3400 3400 4400 4400 4400	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.994 14.994 14.993 14.918 14.931 14.918 14.856 14.737 13.900 13.007 12.326 11.486 9.910 9.263 8.716 8.286 7.993	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.8251 1.0148 1.93648 1.9739 3.0071 4.7813 3.9632 4.5899 4.9592 5.0774 4.7538 4.6357 4.1706 3.1039	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.6851 0.7310 0.6258 1.0217 1.4148 2.2376 4.0922 2.3765 3.7191 4.3865 4.7873 5.0103 5.0643 4.3734 3.2126	0,3051 0.6052 -0.5407 -0.7004 -0.1028 -0.0448 -0.0274 -0.0848 -0.0274 -0.0848 -0.4879 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.7471 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.6635 -3.66	QORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2537 1.2537 1.2746 1.1249 1.1204 1.1204 1.1409 1.1204 1.1408 1.0574 1.14591 1.1657 1.1657 1.1657 1.2083	BAHN 1.1388 1.1191 1.1293 1.2220 1.2535 1.2502 1.2415 1.2271 1.1736 1.1407 1.1095 1.1438 1.1452 1.1493 1.1584 1.1586 1.1614 1.1603 1.7899 1.2053	-0.0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0083 0.0851 0.2668 0.9729 1.7971 -0.1574 -0.0697 -0.0173 0.0431 0.1376 0.2569 0.2269
TEN (K 600 800 1000 1200 1400 1400 1400 2000 2400 24	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.994 14.994 14.993 14.918 14.931 14.918 14.856 14.737 13.900 13.007 12.326 11.486 9.910 9.263 8.716 8.286 7.993	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0. 0. 0. 0. 0. 0. 1660 0,7710 1.4607 0.0243 -0.6135 -0.6583 -0.9261 -0.6583	CP C. GORDON 0.7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.8251 1.0148 1.3448 1.9739 3.0071 4.7813 3.9632 4.5899 4.9592 4.9592 4.6357 4.1206	AL/(MQL)(ASAM) BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.7310 0.6258 1.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103 5.1562 5.0643 4.3734	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0274 -0,0848 -0,0274 -0,0848 -0,0479 -3,6635 -13,3593 -3,6464 -37,7471 -6,1524 -4,8236 -3,4663 -3,4663 -3,235 -3,235 -4,8236 -3,235 -2,0262 -4,7273 -4,8266	G/RDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2503 1.2416 1.271 1.2042 1.1746 1.1049 1.1204 1.1048 1.1449 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1549 1.1687	BAHN 1.1388 1.1191 1.1293 1.2220 1.2535 1.2502 1.2415 1.2041 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493 1.1544 1.1586 1.1614 1.1003	-0,0088 -0.0358 0.0354 0.0973 0.0160 0.0080 0.0081 0.00851 0.3668 0.9729 1.7971 -5.1867 -0.0574 -0.0575 0.0431 0.1376 0.23669
TEM (K 600 800 1000 1200 1400 1600 2000 2200 2400 2500 3500 3400 3600 4000 4400 4600 5000 5200	P GORDON 29,004 23,904 16,994 114,963 14,963 14,964 14,963 14,461 14,461 14,008 13,281 11,434 10,572 9,813 9,178 8,257 7,980 7,722 7,814	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.994 14.943 14.954 14.954 14.954 14.956 14.737 14.437 12.326 11.486 10.658 9.910 9.263 8.716 8.286 7.993 7.821 7.726	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.8251 1.0148 1.9739 3.0071 4.7813 3.9632 4.5899 4.9592 5.0774 5.1538 4.6357 4.1206 3.1039 2.1341 1.5519 1.3022	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.6819 0.6819 0.6881 0.7310 0.0258 1.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103 5.1562 5.1662 2.1872 1.3226	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0448 -0,0274 -0,0848 -0,0274 -0,0848 -0,0479 -3,6635 -13,3538 -3,6635 -13,3538 -13,215 -2,0262 -4,7273 -4,7273 -4,7273 -4,7273 -4,7273 -4,7273 -4,7273 -4,7273 -1,718 -1,5718	QGRDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2533 1.2416 1.2271 1.2046 1.1449 1.1018 1.0874 1.1434 1.1451 1.1657 1.1657 1.1657 1.1657 1.1657 1.1657 1.2633 1.2520 1.3529 1.3529	BAHN 1,1388 1,1191 1,1293 1,2290 1,2535 1,2502 1,2415 1,2271 1,2041 1,1736 1,1407 1,1095 1,0820 1,1438 1,1452 1,1493 1,1544 1,1586 1,1614 1,1603 1,1789 1,2053 1,2484 1,2986 1,3309	-0.0088 -0.0358 0.0358 0.0354 0.0973 0.0160 0.0080 0.0081 0.0085 0.0851 0.3668 0.9729 1.7971 -5.1867 -0.0697 -0.0173 0.0431 0.1376 0.2054 0.2369 0.2875 0.3300 0.3146
TEM (K 600 800 1000 1200 1400 1600 2000 2400 2400 3000 3400 3600 3600 4400 4400 4600 46	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.963 14.954 14.954 14.954 14.954 14.955 14.737 14.487 13.990 13.087 12.326 11.486 0.910 9.263 8.716 6.286 7.993 7.821 7.726	-0,0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 0.8251 1.0148 1.9739 3.0071 4.7813 3.9632 4.5899 4.9992 5.0774 4.1206 3.1039 2.1341 1.5519 1.5022 1.2923	AL/(MQL)/ BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.68819 0.7050 0.6851 0.7310 0.0258 1.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.3686 4.3734 3.2126 2.1872 1.5825	0,3051 0.6052 -0.9407 -0.7004 -0.1028 -0.0448 -0.0486 -0.0274 -0.0848 -0.0799 -3.6655 -13.3593 -36.0846 37.7471 -6.1592 4.8236 -3.4663 1.3215 -2.0262 -4.7273 -4.7273 -4.8282 -1.9718	90RDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2537 1.2537 1.2042 1.1746 1.449 1.1016 1.0874 1.1485 1.1591 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.2083 1.2520 1.5083	BAHN 1.1388 1.1191 1.1293 1.2220 1.24502 1.2535 1.2502 1.241 1.1736 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493 1.1544 1.1603 1.1736 1.1738 1.1614 1.1603 1.1739 1.2053 1.2484 1.2986	-0,0088 -0.0358 0.0354 0.0573 0.0160 0.0080 0.0081 0.0081 0.0851 0.3668 0.9729 1.7971 -0.1574 -0.0697 -0.0173 0.0431 0.1376 0.2054 0.2369 0.2875 0.3850
TEM (K 600 800 1000 1200 1400 1400 2000 2200 2200 2600 3800 3400 3600 4400 4600 4600 5000 5200	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.963 14.954 14.856 14.856 14.737 13.087 12.326 11.486 9.910 9.263 8.716 8.286 7.993 7.821 7.726	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0, 0, 0, 0, 0, 0, 0, 0, 0, 1,4607 0,0272 0,1660 0,7710 1,4607 0,0243 -0,4548 -0,6135 -0,9261 -0,03512 -0,1629 -0,03696 -0,0518 -0,0518 -0,0518 -0,0518	CP C. GORDON 0,7867 2,1976 3,1624 0,9138 0,6812 0,6702 0,6878 0,7308 0,9251 1,0148 1,3648 1,9739 3,0071 4,7813 3,9632 4,5899 4,9592 5,0774 5,0538 4,8357 4,1206 3,1039 2,1341 1,5519 1,3022 1,2923	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.67310 0.6257 1.5146 2.2376 4.7972 4.3685 4.7873 5.1162 2.1872 4.3734 3.2126 2.1872 1.3202	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0448 -0,0488 -0,0488 -0,0489 -3,6635 -13,3593 -3,6635 -13,3593 -3,7471 -4,8236 -3,7471 -2,0262 -4,7273 -4,8236 -3,7471 -2,0262 -1,718 -1,9718 -1,9718 -1,9718 -1,1298	QGRDON 1.187 1.1187 1.227 1.2503 1.2503 1.2416 1.2271 1.2042 1.1746 1.1449 1.1018 1.0874 1.1485 1.1857 1.1542 1.1591 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687	BAHN 1,1388 1,1191 1,1293 1,2220 1,2415 1,2271 1,2041 1,1736 1,1407 1,10820 1,1438 1,1452 1,1454 1,1546 1,1614 1,1586 1,1614 1,1693 1,2986 1,2986 1,2986 1,33309 1,3232	-0.0088 -0.0358 0.0354 0.0973 0.0160 0.0080 0.0081 0.0085 0.0851 0.3668 0.9729 1.7971 -0.1574 -0.0697 -0.01574 -0.0431 0.1376 0.2369 0.2269 0.2488
TEM (K 600 800 1000 1200 1400 1600 2000 2400 2400 3000 3400 3600 3600 4000 4400 4600 5000 5000 5000	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.993 14.994 14.943 14.918 14.856 14.737 13.990 13.087 12.326 11.486 10.658 9.910 9.263 8.716 8.286 7.993 7.821 7.726 7.633	-0.0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2,1976 3,1624 0,9138 0,6812 0,6702 0,6878 0,7308 0,8251 1,0148 1,3648 1,9739 3,0071 4,7813 3,9632 4,5899 4,992 5,0774 5,1538 4,6357 4,1206 3,1039 2,1341 1,5519 1,3022 1,2923	AL/(MQL)(BAHN 0.7843 3.1795 0.9819 0.6891 0.7310 0.6881 0.7310 0.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.11562 5.1662 1.3262 1.3262 1.3262 1.3262 1.3262	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0448 -0,0274 -0,0848 -0,0274 -0,0848 -0,0479 -3,6635 -13,3533 -13,6353 -13,6353 -13,6463 37,7471 4,8236 -3,7471 -4,7273 -4,7273 -4,7273 -4,7273 -4,7273 -1,718 -1,9718 -1,9718 -1,1298 -1,1298	QGRDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2503 1.2416 1.2271 1.008 1.1449 1.1204 1.1443 1.1485 1.1587 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687	BAHN 1,1388 1.1191 1,1293 1.2290 1.2535 1.2502 1.2415 1.2271 1.2041 1.1736 1.1407 1.1095 1.0820 1.1438 1.1452 1.1493 1.1544 1.1586 1.1614 1.1603 1.1789 1.2053 1.2484 1.2053 1.2484 1.2986 1.3309 1.3232	-0.0088 -0.0358 0.0358 0.0354 0.0973 0.0160 0.0080 0.0081 0.0085 0.0085 0.9729 1.7971 -0.1574 -0.0697 -0.0173 0.0431 0.1376 0.2259 0.22483 0.2875 0.3300 0.3146 0.2488
TEM (K 600 800 1000 1200 1400 1600 2800 2800 3800 3800 3400 3600 3600 3600 5000 6000 5000	P GORDON 29,004 23,904 16,994 15,166 14,962 14,963 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,954 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,964 14,9	MOL N7 BAHN 29.012 23.935 17.029 15.172 14.993 14.963 14.954 14.954 14.954 14.856 14.717 14.487 13.007 12.326 11.486 10.658 0.910 9.263 8.716 8.726 7.993 7.821 7.726 7.671 7.633	\$ -0,0276 -0,1297 -0,2060 -0,0264 -0,0067 -0, -0, -0, -0, -0, -1,660 -7,710 1,4607 -0,0272 -0,1660 -0,7710 1,4607 -0,0243 -0,0135 -0,0135 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0136 -0,0	CP C. 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TEM (K 600 800 1000 1200 1400 1400 1600 2000 2200 2600 3800 3400 3600 4400 4600 5000 5200 5600 1000 1200	P	HOL NT BAHN 29.012 23.935 17.029 15.172 14.993 14.993 14.994 14.983 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 14.954 15.357	-0,0276 -0,1297 -0,2060 -0,0264 -0,0067 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0, 0,	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6512 0.6702 0.6878 0.7308 0.8251 1.0148 1.9739 3.0071 4.7613 3.9632 4.5699 4.9592 5.0774 5.0538 4.6357 4.1206 3.1039 2.1341 1.5519 1.3022 1.2923	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.9202 0.8819 0.7310 0.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103 4.3734 3.2126 2.1872 1.3825 1.3222 1.33069	(K) \$\frac{1}{8}\$ \[\text{0.8051} \\ 0.6052 \\ -0.9407 \\ -0.7004 \\ -0.1028 \\ -0.0448 \\ -0.0274 \\ -0.0648 \\ -0.0274 \\ -0.0648 \\ -0.06799 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -13.3593 \\ -3.6635 \\ -1.7471 \\ -4.8236 \\ -3.5020 \\ -3.5020 \\ -1.9718 \\ -1.9718 \\ -1.1298 \\ \end{tabular} \]	QORDON 1.1387 1.1187 1.1297 1.2227 1.2553 1.2416 1.2271 1.2042 1.1746 1.1449 1.1018 1.0874 1.1445 1.1485 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857 1.1857	BAHN 1,1388 1,1191 1,1293 1,2220 1,2415 1,271 1,2041 1,1736 1,1407 1,10820 1,1438 1,1452 1,1493 1,1544 1,1586 1,1614 1,1693 1,2986 1,33309 1,3232	-0,0088 -0.0358 0.0358 0.0354 0.0973 0.0160 0.0080 0.0081 0.0085 0.0851 0.3668 0.9729 1.7971 -0.1574 -0.0697 -0.01574 0.2054 0.2368 0.2054 0.2488 -0.0266 -0.0179 0.0504
TEM (K 600 800 1000 1200 1400 1400 1600 2000 2400 2400 3000 3400 3600 3400 3600 4000 4500 5000 5000 5400 5100 5100 600 1000 1200	P	HOL NT BAHN 29,012 23,935 17,029 15,172 14,993 14,963 14,964 14,964 14,964 14,965 14,717 14,487 13,900 13,087 12,326 11,486 10,658 9,910 9,203 8,716 8,286 7,993 7,821 7,726 7,671 7,726 7,673 7,821 7,726 7,671 7,727 15,083	-0.0276 -0.1297 -0.2060 -0.0264 -0.0067 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C. GORDON 0,7867 2.1976 3.1624 0.9138 0.6812 0.6702 0.6878 0.7308 1.0148 1.9739 3.0071 4.7813 3.9632 4.5899 4.9592 5.0774 4.7206 3.1039 2.1341 1.5519 1.3022 1.2923 10.9811 1.1615 2.6934 2.1674 0.9550	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.9202 0.6819 0.6705 0.6851 0.7310 0.0258 1.0217 1.4148 2.2376 4.0922 2.9765 3.7191 4.3685 4.7873 5.0103 5.1562 5.0643 4.7873 3.2126 2.1872 1.3222 1.3069	0,3051 0.6052 -0.9407 -0.7004 -0.1028 -0.0448 -0.0274 -0.0848 -0.0274 -0.0848 -0.0799 -3.6635 -36.0846 -37.7471 -6.1592 -4.8236 -3.4663 1.3215 -2.0202 -4.7273 -4.826 -3.5020 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.9718 -1.97	GORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2537 1.2537 1.2546 1.2746 1.1446 1.1467 1.1018 1.0874 1.1485 1.1591 1.1687 1.1591 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.1687 1.2683 1.2520 1.3551 1.3265	BAHN 1,1388 1,1191 1,1293 1,2220 1,2451 1,2535 1,2571 1,2041 1,1736 1,1497 1,1492 1,1493 1,1594 1,1604 1,1603 1,1789 1,2053 1,2484 1,2986 1,3309 1,3232 1,1504 1,1792 1,1272 1,1592 1,1592 1,1592 1,1592 1,1592 1,1592 1,1592	-0,0088 -0.0358 0.0358 0.0358 0.0358 0.02578 0.0160 0.0080 0.0081 0.0081 0.0081 0.3668 0.9729 1.7971 -0.1574 -0.0647 -0.0173 0.0431 0.2369 0.2483 0.2875 0.2875 0.3346 0.2488
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GORDON 0,7867 2,1976 3,1624 0,9138 0,6812 0,678 0,7308 0,8251 1,0148 1,3648 1,9739 3,0071 4,7813 3,9632 4,5899 4,9992 5,0774 5,0538 4,6357 4,1706 3,1039 2,1341 1,5519 1,5022 1,2923 10,05811 1,1615 2,6936 2,1674 0,9550 0,7347 0,7029 0,7172 0,7650 0,7347 0,7029 0,7172 0,7650 0,7860 1,7463 2,4397 2,4397 2,4397 2,6789 3,5088 4,9258 4,9558 4,9558 4,9558 4,9558 4,9558 4,9558 4,9558 4,9558	AL/(MQL)(BAHN 0.7843 2.1843 3.1795 0.6819 0.68819 0.6881 0.7310 0.6258 1.0217 1.4148 2.2376 4.0922 2.9765 4.7873 5.0103 5.1562 4.7873 5.0103 5.1562 2.1872 1.3069 0.5803 1.1552 2.6754 0.7361 0.7361 0.7035 0.7175 0.6830 1.1752 0.9604 0.7361 0.7035 0.7175 0.7637 1.3986 2.1201 3.7123 1.9147 2.2935 2.7121 3.1369	0,3051 0,6052 -0,5407 -0,7004 -0,1028 -0,0448 -0,0274 -0,0848 -0,0274 -0,0848 -0,0274 -0,0848 -0,0274 -0,0848 -0,0274 -13,3593 -3,6635 -3,6635 -3,6635 -3,6635 -3,215 -3,6636 -3,7471 -4,7236 -4,7273 -4,8626 -1,7273 -4,8626 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9718 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,9738 -1,97	QORDON 1.1387 1.1187 1.1297 1.2227 1.2537 1.2537 1.2537 1.2537 1.2537 1.2537 1.2537 1.204 1.1018 1.0018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.2018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.1018 1.	BAHN 1,1388 1,1191 1,1293 1,2220 1,2413 1,2271 1,2041 1,1736 1,1407 1,10820 1,1438 1,1493 1,1504 1,1566 1,1614 1,1603 1,2986 1,3309 1,3232 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1504 1,1616 1,1616 1,1616 1,1616 1,1616 1,1616 1,1720 1,1758	-0.0088 -0.0358 -0.0358 -0.0358 -0.0358 -0.0358 -0.02573 -0.0160 -0.0080 -0.0081 -0.0081 -0.0081 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0177 -0.0173 -0.0431 -0.0431 -0.2569 -0.2483 -0.2875 -0.33146 -0.2488 -0.0179 -0.0179 -0.0179 -0.0081 -0.0179 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081 -0.0081

JP-4/LOX	0/	F= 0.6	ATM=			THAN ONE PERCIN			
TEMP (K)	GORGON	HOL WT		CP C GORPON	AL/(MOL): NHAR	(K) *	G GORDON	(S) AMMA	*
800.	29.806 29.060	29.807	-0.0275	0.5139 0.7438	0.5137 0.7408	n,n389 n,4083	1.1564	1.1543	0.0086 -0.0176
1000	24.507	26.535	-0.1056	1.3709	1.3611	D.7149	1.1204	1.1206	-9.0179
1209. 1490.	21.700 17.682	21.753 17.712	-0.2304 -0.1697	2.3211	2.3137	0.3188 -n.5805	1.1284	1.1292	0.0177 0.0600
1600.	16.048	16.067	-n.0748	1.1482	1.1544	-n.5400	1.2094	1.2048	0.0496
1800.	15.462	15.468 15.229	-0.03A5 -0.0263	0.7838	0.8697	-0.3230 -0.1914	1.2274	1.2268	0.0489 0.0570
2200.	15.114	15.117	-0.0198	9.7814	0.7825	-0.1408	1.2157	1.2148	n.0740
2490. 2600.	15.052 15.007	15.056 15.013	-0.0266 -0.0400	0.8318 0.9369	0.8335 0.9435	-n.2044 -n.8013	1.1962	1.1947	0.1254 0.2476
2800.	14.962	14.968	-0.0401	1.1032	1.1382	-3.1726 ·	1.1450	1.1399	n.5328
3000.	14,899	14,899 14.770	U.5556	1.5438	_ 1.4821_ 2.1325	-10.2917 • -27.7329 •	1.121 <u>8</u> 1.1037	1.1107	1.0341 + . 1.6852 +
3400.	14.649	14.521	0.8738	2.0996	1.2041	42.6510 •	1.0911	1.1826	-8.3869 *
3690. 3800.	14.471	14.307	0.7905 0.7627	1.3553	1.339a 1.4996	1.2027 * 3.1704 *	1.1754	1.1791	-0.3148 -0.3581
4000.	13.842	13.753	0.6430	1.7612	1.6841	4.3777 +	1.1723	1.1762	-0.8327
4200.	13.469	13.407_ 13.018	0.4603 0.2376	1.9873 2.2224	1.8894	4.9263 • 5.0036 •	1.1733	1.1767	-0.2898 -n.2297
4600.	12.593	12.593	0.	2.4621	2.3441	4.7927 •	1.1786	1.1808	-n.1867
4800. 5000.	12.111 11.617	12.139 11.668	-0.2312 -0.4390	2.7015 2.9338	2.5823 2.8203	4.4124 * 3.8687 *	1.1822 1.1862	1.1838	-0.1353 -0.0843
5200.	11.122	11.190	-0.6114	3.1491	3.0517	3.0929	1.1905	1.1910	÷n.0420
5400 5600.	<u>10.637</u> 10.173	10.715	-0.7333 -0.7864	3.3330	3,2668	1.9862 •	1.2009	1.1950 . 1.1997 .	0.0251
5000.					0,4407	11,5100	1.2004	1.1777	11.0949
690.	0/I 28.603	F= 0.4 28.612	ATM≖ -0.0315	1. 0.8526	0.8481	0.5278	1.1339	1.1342	-0.0265
800.	23.102	23.139	-0.1602	2.3167	2.3056	0.4791	1.119R	1.1200	-0.0179
1000.	15.027	16.639 15.031	-0.1686 -n.0266	2.8398	0.9502	-0.5810 -0.5077	1.1340	1.1336	
1409.	14.857	14.858	-0.0267	0.7486	0.7492	-0.9801	1.2281	1.2100	0.0081
1600.	14.826	14.826	n.	0.7406	0.7409	-0.0405	1.2239	1.2238	0.0082
1800. 2000	14.816 14.805	14.816 14.805	0. n.	0.7607 0.8n82	0.7610	-0.0394 -0.0247	1.2160	1.2159	0.0082 0.0083
5500	14.778	14,778		0.9116	0.9123	-n.0768	1,1839	1.1838	0.0084
2400. 2600.	14.712 14.570	14,712 14,566	0. 0.0275	1.1197	1.1266	-0.6612 -3.5954 *	1.1586 1.1330	1.1577	0.0777 0.3266
2800.	14.296	14.270	0.1819	2.1683	2.4537	-13.1624 .	1.1116	1.1020	ก.8636
3200.	13.817_ 13.051	13.704 12.679	0.8178 2.8504 •	3.3011 5.2514	4.4827 9.1249	-35.7941 * -73.7613 *	1.0952	1.0772	1.6485 *
3400.	11.909	11.865	0.3695	8.8983	4.1663	53.1787 .	1.0721	1.1402	-6.3520 -
3600.	10.898	10.992	-0.8625	5.3225	4.9460	7.0737 •	1.1436	1.1445	-0.0767
3800. 4000.	9.183	10.128 9.338	-1.4220 + -1.6879 +	5.8230 6.1039	5.5316 5.9806	5.0043 • 2.0200 •	1.1491	1.1492 1.1525	-0.0087 0.0607
4200	8.504	8,638	-1.5757 •	6.2913	6.4424	-2.4017 •	1.1557	1-1540	0.1471
4400.	7.936 7.477	8.027 7.525	-1.1467 • -0.6420	6.3230 5.8129	6.7039 6.1852	-6.0240 * -6.4047 *	1.1598	1.1569	0.2070
4800.	7.143	7.164	-0.2940	4.5800	4.7934	-4.6594 *	1.1881	1.1653	0.2357
5000. 5200.	6.93 <u>1</u> 6.811	6.942 6.817	-0.1587 -0.0881	3.1684 2.1657	3.2706 2.2228	-3.2256 • -2.6366 •	1.2733	1.2200	0.2698
5400	6.744	6.74B	-D.0593	1,6306	_1.6671_	-2.2384 •	1.3247	1.3192	0 • 4152
5600.	6.704	6.706	-0.0298	1.4164	1.4415	-1.7721 -	1.3522	1.3469	0.3920
JP-4/LOX -	0/8	= 0.4	ATM=			HAN ONE PERCINT			
TEMP		HOL WT		CP C	ALZ(HOL)(K)	GA	MMA (S)	*
TEMP (K)	GORDON	TW JON PHAR	•	CP C/ GORDON	ALZ(HOL)(RAHN	K) K	GORDON PORROD	RAHN	*
TEMP (K) 690.	GORDON 29.289	MOL WT RAHM 29,292	% -0.0102	CP C/ GORDON 0.6175	4L/(HOL)(RAHN 0.6152	K) K 0.3725	GA GORDO4 1.1443	RAHN _1.1447	-0.0350
TEMP (K) 690. 890. 1030.	GORDON 29.289 26.948 21.336	29.292 26.970 21.380	-0.0102 -0.0816 -0.2062	CP C/ GORDON 0.6175 1.2382 2.6260	0.6152 1.2323 2.6126	K) K	GORDON PORROD	RAHN	
TEMP (K) 690. 890. 1030.	GORDON 29.289 26.948 21.336 16.544	NOL WT FIAHN 29.292 26.970 21.380 16.567	% -0.0102 -0.0816 -0.2062 -0.1390	CP C/ GORDON 0.6175 1.2382 2.6260 2.0595	0.6152 1.2323 2.6126 2.0745	K) K 0.3725 0.4765 0.5103 -0.7283	GORDON 1.1443 1.1237 1.1203 1.1593	7,1447 1,1238 1,1274 1,1588	-0.0350 -0.0089 -0.0089 0.0431
TEMP (K) 690. 810. 1070. 1270. 1470.	29.289 26.948 21.336 16.544 15.247 14.961	NOL WT RAHN 29.292 26.970 21.380 16.567 15.253 14.963	-0.0102 -0.0816 -0.2062	CP C/ GORDON 0.6175 1.2382 2.6260	0.6152 1.2323 2.6126	K) K 0.3725 0.4765 0.5103	GORDON 1.1443 1.1237 1.1203 1.1593 1.2074	RAHN 1,1447 1,1238 1,1234 1,1588 1,2071	-0.0350 -0.0089 -0.0089 0.0431 0.0248
TEMP (K) 600. 800. 1000. 1200. 1400. 1600. 1820.	GORDON 29.289 26.948 21.336 16.544 15.247 14.877	NOL WT RAHN 29.292 26.970 21.380 16.567 15.253 14.963 14.878	-0.0102 -0.0816 -0.2062 -0.1390 -0.0394 -0.0434 -0.067	CP C/ GORDON 0.6175 1.2382 2.6260 2.0595 1.0156 G.8091 0.7779	0.6152 1.2323 2.6126 2.0745 1.0202 0.8105 0.7785	K) 0.3725 0.4765 0.5103 -0.7283 -0.4529 -0.1730 -0.0771	GORDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2191 1.2159	8AHN 1.1447 1.1238 1.1274 1.1588 1.2071 1.2190 1.2158	-0.0350 -0.0089 -0.0089 0.0431 0.0248 0.0082
TEMP (K) 690. 810. 1070. 1270. 1470.	29.289 26.948 21.336 16.544 15.247 14.961	NOL WT RAHN 29.292 26.970 21.380 16.567 15.253 14.963	-n.0102 -n.0816 -0.2062 -n.190 -n.0394 -n.034	CP C/ GORDON 0.6175 1.2382 2.6260 2.0595 1.0156 0.8091	0.6152 1.2323 2.6126 2.0745 1.0202 0.8105	K) 0.3725 0.4765 0.5103 -0.7283 -0.4529 -0.1730	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2191	8AHN 1.1447 1.1238 1.1204 1.1588 1.2071 1.2190 1.2158 1.2071	-0.0350 -0.0089 -0.0089 0.0431 0.0082 0.0092 0.0083
TEMP (K) 690. 890. 1000. 1200. 1400. 1670. 1690. 2090. 2410.	GORDON 29.289 26.948 21.336 16.544 15.247 14.861 14.877 14.843 14.821	PANN WT FIAMN 29.292 26.970 21.380 16.567 15.253 14.963 14.848 14.843 14.842 14.794	-0.0102 -0.0816 -0.0816 -0.0762 -0.1790 -0.0394 -0.067 0.	CP C/ GORDON 0.6175 1.2382 2.6260 2.0595 1.0156 6.8091 0.7779 0.7943 0.8475 0.9540	9.6152 1.2323 2.6126 2.0745 1.0202 0.8105 0.7785 0.7946 0.8478 0.9563	K) R 0.3725 0.4765 0.5103 -0.7263 -0.4529 -0.1730 -0.0771 -0.0354 -0.0354	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2191 1.2159 1.2077 1.1928 1.1723	RAHN 1.1447 1.1238 1.1274 1.1588 1.2071 1.2190 1.2158 1.2071 1.1927 1.1719	-0.0350 -0.0089 -0.0089 -0.0431 0.0248 0.0082 -0.0092 -0.0084 0.0084
TEMP (K) 690. 870. 1970. 1470. 1670. 1820. 2096.	GORDON 29.289 26.948 21.336 16.544 15.247 14.961 14.877 14.843 14.821	MOL WT FIAHN 29.292 26.970 21.380 16.567 15.253 14.963 14.878 14.843 14.822 14.794	-0.0102 -0.0816 -0.2062 -0.1390 -0.0394 -0.0134 -0.0067 0.0067	CP C/ GORDON 0.6175 1.2382 2.6260 2.0595 1.0156 G.8091 0.7779 0.7943 0.8475 0.9540 1.1421	0.6152 1.2323 2.6126 2.0745 1.0202 0.8105 0.7785 0.7945 0.6478 0.6478 1.1598	K) R 0.8725 0.4765 0.5103 -0.7263 -0.4529 -0.1730 -0.0771 -0.0378 -0.0354 -0.0411 -1.5498	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2191 1.2159 1.2077 1.1928 1.1723 1.148)	RAHN 1.1447 1.1238 1.1204 1.1588 1.2071 1.2190 1.2158 1.2071 1.1927 1.1719 1.1460	-0.0350 -0.0089 -0.0089 -0.4031 0.0248 0.0082 0.0092 0.0083 0.0084 0.0341 0.1829
TEMP (K) 690. 890. 1000. 1200. 1400. 1600. 1400. 2000. 2410. 2600. 2800. 3000.	GORDON 29.289 26.948 21.336 16.544 15.247 14.961 14.877 14.843 14.821 14.794 14.745 14.652 14.652	MOL WT FIAHN 29.292 26.970 16.567 15.263 14.878 14.843 14.843 14.842 14.744 14.744 14.644 14.447	-0.0102 -0.0816 -0.2062 -0.1990 -0.0394 -0.034 -0.067 -0.0367 0.0368 0.0366 0.2761	CP C/ GORROW 0.6175 1.2382 2.6260 2.5595 1.0156 G.8091 0.7779 0.743 0.8475 1.9540 1.421 1.427 1.4311	0.6152 1.2323 2.6126 2.0745 1.0205 0.7785 0.7785 0.7946 0.8478 0.9563 1.1598 1.3358	K) 1.3725 1.4765 1.5103 -0.4529 -0.1730 -0.4771 -0.0378 -0.0354 -0.2411 -1.5498 -6.6428 -20.9570	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2191 1.2159 1.2072 1.1928 1.1723 1.1481 1.1744 1.1044	RAHN 1.1447 1.1238 1.1274 1.1588 1.2071 1.2190 1.2158 1.7071 1.1927 1.1719 1.1460 1.1182 1.7915	-0.0350 -0.0089 -0.0089 -0.0083 0.0082 0.0092 0.0083 0.0084 0.1829 0.5514 1.1681
TEMP (K) 690. 800. 1000. 1200. 1400. 1600. 2006. 2200. 2400. 2600. 2800. 3000.	GORDON 29.289 26.948 21.336 16.544 15.247 14.961 14.873 14.821 14.794 14.745 14.652 14.487	MOL WT FIAHN 29.292 26.970 21.380 16.567 15.253 14.878 14.878 14.843 14.822 14.794 14.644 14.644 14.644	-0.0102 -0.0816 -0.2062 -0.1390 -0.0394 -0.0394 -0.067 0.0967 0.0968 0.0546 0.2761	CP C/ GORROW 0.6175 1.2382 2.0595 1.0156 0.8091 0.7779 0.7043 0.8475 0.9547 1.4497 1.4497 1.9311 2.6726	9.6152 1.2323 2.6126 2.0745 1.0202 0.8105 0.7785 0.7446 0.8478 0.9563 1.1598 1.5460 4.0736	K) R 0.3725 0.4765 0.5103 -0.7283 -0.4529 -0.1730 -0.0771 -0.0378 -0.0354 -0.0411 -1.5498 -6.6428 -0.9570 -52.4209	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2190 1.2072 1.1928 1.1723 1.1481 1.1044 1.1044 1.1044	RAHN 1.1447 1.1238 1.1238 1.1238 1.1238 1.2071 1.2190 1.2158 1.2071 1.1927 1.1719 1.1460 1.1182 1.7915 1.0694	-0.0350 -0.0089 -0.0089 -0.0083 0.0431 0.0082 0.0092 0.0092 0.0083 0.0084 0.0341 0.1829 0.5514 1.1681
TEMP (K) 690. 890. 1900. 1200. 1400. 1600. 2006. 2200. 2410. 2600. 3800. 3400. 3600.	GORDON 29.289 26.948 21.336 16.544 15.247 14.961 14.877 14.821 14.794 14.745 14.652 14.487 14.205 13.747	NOL WT RAHN 29.292 26.970 21.380 16.567 15.253 14.878 14.878 14.872 14.794 14.744 14.644 14.644 14.644 13.408 12.920	-0.0102 -0.0816 -0.2062 -0.1390 -0.0394 -0.0384 -0.0367 -0.0367 0.0546 0.2761 1.0630 • 2.4660 •	CP C/ GORROW 0.6175 1.2382 2.0260 2.0595 1.0156 G.8091 0.7779 0.7943 0.8475 0.9749 1.1421 1.4497 1.4497 1.4311 2.6726 3.8288 2.8763	ALZ(MOL): RAMN 0.61523 2.6126 2.0745 2.0745 0.8105 0.77846 0.8478 1.1598 1.54608 4.07360 2.1527	K) (1.3725 (1.4765 (1.5103 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1.9728 (1	GARDON 1.1443 1.1237 1.1203 1.1593 1.2074 1.2190 1.2072 1.1928 1.1723 1.1481 1.1044 1.1044 1.1044	RAHN 1.1447 1.1238 1.1274 1.1588 1.2071 1.2190 1.2158 1.7071 1.1927 1.1719 1.1460 1.1182 1.7915	-0.0350 -0.0089 -0.0089 -0.0083 0.0082 0.0092 0.0083 0.0084 0.1829 0.5514 1.1681
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付録 - C -

G. S. Bahn, S. Gordon の熱力学データを使用した場合の, JP-4/AIR燃焼生成物の定温・定圧下における平均分子量, 比熱, 比熱比の比較

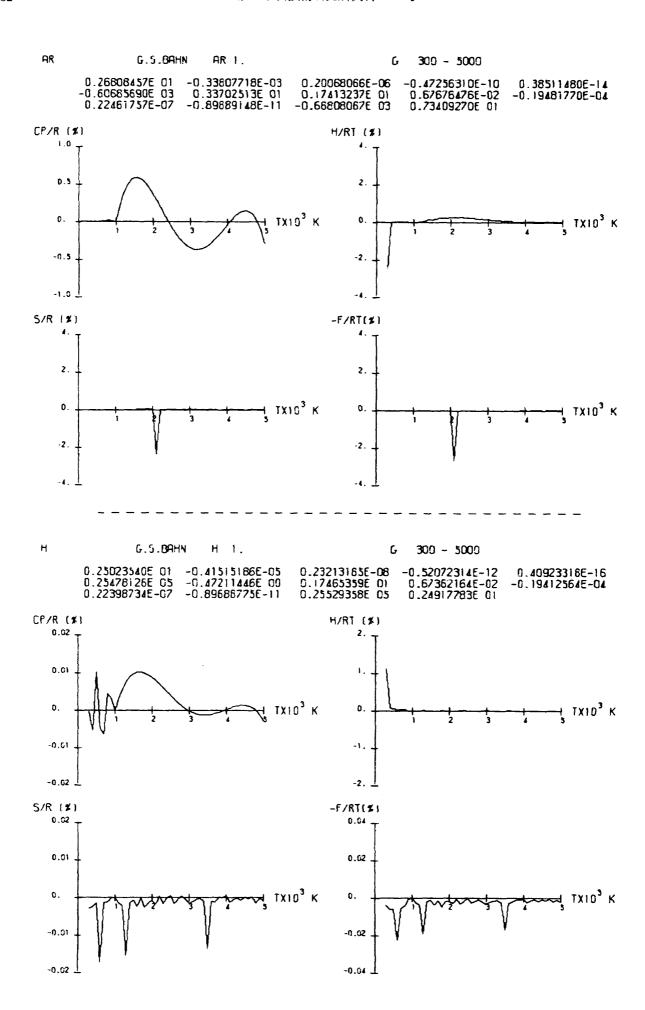
	50.7		. 7.		16 AUER 7	MAN AND BEG	CTHT		
JP-4/AIR TEMP		10= 0.5 HOL NT		CP CAL	L/(MOL)(K	HAN ONE_PER	GAM	MA (S)	*
(K)	GORDON	BAHN	*	GORDON	BAHN		GORDON	BAHN	
<u>500.</u> 600.	28.958	28.958	<u>-:</u>	0.2564	0.2578	-0.5460 0.5714		1.3628	0.1977
700.	28.958	28.958	0.	0.2691	0.2667	0.8919	1.8422	1.3464	-0.3129 -0.1502
800. 990.	28.958 28.958	28.958 28.958	n. n.	0.2758 0.2821	0.2746	0.4351 -0.1418		1.3382	0.0454
1000.	28.958	28.958	0.	0.2879	0.2869	0.3473		1.3143	-0.0990
1250. 1500.	28.958	28.958	<u> </u>	0.3115	0.3112	0.0963	1.2827	1.2831	-0.0312
1750. 2000.	28.954 28.940	28.954 28.940	0. 0.	0.3252 0.3495	0.3252 0.3497	0. -0.0572	1.2684	1.2684	0.0160
2250.	28.879	28.880	-0.0035	0.4071	0.4071	0.	1.2184	1.2183	0.0062
2500. 2750.	28.689	28.690	-0.0035 -0.0106	0.5357 0.7439	0.5354	0.0560	1.1815	1.1815	0-
3000.	27.453	27,457	-0.0146	0.9796	0.9803	-0.0715	1.1467	1.1466	0.0087
3250. 3500.	26.368 25.155	26.370 25.156	-0.0076 -0.0040	1.1776 1.2310	1.179û 1.2323	-0.1189 -0.1056	1.1591	1.1590	0.0066
3750. 4000.	24.087 23.335	24.087	0. 0.0043	1.0814 0.8450	1.0819	-n.0462 n.0355	1.1783 1.2052	1.1783	-0.0088
4250.	22,873	23.334	0.00-3	0.6672	0.6667	0.0749	1.2315	1.2317	-0.0162
4500. 4750.	22.588 22.377	22.588 22.377	n.	0.5932	0.5928 0.6092	0.0674	1.2421	1.2423	-0.0161
5n^n.	22.170	22.170	0.	0.7010	0.7015	-0.0713	1.2086	1.2064	0.0165
5250. 5500.	21,917 21,577	21.917 21.577	n. n.	9.8671 1.1155	0.8683	-0.1384 -0.1793	1.1655	1.1651	0.0343
5750.	21,115 20,503	21.115	n.	1.4589	1.4612	-0.1577 -0.0838	1.1517	1.1518	0.0263
6030.	211, 300	20.300			11.770				
500.	28.958	28.958	ρ. . η	4= 10. C.2564	0.2578	-0.5469	1.3655	1.3628	0-1977
600.	26,958	28.958	ŋ.	0.2625	0.2610	0.5714	1.3539	1.3568	-0.2142 -0.3129
700. 800.	28,958 28,958	28.958, 28.958	0 · .	0.2691 0.2759	0.2667	n.8919 n.4351	1.3312	1.3332	-0.1502
9 00.	28.958	28.958	ŋ.	0.2821	0.2825	-0.1418 0.3473	1.3214 — 1.313n	1.3208	-0.0990
1000. 1250.	28,958 28,958	28.958 28.958	n.	0.2444	0.2869 0.2993	0.2001	1.2967	1.2975	-0.0617
1500.	28,958 28,956	28.958 28.956	0. 0.	0.3111	0.3108 0.3231	n.0964 0.	1.283n 1.2702	1.2034	-0.0312 D.0079
1750. 2008.	28,950	28.950	0.	0.3387	0.3389	-0.0590	1.2561	1.2559	0.0159
2250. 2500.	28,926 28,855	28.926 28.856	0. -0.0035	0.7655 0.4180	0.3658	-0.0821 -0.0239	1.238r 1.2140	1.2377	0.0242
2750.	28,580	28,682	-0.0070	0.5112	0.5110	0.0391	1.1887	1.1886	n.0084
3000. 3250.	28,338 27,799	28.340 27.802	-0.0071 -0.0108	0.6387 0.7704	მ. 63 95 მ .77 07	n.n313 -n.n389	1.1708 1.1685	1.1634	0. 0.0086
3500.	27.084	27.087 26.247	-0.0111 -0.0038	0.8846 0.9647	0.8853	-0.0791 -0.0829	1.1640	1.1659	0.00%6 0.0085
3750. 4000.	26,246 25,367	25.368	-0.0039	0.9829	0.9834	-0.0509	1-1801	1.1601	0.
4250. 4500.	24,555 23,886	24.555 23.886	n. G.	0.9275 0.8261	0.9276 0.8259	-0.0108 0.0242	1-1944 1-2111	1.1945	-0.8084 -0.8083
4750.	23,379	23.379	0 -	c.725*	0.7257	n.0138	1.2265	1.2266	-0.0082 0.0162
50:0. 525e.	23,005 22,715	23.005 22.715	6 •	6.661A 0.6463	0.6619	-0.0453 -0.1702	1.2353	1.2351	0.486
5510.	22,463	22.463 22.209	n. n.	0.6801 0.7610	0.6823 0.7645	-0.3235 -0.4599	1.2229	1.2219	0.0818 0.1076
5750. 6090.	21.925	21.923	e.	6.8891	0.8939	-0.5399	1.1923	1.1908	0.1258
01,	210,50	21.770		0.0047	0.0707	-174 30 77	1.1.50		
JP-4/AIR - TEMP	ERA	TIO= 0.5	AT	H= 20. ◆ CP CA	IS OVER	THAN ONE PE	PCINT GA	NHA (S)	,
JP-4/AIR - TEMP (K)	ERA GORDON	TIO= 0.5 MOL WT RAHN		H= 20. • CP CA GORDOF	IS OVER NL/(MOL)(RAHN	THAN ONE PE K)	RCINT GA GORĐON	NHA (S) Bahn	y
JP-4/4IR - TEMP (K) 500.	ERA GORTON 28,958	TIO= 0.5 MOL WT RAHN 28.958	AT %	M= 20. • CP CA GORDON 0.2564	IS OVER AL/(MOL)(RAHN 0.2578	THAN ONE PE K) % -0.5460	RCINT GA GORĐON 1-3655	NHA (S)	0.1977
JP-4/AIR - TEMP (K) 500. Ach. 706.	ERA GORDON 28,958 25,958 25,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958	AT % n. n. e.	M= 20. • CP CA GORDON 0.2564 0.2625 0.2691	1S OVER AL/(MOL)(BAHN 0.2578 0.2610 0.2667	THAN ONE PE K) % -0.5460 0.5714 0.8919	GA GORDON GA GORDON 1.3655 1.3539 1.3422	1.3628 1.3568 1.35464	0.1977 -0.2142 -0.3129
JP-4/AIR - TEMP (K) 500. 600.	ERA GORDON 28,958 26,958	TIO= 0.5 MOL WT RAHN 28.958 28.958	AT S O.	H= 20.	IS OVER NL/(MOL)(RAHN 0.2578 0.2610	THAN ONE PE K) % -0.5460 0.5714	RCINT GORDON 1.3655 1.3539	1.3628 1.3568 1.3568 1.3332 1.3208	0.1977 -0.2142 -0.3129 -0.1502 0.0454
JP-4/AIR - TEMP (K) 500. 600. 706. 800. 900.	GORDON 28,958 26,958 26,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958	AT 6. 6. 6. 6. 7.	M= 20.	1S OVER L/(HOL)(I RAHN 0.2578 0.2610 0.2667 0.2746 0.2825 0.2869	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473	GORDON 1.8655 1.8539 1.8422 1.8812 1.8714 1.8136	NHA (S) BAHN 1.3628 1.3568 1.3464 1.3332 1.3208 1.3143	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990
JP-4/AIR - TEMP (K) 500, 600, 700, 800, 0.0, 10-0, 1250,	ERA GORPON 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958	AT 8 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2625 0.2691 0.2754 0.2879 0.2099 0.3111	15 OVER RAHN 0.2578 0.2610 0.2667 0.2746 0.2825 0.2869 0.2993 0.3108	THAN ONE PE K) % -0.5714 0.6919 0.4351 -0.1418 0.3473 0.2001 0.0964	GORDON 1.3655 1.3539 1.3422 1.3312 1.3724 1.3136 1.2967	NMA (S) BAHN 1.3628 1.3568 1.3464 1.3332 1.3208 1.3143 1.2975	0.1977 -0.2142 -0.3129 -0.1502 0.0454 -0.0990 -0.0617
JP-4/AIR - TEMP (K) 500. 600. 706. 800. 900. 1006. 1250. 1510. 1750.	ERA GORPON 28,958 26,958 26,958 26,958 26,958 26,958 27,958 28,958 28,958 28,958 28,958	TIO= 0.5 NOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958	AT 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2625 0.2691 0.2754 0.2819 0.2819 0.2819 0.2999 0.3111 0.3227	15 OVER L/(HOL)(I BAHN 0.2578 0.2610 0.2667 0.2746 0.2869 0.2869 0.2993	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001	GORPON 1.8655 1.3539 1.8422 1.8312 1.8714 1.8136	NHA (S) BAHN 1.3628 1.3568 1.3464 1.3332 1.3208 1.3143 1.2975 1.2834 1.2704	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617
JP-4/AIR - TEMP (K) 500, 600, 706, 800, 90, 1006, 1250, 1756, 2000, 2250,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957	8 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2691 0.2691 0.2758 0.2819 0.2879 0.3911 0.327 6.3370 0.3593	1S OVER LL/(HOL)(I RAHN 0.2578 0.2610 0.2646 0.2825 0.2869 0.2869 0.3108 0.3227 0.3372 0.3372	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 6.0964 0.373 0.0593	GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3136 1.2967 1.2973 1.2705	NHA (S) BAHN 1.3628 1.3568 1.3464 1.3332 1.32975 1.2834 1.2704 1.2571 1.2411	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0734 -0.0979 -0.0159 -0.0242
JP-4/AIR - TEMP (K) 50n, 64n, 700, 80n, 0 10-6, 125n, 1510, 1750, 2001	GORDON 28,954 26,958 26,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.959 28.957 28.957	AT 6. 6. 6. 7. 7. 7. 7. 7. 7.	M= 20. CP CA GORDON 0.2564 0.2691 6.2758 0.2879 0.2879 0.3111 6.3227 6.3370 0.4718	1S OVER (1 (MOL) (1 (MAHN) 10 (2578 0.2667 0.2746 0.2825 0.2869 3 0.3108 0.3227 0.3596 0.4003 0.4718	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 6.0964 0. -0.0593 -0.0835	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3136 1.2967 1.2705 1.2757 1.2757 1.2414 1.2209 1.1986	MHA (S) BAHN 1.3628 1.3568 1.3564 1.3232 1.3236 1.3143 1.2834 1.2704 1.2571 1.2411 1.2217	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0164 -0.0167
JP-4/AIR - TEMP (K) 500. 600. 700. 800. 900. 100. 1500. 1500. 2750. 2000. 2250. 3000.	GORDON 28,958 26,958 26,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957	8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2691 6.2758 0.2879 0.2879 0.3877 6.327 6.3370 0.3593 0.4718 0.5748	1S OVER (1/40L) (1/64N) (1/40L) (1/64N) (1/40L) (1/40N) (1/40N	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 6.0964 0.593 -0.0593 -0.0593	GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3136 1.2967 1.2705 1.2705 1.2573 1.2414 1.2209 1.1986	NMA (S) BAHN 1.3628 1.3568 1.3568 1.3528 1.3295 1.2834 1.2704 1.2704 1.271 1.2411 1.2207 1.1978	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 0.0159 0.0159 0.0164
JP-4/AIR - TEMP (K) 500, 600, 706, 800, 1006, 1250, 1756, 2000, 2750, 2750, 3756, 3756, 3756, 3756, 3756, 3756, 3756, 3756, 3756,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,457 28,756 28,763 28,763 28,763 28,763	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.958	8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2691 0.2691 0.2758 0.2879 0.2879 0.3911 0.3227 0.3370 0.4593 0.401 0.4718 0.5748 0.5748	1S OVER (1 (HOL) (1 (THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 0.9964 0.0593 -0.0593 -0.0500 0.0522 0.0555	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2831 1.2705 1.2753 1.2414 1.2209 1.1980 1.1794 1.1598	MMA (S) BAHN 1.3628 1.3568 1.3568 1.3568 1.3143 1.2934 1.2704 1.2704 1.2704 1.2207 1.2411 1.2207 1.1794 1.1698 1.1698	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0242 -0.0164 -0.0167 -0.0266
JP-4/AIR - TEMP (K) 500. 600. 700. 800. 1000. 1250. 1500. 1750. 2000. 2250. 2510. 3060. 3060. 3750.	GORPON 28,954 26,958 26,958 26,958 26,958 26,958 26,958 27,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,758	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.952 28.957 28.957 28.957 28.957	8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20. CP CA GORDON 0.2564 0.2691 0.2621 0.2819 0.2999 C.3111 G.3227 G.3370 0.3593 C.4001 0.4718 6.6873 0.3873 0.8675	1S OVER 1L/ (HOL) (I RAHN 0.2578 0.2610 0.2746 0.2825 0.2869 0.3337 0.3327 0.3596 0.4018 0.5745 0.6873	THAN ONE PE K) % -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 6.0964 00.0593 -0.0835 -0.0502 0.	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2705 1.2773 1.2414 1.2209 1.1986 1.1794 1.1692 1.1718	1.3628 1.3568 1.3568 1.3564 1.3362 1.3208 1.3143 1.2975 1.2834 1.2704 1.2571 1.2207 1.1978 1.1978	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0259 -0.0164 -0.0167 -0.0266 -0.0086
JP-4/AIR - TEMP (K) 500, 600, 706, 800, 1250, 1500, 1756, 2000, 2750, 2750, 3750, 3750, 4000, 4250,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,957 28,957 28,952 28,958 28,750 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957	8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER (1) (HOL) (I) RAHN (0.2578 (0.2610 (0.2746 (0.2825 (0.3108 (0.3372 (0.33796 (0.4018 (0.5745 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0.6873 (0	THAN ONE PE K) -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 0.0964 0.0593 -0.0835 -0.0502 0.0522 0.0692 -0.0692 -0.0692	RCINT GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2963 1.2705 1.2573 1.2414 1.2209 1.1986 1.1794 1.1692 1.1682 1.1718 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194 1.17194	1.3628 1.3568 1.3568 1.3568 1.3568 1.3143 1.2975 1.2704 1.2571 1.2411 1.2207 1.1794 1.1698 1.1794 1.1716 1.1716	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0164 -0.0167 -0.0084
JP-4/AIR - TEMP (K) 500, ACO, ACO, ACO, ACO, ACO, ACO, ACO, ACO	GORDON 28,954 26,958 26,958 26,958 26,958 26,958 27,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,756 28,488 28,766 27,481 28,765 27,481	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957	8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER (1) (HOL) (I) RAHN (1, 2578 (1, 2612 (1, 2746 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1, 2825 (1,	THAN ONE PE K) -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 0.9964 00.0593 -0.0835 -0.0500 00.0522 0.0692 -0.0692 -0.0692 -0.0692 -0.0692 -0.0696	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2831 1.2705 1.2753 1.2414 1.2209 1.1986 1.1794 1.1692 1.1718 1.1794 1.1692 1.1719 1.1794 1.1794 1.1903 1.1203	MMA (S) BAHN 1.3628 1.3568 1.3568 1.3568 1.3143 1.2975 1.2207 1.2411 1.2207 1.2411 1.2207 1.1698 1.1794 1.1698 1.1718 1.1718 1.1718 1.1718 1.1904 1.2039	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0164 -0.0167 -0.0086 -0.0083 -0.0083
JP-4/AIR - TEMP (K) 500, 670, 706, 830, 970, 1076, 1250, 1756, 2000, 2750, 3750, 3750, 3750, 4000, 4750, 4750, 5000,	GORPOW 28,954 26,958 26,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,952 28,463 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,750 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28,486 28	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.957 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.958 28.958 28.957 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958	8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	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JP-4/AIR - TEMP (K) 500, 600, 706, 800, 1250, 1500, 1756, 2004, 2250, 2516, 2750, 3750, 3750, 4000, 4750, 4750, 5000, 5000, 5000, 5000, 5000, 5000,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,952 28,958 28,750 28,750 28,760 25,973 27,481 26,770 25,973 27,481 24,470 25,973 27,481 23,079	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.958 28.957 28.954 26.8451 28.491 28.066 27.484 26.773 25.928 23.492 23.442 23.079	8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER (L/(HOL)(I) RAHN 0.2578 0.2610 0.2746 0.2869 0.2993 0.3108 0.3227 0.3596 0.4718 0.5745 0.6873 0.9119 0.8602 0.9149 0.8602 0.7109 0.6650 0.6650	THAN ONE PE K) -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 0.0964 00.0593 -0.0835 -0.0500 00.0522 00.0502 -0.0692 -0.0656 -0.0329 -0.0116 -0.1650 -0.1329	RCINT GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2831 1.2705 1.2573 1.2414 1.2209 1.1960 1.1794 1.1692 1.1718 1.17194 1.1903 1.2038 1.2180 1.2299 1.2353	1.3628 1.3568 1.3568 1.3568 1.3568 1.3143 1.2975 1.2704 1.2571 1.2411 1.2411 1.2411 1.1794 1.1698 1.1794 1.1794 1.1939 1.2347 1.2347 1.2347	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0164 -0.0167 -0.0088 -0.0088 -0.0088 -0.0088
JP-4/AIR - TEMP (K) 50n. 60n. 700. 80n. 100. 125n. 151n. 1750. 225n. 251. 3250. 3750. 3750. 4750. 4750. 500. 500. 500. 500.	GORDON 28,954 28,958 28,958 28,958 28,958 28,958 28,958 28,952 28,952 28,952 28,863 27,481 28,750 24,484 28,763 27,481 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753 24,753	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.957 28.957 28.958 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959 28.959	AT 8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER 1 (HOL) (I RAHN 0.2578 0.2610 0.2667 0.2849 0.3108 0.3227 0.3596 0.4018 0.5745 0.6873 0.7882 0.8681 0.6677 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607 0.7607	THAN ONE PE K) % -n.5460 n.5714 n.8919 n.4351 -n.1418 n.3473 n.2001 -n.0593 -n.0835 -n.0835 -n.0500 n. n.0522 nn.0656 -n.0329 -n.0116 n.0116	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2705 1.2773 1.2414 1.2209 1.1980 1.1794 1.1698 1.1698 1.1794 1.1698 1.1794 1.1903 1.2038 1.2189 1.2239	MMA (S) BANN 1.3628 1.3564 1.3566 1.3143 1.2975 1.2975 1.2971 1.2411 1.2277 1.1794 1.1794 1.1794 1.1794 1.1796 1.1794 1.1796 1.1798 1.1798 1.1798 1.1798 1.1798 1.1798 1.1798 1.1798 1.1798 1.1904 1.2039 1.2181 1.2296	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0164 -0.0167 -0.0088 -0.0088 -0.0088 -0.0088
JP-4/AIR - TEMP (K) 500, 600, 706, 800, 1250, 1500, 1756, 2004, 2250, 2516, 2750, 3750, 3750, 4000, 4750, 4750, 5000, 5000, 5000, 5000, 5000, 5000,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,952 28,958 28,750 28,750 28,760 25,973 27,481 26,770 25,973 27,481 24,470 25,973 27,481 23,079	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.958 28.957 28.954 26.8451 28.491 28.066 27.484 26.773 25.928 23.492 23.442 23.079	AT 8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	M= 20.	1S OVER LZ (HOL) (I RAHN 0.2578 0.2610 0.2746 0.2825 0.2869 0.33272 0.3596 0.4718 0.5745 0.6873 0.7882 0.8681 0.8681 0.7602 0.7602 0.6630 0.6630 0.6988	THAN ONE PE K) % -0.5460 0.5714 0.4919 0.4351 -0.1418 0.3473 0.2001 0.0954 0.0593 -0.0835 -0.0502 0.0092 -0.0656 -0.0892 -0.0856 -0.0892 -0.0116 0.0329 -0.0329 -0.3329	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3134 1.2967 1.2837 1.2775 1.2573 1.2414 1.2209 1.1980 1.1794 1.1698 1.1794 1.1698 1.1794 1.1698 1.1794 1.1093 1.2180 1.2180 1.2283 1.2283 1.2283	MMA (S) BANN 1.3628 1.3568 1.3568 1.3568 1.3143 1.2704 1.2571 1.2411 1.207 1.1978 1.1698 1.1681 1.1716 1.1794 1.1794 1.1794 1.1794 1.1794 1.1904 1.2039 1.2181 1.2039 1.2181 1.2214 1.2347 1.2347 1.2344	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0167 -0.0242 -0.0167 -0.0083 -0.0082 -0.0083 -0.0082 -0.0083 -0.0082 -0.0083 -0.0082 -0.0084 -0.0083 -0.0084 -0.0084 -0.0085 -0.00874 -0.0084
JP-4/AIR - TEMP (K) 50n. 60n. 700. 80n. 100. 125n. 151n. 1750. 225n. 251. 3250. 3750. 3750. 4750. 4750. 500. 500. 500. 500.	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,750 28,750 28,760 25,215 24,503 23,443 23,079 25,215 24,503 23,443 23,079 27,783 27,518 22,552	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.953 28.957 28.957 28.2515 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.491 28.2515 24.503 25.215 24.503	AT 8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	M= 20.	1S OVER (L/ (HOL) (I) RAHN 0.2578 0.2610 0.2746 0.2829 0.2910 0.35227 0.3596 0.4010 0.5745 0.6873 0.2740 0.8601 0.9119 0.8600 0.7743 0.2578	THAN ONE PE K) -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 -0.0835 -0.0835 -0.0835 -0.0502 0.0522 0.0522 0.0522 0.0522 0.0533 -0.1650 -0.1650 -0.1650 -0.1650 -0.3229 -0.5460	RCINT GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3136 1.2967 1.2831 1.2705 1.2573 1.2414 1.2209 1.1980 1.1794 1.1692 1.1718 1.1794 1.1692 1.1718 1.1794 1.2038 1.2180 1.2253 1.2253 1.2299 1.2353 1.2099	MMA (S) 8AHM 1.3628 1.3568 1.3568 1.3568 1.3143 1.2934 1.2704 1.2704 1.2704 1.2704 1.1794 1.1794 1.1796 1.1796 1.1796 1.1796 1.1796 1.1796 1.1796 1.1796 1.1796 1.1797 1.2314 1.2037 1.2314 1.2212 1.2077	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0164 -0.0167 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0163 -0.0163 -0.0163 -0.0163 -0.0163 -0.0163 -0.0163 -0.0163 -0.0163
JP-4/AIR - TEMP (K) 50n, Afn, 700, Ron, 10-0, 125n, 151n, 1750, 205n, 255n, 375n, 386n, 375n, 386n, 375n, 475n, 500, 475n, 500, 575n, 600,	GORDON 28,954 28,954 28,958 28,958 28,958 28,958 28,958 28,952 28,958 28,750 28,4864 28,763 27,481 28,770 25,215 24,513 23,910 23,079 27,783 27,783 27,783 27,783 28,952 28,958 28,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.951 28.491 28.491 28.751 28.491 28.751 28.491 28.751 28.491 28.751 28.491 28.751 28.491 28.751 28.934 25.215 24.503 23.999 23.472 23.679 22.783 22.253	AT 8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER 1L/ (HOL) (I RAHN 0.2578 0.2610 0.2746 0.2825 0.2869 0.3108 0.3237 0.3596 0.4018 0.5745 0.6873 0.7882 0.8681 0.7743 0.6630 0.7743	THAN ONE PE K) % -n.5460 n.5714 n.8919 n.4351 -n.1418 n.3473 n.2001 n.0964 nn.0593 -n.0835 -n.0502 nn.0522 nn.0522 nn.0656 -n.0529 -n.0116 nn.0563 -n.0509 -n.0116 -n.0593 -n.0656 -n.0892 -0.5460 -0.5514	RCINT GARDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3134 1.2967 1.2705 1.2775 1.2414 1.2209 1.1980 1.1794 1.1698 1.1794 1.1698 1.1794 1.1907 1.2180 1.2289 1.2353 1.2280 1.2799	MMA (S) BANN 1.3628 1.3568 1.3568 1.3568 1.3143 1.2704 1.2704 1.2704 1.2704 1.2704 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.2039 1.2181 1.2037	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0079 -0.0159 -0.0167 -0.0167 -0.0083 -0.0083 -0.0082 -0.1063 -0.0082 -0.1163 -0.0084 -0.0083 -0.1977 -0.1818
JP-4/AIR - TEMP (K) 50n. 60n. 700. 80n. 1000. 1250. 1500. 2250. 2350. 2350. 3750. 4750. 4750. 5250. 5500. 5500. 500. 600.	GORPOOM 28,954 26,958 26,958 26,958 28,958 28,958 28,958 28,958 28,750 28,750 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760 28,760	TIO= 0.5 MOL MTN 28.958 28.958 28.958 28.958 28.958 28.958 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.958 28.958 28.958 28.958	AT 8 0. 6. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	M= 20.	1S OVER 1L/(HOL)(I) RAHN 0.2578 C.2667 0.2746 0.2825 0.2869 0.3108 0.3272 0.3527 0.3527 0.3594 0.4718 0.5745 0.6673 0.7882 0.6677 0.6638 0.7743 0.2578 0.2578 0.2578	THAN ONE PE K) % -0.5460 0.5714 0.4919 0.4351 -0.1418 0.3473 0.2001 6.0944 0. 0.0593 -0.0835 -0.0502 00.0522 00.0656 -0.0329 -0.0116 00.3329 -0.4680 -0.3329 -0.5460 -0.5714 0.4351	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3134 1.2867 1.2831 1.2775 1.2775 1.2775 1.2141 1.2209 1.1980 1.1794 1.1692 1.1794 1.1692 1.1718 1.1794 1.203 1.2180 1.2738 1.2180 1.2738 1.2283 1.2283 1.2353 1.2353	MMA (S) BANN 1.3028 1.3508 1.3508 1.3508 1.3508 1.3145 1.2704 1.2571 1.2411 1.207 1.1794 1.1794 1.1794 1.1794 1.1794 1.2039 1.2181 1.2039 1.2181 1.2037 1.2314 1.2077	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0164 -0.0167 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.0163 0.0486 0.0974 -0.1472 -0.1618
JP-4/AIR - TEMP (K) 50n, Afn, 700, Rnn, 0 10, 10-0, 125n, 1750, 205n, 225n, 255n, 375n, 386n, 375n, 386n, 375n, 500, 475n, 500, 575n, 600, 570, 600, 600, 600, 600,	GORDON 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,750 28,486 28,763 27,481 26,779 25,215 24,503 23,979 27,283 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL MT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.934 29.841 28.751 28.491 28.761 28.491 28.773 28.491 28.773 22.783 22.513	AT 8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER 1L/ (HOL) (I RAHN 0.2578 0.2617 0.2746 0.2825 0.2869 0.2918 0.3327 0.3596 0.4018 0.5745 0.6873 0.9119 0.8607 0.9119 0.8607 0.6630 0.6988 0.7743	THAN ONE PE K) -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 -0.0835 -0.0835 -0.0502 0.0502 0.0692 -0.0692 -0.056892	RCINT GARDON 1.3655 1.3530 1.3422 1.3312 1.3714 1.3136 1.2967 1.2831 1.2705 1.2573 1.2414 1.2209 1.1980 1.1980 1.1794 1.1082 1.1718 1.1794 1.1082 1.1718 1.1794 1.203 1.218n 1.2299 1.2353 1.2726 1.2299 1.3655 1.3530 1.3099	MMA (S) 8AHM 1.3628 1.3568 1.3568 1.3568 1.3143 1.2934 1.2704 1.2934 1.2704 1.2207 1.1698 1.1718 1.1718 1.1718 1.1718 1.1718 1.1704 1.1904 1.2039 1.2314 1.2212 1.2077 1.3628 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528 1.3528	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0164 -0.0167 -0.0083 -0.0083 -0.0083 -0.0084 -0.0083 -0.0084 -0.0083 -0.0084 -0.0084 -0.0083 -0.0084 -0.0084 -0.0083 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0085 -0.0084 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085
JP-4/AIR - TEMP (K) 50n, Arn, 700, Ron, 10-0, 125n, 151n, 1750, 275n, Ron, 275n, Ron, Ron, Ron, Ron, Ron, Ron, Ron, Ro	GORPOOM 28,954 28,958 28,958 28,958 28,958 28,958 28,958 28,952 28,958 28,750 24,484 28,763 27,481 26,770 25,215 24,513 23,910 23,079 27,783 27,783 27,788 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= 0.5 MOL WT RAHN 28.958 28.958 28.958 28.958 28.958 28.958 28.957 28.958 28.957 28.751 28.491 28.751 28.491 28.751 28.491 28.751 28.491 28.751 28.253 23.979 23.479 22.753 23.979 22.753 23.979 23.479 22.753 28.958 28.958 28.958 28.958	AT 8 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	M= 20.	1S OVER LL/(HOL)(I RAHN 0.2578 0.2610 0.2746 0.2825 0.2869 0.33372 0.3596 0.4718 0.5745 0.7882 0.6630 0.4718 0.6630 0.7743 0.2578 0.2578 0.2578 0.2578 0.2578 0.2578 0.2578 0.2825 0.2825 0.2829 0.2829	THAN ONE PE K) 4 -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 -0.0529 -0.0529 -0.0552 0.0520 -0.0552 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522 -0.0656 -0.0522	RCINT GA GORDON 1.3655 1.3539 1.3422 1.3312 1.3714 1.3134 1.2967 1.2735 1.2741 1.2573 1.2414 1.2209 1.1980 1.1794 1.1082 1.1794 1.1082 1.1718 1.1794 1.1083 1.2736 1.2737 1.2414 1.3136 1.2799 1.3655 1.3539 1.3655 1.3539 1.3539 1.35312 1.3514 1.31367	MMA (S) BANN 1.3628 1.3568 1.3568 1.3568 1.3143 1.2704 1.2571 1.2411 1.2207 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.1794 1.2037 1.2317 1.2317 1.2077	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0159 -0.0159 -0.0167 -0.0083 -0.0083 -0.0083 -0.0083 -0.0083 -0.1083 -0.163 -0.163 -0.1472 -0.1818 -1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0907
JP-4/AIR - TEMP (K) 50n. Arn. 700. Ran. 9 10. 1250. 1510. 2250. 2350. 3750. 4750. 4750. 5250. 5500. 5750. 6000. 1250. 1250. 1250. 1250. 1250. 1250. 1250.	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JP-4/AIR - TEMP (K) 500, A700, A200, 1250, 1250, 1250, 2250, 2250, 2250, 3750, A000, A500, A5	ERA GORPON 28,954 24,954 24,958 24,958 24,958 24,958 24,957 24,957 24,750 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 24,760 26,956 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958 28,958	TIO= O.5 MOL WIT N 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.752 28.934 24.751 28.491 28.491 28.751 28.491 28.491 28.25.398 25.215 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958 28.958	AT 8 0. 6. 6. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7.	M= 20.	1S OVER LL/(HOL)(I) RAHN 0.2578 0.2610 0.2667 0.2825 0.2869 0.3327 0.3596 0.4018 0.5745 0.6873 0.7882 0.8691 0.6630 0.7743 0.2578 0.2510 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.2507 0.250	THAN ONE PE K) 4 -0.5460 0.5714 0.8919 0.4351 -0.1418 0.3473 0.2001 0.0522 0.0552 0.0552 0.0656 -0.0522 0.0656 -0.0522 0.0656 -0.0522 0.0656 -0.0522 0.0656 -0.0522 0.0552 0.0552 0.0656 -0.0522 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.0552 0.05552	GORDON 1.3655 1.3539 1.3422 1.3312 1.3214 1.3134 1.2967 1.2831 1.2773 1.2414 1.2009 1.1980 1.1794 1.1692 1.1798 1.1698 1.1794 1.1903 1.2038 1.2180 1.2799 1.3655 1.3530 1.2820 1.3530 1.2820 1.3530 1.2820 1.3530 1.2820 1.3530 1.2820 1.3530 1.2820 1.3530 1.2831 1.2831 1.2831 1.2831 1.2831	NMA (S) BANN 1.3028 1.3568 1.3568 1.3568 1.3508 1.3145 1.2704 1.2704 1.2704 1.2704 1.1798 1.1798 1.1681 1.1794 1.1794 1.1794 1.1794 1.2039 1.2181 1.2039 1.2347 1.2039 1.2347 1.2039 1.2347 1.2039 1.2347 1.2039 1.2347 1.2039 1.2347 1.2039 1.2347 1.2077	0.1977 -0.2142 -0.3129 -0.1502 -0.0454 -0.0990 -0.0617 -0.0234 -0.0169 -0.0169 -0.0169 -0.0083 -0.0084 -0.0083 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084 -0.0084
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JP-4/AIR - TEMP (K) 50n. Afn. 700. Ran. 10-0. 125n. 1510. 1750. 275n. Rapen. 3256. 85n6. 875n. 875n. 875n. 875n. 875n. 875n. 800. 575n. 800. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250. 1250.	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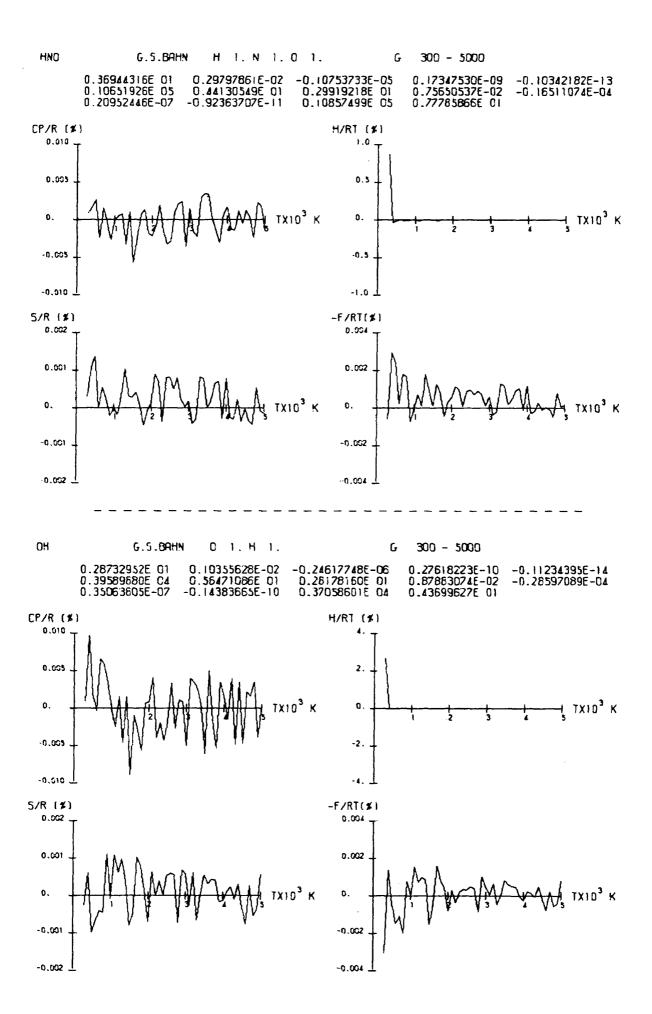
JP-4/AIR	- ERA	T10= 1.0	ATH	1: 1. •	IS OVER	THAN ONE PER	CINT	MMA (S)	
(K)	GORDON	BAHN		BORDON		<u> </u>	GORDON	BAHN	<u> </u>
500.	28,952	20.952	0.	0.2660	0.2684	-0.9023	1.3478	1.3435	0.3190
600. 700.	28.952 28,952	28.952 28.952_	0.	0.2782	0.2723	0.3294 0.9263	1.3355 1.3286	1.3370	-0.1123 -0.3098
800.	28.952	28.952	0.	0.2882	0.2858	0.8328 Q.4064	1.3126	1.3160	-0.2590 -0.1305
900.	28.952	28,952 28,952	0.	0.3017	0.3001	0.5303	1.2945	1.2965	-0.1545
1250. 1500.	28,951 28,950	28.951 28.950	0,	0.3148	0.3139	0.1220	1.2788	1,2799	-0.0860
_1750. 2000.	28,936	28.936 28.877	-0. -0.0035	0.3512	0.3511	0.0285	1,2469	1.2163	-0.0000
2250.	28.696	28,698_	-0.0070	0.5249	0.5244	0.0953	1.1802	1.1802	0
2500. 2750.	28.295 27.591	28.299 27,597	-0.0141 -0.0217	0.7121 0.9454	0.7115 0.9455	0.0843	1.1583	1.1532	0.0087 0.0088
3000. 3250.	26.563 25.252	26.569 25.256	-0.0226 -0.0158	1.1987	1.1999	-0.1001 -0.1332	1.1379	1.1378	0.0088
3500.	23.843	23.845	-0.0084	1.4767	1.4785	-0.1219	1.1546	1.1545 1.1758	0.0087
3750. 4000.	22,654	22.654	0	0.9383	1.2565 0.9382	0.0107	1.1754 1.2044	1.2044	0.
4250. 4500.	21.404	21.404	<u>0</u> _	0.7166	0.7162	0.0558	1,2380	1.2332	-0.0162 -0.0161
4750	20,944	_20.944	. 0.	0.6362	0.6361	0.0157	1.2354	1.2354	0.0082
5000 · .5250 ·	20.760 20.535	20.760 20.535	0.	0.7291	0.7293 0.9033	-n.0274 -n.0886	1.2122 1.1873	1.1871	0.0168
5500. 5750.	20.229 19.805	20.229 19.806	0. 0.0050	1.1693	1.1703	-0.0855 -0.0515	1,1666	1.1663	0.0257 0.0261
6020.	19.230	19.231	-0.0052	2,0766	2.0767	-0.0048	1.1410	1.1407	0.0263
_				= 10,					. 740-
500. 600.	28.952 28.952	28.952 28.952	0.	0.2660 0.2732	0.2684 0.2723	-0.9023 0.3294	1.3478 1.3355	1.3435 1.3370	0.3190 -0.1123
700.	28,952	28.952	0	C.2807	0.2781	0.9263	1,3736	1.3277	-0.2590
900∙	28.952	28.952	a.	0.2953	D. 2941	0.4064	1.3028	1.3045	-0.1305
1000. 1250.	28.952 28.952	28.952 28.951	0. 0.0035	0.3017 0.3147	0.3001 0.3138	0.5303 0.2860	1.2945 1.2789	1.2965 1.2800	-0.1545 -0.0860
1500. 1750.	28,951 28,944	28.951 28.944	0.	0.3263	0.3259	0.1226	1,2667 1,2534	1.2671	-0.0316 0.
2000.	28.916	28.916	0.	0.3721	0.3722	-0.0269	1.2336	1.2335	0.0081
2250 2500.	28.830 28.632	28.831 28.635	-0.0035 -0.0105	0.4322 0.5318	0.4321	0.0231 0.0565	1.2071	1.2069	0.0166
2750. 3000.	28.271 27.719	28.275 27.724	-0.0141 -0.0180	0.6618 0.8014	0.6609 0.8014	0.0605	1.1629 1.1543	1.1628 1.1541	0.0086 0.0173
3250.	26.986	26.991	0.0185	0.9356	0.9362	-0-0641	1.1529	1.1528	0.0087
3500 · 3750 · _	26.098 25.099	26,102 25,102	-0.0153 -0.0120	1.0596	1.0606	-0.0944 -0.0955	1.1563	1.1562	0.0086 0.0086
4000. 4250.	24.ŋ82 23.168	24.084	-0.0083 0.	1.1655	1.1665 1.8834	-n.n858 -n.n462	1.1751 1.1905	1.1751	n. n.
4500.	22.439	22,439	0.	0.9418	0.9419	-0.0106	1.2085	1.2085	0 •
4750. 5000.	21.530	21.907 21.530	0.	0.8060_ 0.7176	0.8059 0.7178	. 0.0124 -0.0279	1.2356	1.2356	n
5250. 5500.	21.250	21.250 21.015	n. a.	0.688A 0.7169	0.6896	-n.1452 -n.2650	1.2360 1.2257	1.2855	0.0405 0.0734
5750.	20.783	20.784	-0.0048	0.7992 0.9366	0.8022	-0.3754 -0.4164	1.2100	1.2088	0.0992
6000.	20.524	20.525	-0.8949						
					•				
JP-4/AIR TEMP		TIO: 1.0 HOL WT	АТА	20. • CP C/	IS OVER	THAN ONE PERI	CINT G4	MMA (S)	
	- ERA GORDON	TIO: 1.0	ATH %	= 20. •	IS OVER	THAN ONE PERI	CINT	HMA (S) Bahn	*
TEMP (K)	GORDON _28.952	TIO: 1.0 MOL WT RAHN	ATH * 0	20. CP C/ GORDON	IS OVER	THAN ONE PERI K)	GORDON GA	MMA (S) BAHN 1.3435	0.3190
TEHP (K) 590. 600. 700.	GDRDON _28.952 _28.952 _28.952	TIO: 1.0 MOL WT HAHN 26.952 28.952 28.952	# 0	20. CP C/ GORDON 0.2667 0.2732 0.2807	1S OVER AL/(MOL)(I BAHN -0.2684 0.2723 0.2781	THAN ONE PERIK) -0.9023 0.3294 0.9263	GORDON GORDON 1.3478 1.3355 1.3236	MMA (S) BAHN 1.3435 1.3370 1.3277	0.3190 -0.1123 -0.3098
TEMP (K) 600.	GORDON 28.952 28.952 28.952 28.952 28.952	TIO: 1.0 MOL WT RAHN 26.952 28.952 28.952 28.952 28.952	# 0	20. CP C/ GORDON 0.266/ 0.2732	IS OVER ALZ(MOL)(BAHN _0.2684_ 0.2723	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.9328 0.4064	GARDON 1.3478 1.3355 1.3236 1.3126 1.3028	MMA (S) BAHN 2.3435 1.3370 1.3277 1.3160 1.3045	0.3190 -0.1123 -0.3098 -0.2590 -0.1305
TEMP (K) 500. 700. 800. 900.	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.952	TIO: 1.0 MOL WT RAHN 26.952 28.952 28.952 28.952 28.952 28.952	0	20. CP C/ GORDON 0.2667 0.2732 0.2807 0.2882 0.2953 C.3017	IS OVER AL/(HOL)(BAHN -0.2684 -0.2723 0.2781 0.2858 0.2941 0.3001	THAN ONE PERI K) * -0.9023 0.3294 0.9263 0.4064 0.5303	GARDON 1.3478 1.3355 1.3236 1.3126 1.3028 1.2945	MMA (S) BAHN 1.3435 1.3370 1.3277 1.3160 1.3045 1.2965	0.3190 -0.1123 -0.3098 -0.2590 -0.1305 -0.1545
TEMP (K)	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.951	TIO: 1.0 HOL WT RAHN 26.952 28.952 28.952 28.952 28.952 28.951 28.951	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP C/ GORDON 0.2667 0.2732 0.2807 0.2867 0.2852 0.2953 C.3017 0.3147 0.3260	IS OVER BL/(MOL)(I RAHN -0.2684 0.2723 0.2781 0.2858 0.2941 0.3001 0.3138 0.3256	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227	GROON 1.3478 1.3355 1.3256 1.3126 1.3028 1.2945 1.2790 1.2670	MMA (S) BAHN 1.3435 1.3370 1.3277 1.3160 1.3045 1.2965 1.2800 1.2674	0.3190 -0.1123 -0.3098 -0.2590 -0.1305 -0.1545 -0.0782 -0.0316
TEMP (K)	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.952	TIO: 1.0 HOL WT RAHN 26.952 28.952 28.952 28.952 28.952 28.951 28.951 28.946 28.946 28.946	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP C/ GORDON	IS OVER BL/(MOL)(I BAHN -0.2684 -0.2723 D.2781 C.2858 0.2941 0.3001 0.3138 0.3256 0.3399 0.3657	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.83294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 00.0274	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2670 1.2546 1.25372	MMA (S) BAHN 1.3435 1.3370 1.3277 1.3160 1.3045 1.2965 1.2800 1.2674 1.2546 1.2546	0.3190 -0.1123 -0.3098 -0.2590 -0.1305 -0.1545 -0.0782 -0.4316 0.0081
TEMP (K)	28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.946 28.923 28.854	TIO: 1.0 HOL WT HAHN 26.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.953 28.855	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	P 20. CP C/ GORDON	IS OVER L/(MOL)(BAHN 0.26 <u>84</u> 0.2723 0.27858 0.2941 0.3001 0.3138 0.3256 0.3359 0.3657 0.4151	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 0.	GORDON 1.3478 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2676 1.2546 1.2346	MMA (S) BAHN 1,3435 1.3370 1.3277 1.3160 1.3045 1.2965 1.2800 1.2674	0.3190 -0.1123 -0.3098 -0.2590 -0.1305 -0.1545 -0.0782
TEMP (K)	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.953 28.854 28.854 28.400	TIO: 1.0 MOL WT RAHN 24.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.951 28.952 28.953 28.855 28.697 28.697	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP C/ GORDON	1S OVER 1L/(MOL)(I BAHN 0.2684 0.2723 0.2781 0.2858 0.2941 0.3101 0.3138 0.3256 0.3399 0.3657 0.4151 0.4964	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.1227 0. -0.0274 0. 0.0495	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2796 1.2546 1.25372 1.2136 1.1889 1.1702	HMA (S) BAHN 1.3435 1.3370 1.3277 1.3160 1.3045 1.2965 1.2674 1.2546 1.2546 1.2371 1.1888 1.1702	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.0782 -0.0081 0.0165 0.0084
TEMP (K) -5006007008009001000125015001750200022502250235032503250.	GDR DON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.952 28.952 28.952 28.952 28.952 28.953 28.854 28.854 28.953 28.854 28.953 28.854 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.353 28.35	TIO: 1.0 MOL WT RAHN 26.952 28.952 28.952 28.952 28.951 28.951 28.951 28.961 28.963 28.855 28.855 28.857 28.403 27.947 27.333	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP CJ GORDON 0.2660, 0.2732 0.2807 0.28807 0.2882 0.2953 0.3017 0.3147 0.3260 0.3399 0.3656 0.4151 0.4965 0.6060 0.7262 0.6401	1S OVER L/(HOL)(I) BAHN -0.2644 0.2723 0.2781 0.28941 0.3001 0.31256 0.33557 0.4964 0.6057 0.4964 0.6057	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 0. 0.0274 0. 0.0201 0.0495 0.01357	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2670 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601	BAHN 3.435 1.3370 1.3277 1.3160 1.3045 1.2965 1.2860 1.2674 1.2546 1.2546 1.1888 1.1702 1.1600 1.1571	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0782 -0.0316 0.0081 0.0084 0.0086
TEMP (K)	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.946 28.953 28.854 28.695 28.400 27.943	TIO: 1.0 NOL MT RAHN 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.964 28.855 28.697 28.403 27.947	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP C/ GORDON 0.2667 0.2732 0.2887 0.2882 0.2953 C.3017 0.3147 0.3260 0.3399 0.3656 0.4151 0.4965 0.6060 0.7262	1S OVER L/(MOL)(I RAHN 0.2684 0.2723 0.2781 0.2858 0.2941 0.3138 0.3256 0.3256 0.3359 0.3657 0.4151 0.4964 0.6057	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 00.0274 0. 0.0495 0.0138	GORDON 1.3478 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2676 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601	#MA (S) BAHN 1,3435 1.3370 1.3277 1.3160 1.3045 1.2800 1.2674 1.2546 1.2674 1.2134 1.1888 1.1702	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0782 -0.0081 0.0081 0.0084 0.0086 0.0086 0.0086
TEMP (K)	GOR DON 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.961 28.864 28.695 28.734 28.695 27.343 27.343 27.343 27.343	TIO: 1.0 MOL WT RAHN 24.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.961 28.963 28.855 28.697 28.855 28.697 27.947 27.343 26.583 25.725 24.886	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP C/ GORDON	1S OVER L/(HOL)(I) RAHN 0.2684 0.2723 0.2781 0.2884 0.3001 0.3138 0.3256 0.3359 0.3657 0.4151 0.4964 0.657 0.7261 0.8404 0.9443 1.0355	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.1227 0. -0.0274 0. 0.0201 0.0495 0.01357 -0.0357 -0.0742 -0.0830	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2796 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601 1.1572 1.1593 1.1648 1.1736	MMA (S) BAHN 1,3435 1,3370 1,3277 1,3160 1,3045 1,2965 1,28674 1,2546 1,2546 1,1888 1,1702 1,1600 1,1571 1,1592 1,1647 1,1735	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0081 -0.0081 -0.0084 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086
TEMP (K) -5006007008009001000125015001750250025502550350037504004500.	GORDON 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.952 28.951 28.855 28.855 28.657 27.943 27.328 26.579 24.804 23.905 23.108	TIO: 1.0 MOL WT RAHN 26.952 28.952 28.952 28.952 28.951 28.951 28.951 28.961 28.963 28.855 28.855 28.6583 27.933 26.583 25.725 24.806 23.906	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP CJ GORDON 0.2667, 0.2732 0.2807 0.2807 0.28267 0.3147 0.3147 0.3349 0.3369 0.3369 0.4151 0.4965 0.4165 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965 0.4965	1S OVER L/(HOL)(I) BAHN -0.2644 0.2723 0.2781 0.28941 0.3138 0.3138 0.3156 0.3357 0.4964 0.3657 0.4964 0.3657 0.4964 0.3657 0.4964 0.3657	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 0.0274 0.0201 0.0495 0.01357 -0.0742 -0.0357 -0.0742 -0.0830 -0.0852 -0.0652	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2670 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601 1.1572 1.1593 1.1648 1.1736 1.1855 1.2000	HMA (S) BAHN 3.3435 1.3377 1.3160 1.3045 1.2965 1.2800 1.2674 1.2546 1.2771 1.2134 1.1888 1.1702 1.1600 1.1571 1.1572 1.1647 1.1735 1.1855 1.28000	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0081 0.0081 0.0165 0.0084 0.0086 0.0086 0.0086 0.0086
TEMP (K) -500600700800900100012501500250025002500350035003500350045004500450050005000.	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 27.328 26.579 27.43 27.328 26.579 25.721 24.804 23.905 23.108 22.463	TIO: 1.0 MOL MT RAHN 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.951 28.961 28.855 28.697 28.403 27.947 27.333 26.583 25.725 24.806 23.108 22.462 21.971	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP CJ GORDON 0.2660, 2732 0.2782 0.2807 0.2882 0.2953 C.3017 0.3147 0.3147 0.3656 0.4151 0.4965 0.6060 0.7262 0.6401 0.9436 1.0324 1.0849 1.0739 0.9986 0.6902 0.7899	1S OVER L/(HOL)(I) BAHN -0.2644 0.2723 0.2781 0.28941 0.3011 0.3138 0.3256 0.3357 0.4954 0.5357 0.4954 0.6057 0.7461 0.9940 0.9940 0.9940 0.9940 0.9940 0.9940 0.9940 0.9940 0.9940 0.9940	THAN ONE PEN K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 00.0274 00.0274 00.0274 00.0357 -0.0138 -0.0357 -0.0742 -0.0852 -0.0852 -0.0652 -0.0255 -0.0506	GORDON 1.3478 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2677 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601 1.1572 1.1593 1.1648 1.1736 1.1855 1.2000 1.2155	MMA (S) BAHN 1,3435 1.3370 1.3277 1.3160 1.3045 1.2800 1.2674 1.2546 1.2674 1.2134 1.1600 1.1571 1.1571 1.1647 1.1647 1.1785 1.1885 1.1700 1.1592 1.1647 1.1785 1.2000 1.2155 1.2000	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0782 -0.0081 0.0081 0.0084 0.0086 0.0086 0.0086 0.0086 0.0085 0.0085
TEMP (K) -500. 600. 700. 800. 900. 1000. 1250. 1250. 2250. 2250. 2350. 3250. 3350. 3750. 4800. 4750.	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.946 28.953 28.854 28.695 27.328 27.328 26.579 25.721 24.804 23.905 23.108	TIO: 1.0 MOL WT RAHN 24. 952 28. 952 28. 952 28. 952 28. 951 28. 961 28. 961 28. 963 28. 855 28. 8697 27. 947 27. 343 26. 583 25. 725 24. 806 23. 108 22. 462 21. 971 21. 603	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP CJ GORDON 0.2667 0.2782 0.2807 0.2882 0.2953 0.3017 0.3147 0.3260 0.3399 0.3656 0.4151 0.4965 0.401 0.7762 0.6401 0.9436 1.0326 1.0326 1.0326 1.0326 0.9436 0.9436 0.9436 0.9436 0.9436 0.9436 0.9436 0.9436 0.9436	1S OVER 1L/(MOL)(I RAHN 0.2684 0.2781 0.2858 0.2941 0.301 0.3138 0.3596 0.3399 0.3657 0.4151 0.4964 0.9443 1.0385 1.0858 1.0746 0.9990 0.8994	THAN ONE PERI K) -0.9023 0.3294 0.9263 0.8328 0.4064 0.5303 0.2860 0.1227 0.0274 0.0201 0.0495 0.0138 0.0357 0.0742 0.0872 0.0872 0.0872 0.0872 0.0052	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2796 1.2546 1.2546 1.2546 1.1702 1.1601 1.1572 1.1593 1.1604 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736 1.1736	MMA (S) BAHN 1,3435 1,3370 1,3277 1,3160 1,2800 1,2674 1,2546 1,2371 1,2134 1,1702 1,1640 1,1571 1,1592 1,1647 1,1735 1,1655 1,2000 1,2155	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0081 0.0081 0.0084 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086
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TEMP (K) -500. 600. 700. 800. 900. 1000. 1250. 1250. 2250. 2250. 2250. 3250. 3250. 3550. 4500. 4750. 5500.	GORDON 28.952 28.952 28.952 28.952 28.952 28.952 28.951 28.946 28.923 28.854 28.695 27.943 27.328 26.579 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79 25.79	TIO: 1.0 MOL MT RAHN 28.952 28.952 28.952 28.952 28.952 28.951 28.951 28.951 28.966 28.975 28.697 27.947 27.333 25.725 24.806 23.966 23.966 23.966 23.966 23.108 22.462 21.971 21.603 21.514	0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0	20. CP CJ GORDON 0.2660, 2732 0.2782 0.2807 0.2882 0.2953 C.3017 0.3147 0.3147 0.3656 0.4151 0.4965 0.6060 0.7262 0.6401 0.9436 1.07436 1.07439 1.07439 0.9986 0.6902 0.7754 0.7750 0.7761 0.8116	1S OVER (1/10 / 10 / 10 / 10 / 10 / 10 / 10 / 1	THAN ONE PERI K) -0.9023 -0.3294 -0.9263 -0.8328 -0.4064 -0.5303 -0.2860 -0.1227 -0.0201 -0.0495 -0.0138 -0.0495 -0.0138 -0.0138 -0.0357 -0.0742 -0.0830 -0.0852 -0.0652 -0.0405 -0.0225 -0.0405 -0.0225 -0.04062 -0.0495 -0.0401 -0.0225 -0.0495 -0.0495 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830 -0.0830	GORDON 1.3478 1.3355 1.3236 1.3126 1.3028 1.2945 1.27676 1.2546 1.2372 1.2136 1.1889 1.1702 1.1601 1.1573 1.1648 1.1736 1.1736 1.1855 1.2000 1.2155 1.2269 1.2360	#MA (S) BAHN 1,3435 1,3370 1,3277 1,3160 1,3045 1,2800 1,2674 1,2134 1,1838 1,1702 1,1600 1,1571 1,1592 1,1647 1,1735 1,2000 1,2155 1,2000 1,2155 1,2287 1,2354	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0081 0.0081 0.0084 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086 0.0086
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CP C/ GORDON	1S OVER 1L/(HOL)(1) RAHN 0.2684 0.2723 0.2781 0.28941 0.3001 0.3138 0.3256 0.33597 0.4151 0.4964 0.9443 1.0358 1.0746 0.9940 0.8964 0.7265 0.7093 0.8163 0.2684 0.2723 0.2765 0.2816 0.2826 0.4794 0.53138 0.2684 0.2723 0.2765 0.2826 0.4794 0.53138 0.3254 0.3626 0.4794 0.57861 0.6866 1.0429 1.0030 0.9922	THAN ONE PERIK -0.9023 -0.3294 0.9263 0.4328 0.4064 0.5303 0.0274 0.0201 0.0495 0.01327 0.0495 0.01357 -0.0552 -0.0552 -0.0295 -0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0366 0.0295 -0.0564 -0.0497 -0.0494 -0.0494 -0.0494 -0.0434 -0.0454	GORDON 1.347A 1.3355 1.3236 1.3126 1.3028 1.2945 1.2790 1.2670 1.2546 1.2372 1.2136 1.1601 1.1572 1.1601 1.1572 1.1693 1.164A 1.1736 1.1637 1.164A 1.1736 1.2000 1.2155 1.2269 1.2361 1.3355 1.2269 1.2361 1.3355 1.3236 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126 1.3126	BAHN 3.435 1.3370 1.3277 1.3160 1.3045 1.2800 1.2674 1.2546 1.28371 1.1600 1.1571 1.1592 1.1600 1.2155 1.2000 1.2155 1.2000 1.2155 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.255 1.2000 1.2168 1.2000 1.255 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168 1.2000 1.2168	0.3190 -0.1123 -0.3098 -0.2590 -0.1545 -0.1545 -0.0081 -0.0081 -0.0086 -0.0086 -0.0086 -0.0086 -0.00891 -0.1306 -0.1651 -0.3190 -0.1305 -0.1545 -0.2590 -0.1305 -0.1545 -0.0316 -0.0316 -0.0316 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0086 -0.0085 -0.00245

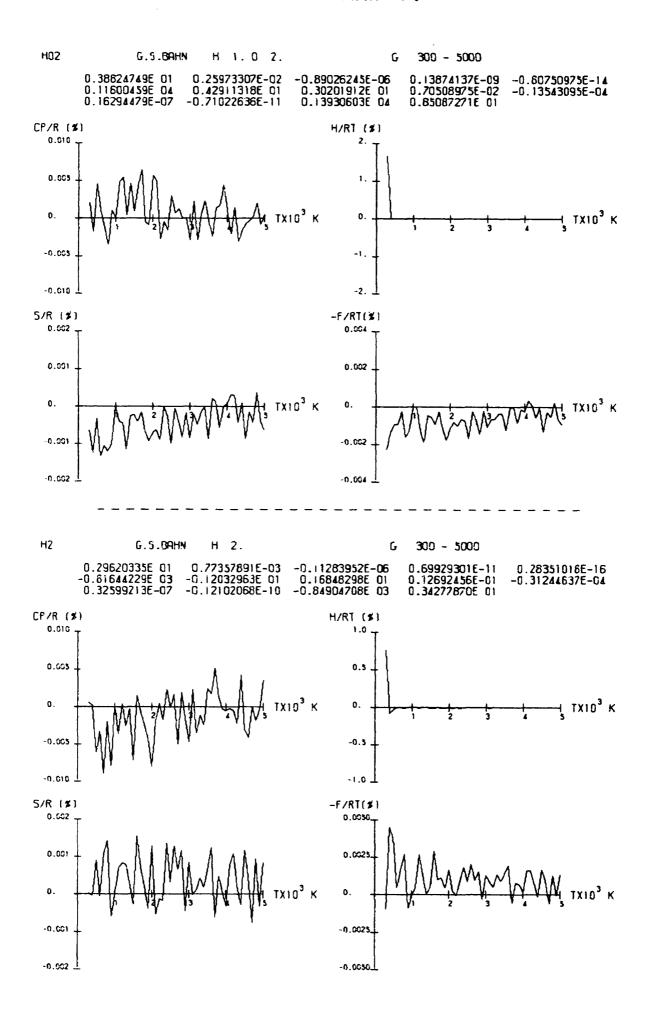
JP-4/AIR	ERA	110= 1.4	ATH			THAN ONE PER			
TEMP (K)	GORDON	HOL HT BAHN	•	GORDON	L/(MOL)(Bahn	K) %	GORDON	BAHN	*
508. 600.	28.913 28.75n	28.914 28.752	-0.0035 -0.0070	0.2982 0.3665	0.3007 0.3658	-0.8384 0.1910		.3049 .2641	0.2599 -0.0396
750.	28.276	28.279	-0.0106	0.5294	0.5259	0.6986		2104	-0.1324
ano.	27.312	27.327	-0.0366	0.6726	0.6697	0.4312		1876	-0-1011
930. 1000.	26.989 26.989	26.909 26.889	-0.0637 0.	0.3693 0.3414	0.3697 0.3404	-n.1083 n.2929		.2627 .2779	-0.0238 -0.0662
1250.	884.45	26.888	0.	0.3403	r.3400	0.0882	1.2774 1.	2777	n.G235
1500. 1750.	26.888 26.887	26.888 26.887	0• 0•	0.3439	0.3439	0. -0.0859		.2737 .2684	n.0079 G.0158
2000.	26.882	26.882	n.	0.3597	0.3601	-0.1112		2603	0.0238
2250. 2500.	26.856 26.747	26.856 26.748	0. -0.0037	0.391n 6.5020	0.3914	-0.1023		2420	0.0241
2750.	26.374	26,376	-0.0076	0.7977	0.7966	0.0598 0.1379		.2016 .1575	n. n.
annn.	25.532	25.536	-0.0157	1.1905	1.1906	-0.0084	1.1415 1.	.1414	0.0088
325c. 3510.	24.272 22.859	24.275 22.861	-0.0124 -0.0087	1.5093	1.5107	-0.0928 -0.1130		.1428 .1541	0.0087 0.0087
3750.	21.659	21.659	0.	1.3550	1.3561	-0.0812	1.1748 1.	. 1748	0.
4000. 4250.	20.867 20.417	26.866 20.416	0.0048 0.0049	1.0013	1.0013	0. 0.0531		.2042 .2339	0. -0.0081
4500.	20.159	20.159	0.	0.6506	0.6502	P.0615		.2476	-0.0160
4750.	19.980	19.980	O.	0.6575	0.6572	0.0456	1.2379 1	2380	-0-0081
5000. 5250.	19.810 19.602	19.602	ր. ն.	0.752n 0.9342	0.7519	n.0133		.2144 .1883	0. 0.0084
5500.	19.315	19.315	0.	1.2231	1.2229	0.0164	1.1663 1.	1662	0.0086
5750. 6000.	18.910 16.348	18.911 18.350	-0.0053 -0.0109	1.6527 2.2527	1.652g 2.2522	0.0424		1495	0.0174 0.0176
O(tott)	10.040	10.070			218328	11.0222	1.1307 1.	.1003	0.0176
~~~		00 011		= 10.					
500. 600.	28.937 28.882	28.937 28.883	0. -0.0035	0.2856 0.3136	0.2881 0.3130	-n.8754 0.1913		.3158 .2951	0.2880 -0.0541
700.	28.703	28.704	-0.0035	0.3825	0.8797	n.7320	1.2544 1.	2567	-0.1834
#30. <b>9</b> 10.	28.259 27.438	28.263 27.450	-0.0142 -0.0437	0.5443 0.6423	0.5390	0.9737 0.2335		.2065 .1951	-0.1577 -0.0502
1000.	26.955	26.958	-0.0111	0.4104	0.4124	-0.4873	1.2484 1.	.2482	0.0160
1250.	26.889 26.888	26.889 26.888	0.	0.3405	0.3402	0.0881	1.2778 1	.2776	-0.0235
1530. 1750.	26.888	26.888	ი. . 0	0.3438	0.3439	-0.0291 -0.0574		.2738 .2689	0.0158
2000.	26.886	26.886	0.	0.3548	0.3551	-0.0846	1.2638 1	.2634	0.0317
2250. 2500.	26.878 26.847	26.878 26.847	0. 0.	0.3667 0.3987	0.3671 0.3990	-0-1091 -0-0752		.2551 .2381	0.0819 0.0162
2750.	26.744	26,745	-0.0037	0.4868	0.4866	0.0411		2071	0.0083
3000.	26.466 25.914	26.468 25.917	-0.0076	0.6695 0.8950	0.6687	0.1195	1.1749 1. 1.1597 1	.1749 .1597	0.
	25.102	25.106	-0.0116 -0.0159	1.0901	1.0906	-0.0223		1580	0.0086
3750.	24.123	24.125	-0.0083	1.2222	1.2232	-0.0818	1.1637 1	.1637	0
4000. 4250.	23.102 22.178	23.103 22.178	-n.gn43 D.	1.2530 1.1685	1.2540	-0-0798 -0-0428		.1745 .1898	0.0085
4590.	21.442	21.442	0 •	1.0135	1.0136	-0.0099	1.2078 1	2078	0 -
4750. 5000.	20.537	20.909 20.537	<u>0.</u>	0.7582	0.8604	0.0116 -0.0132		2254	0.0162
5250.	20.265	20.265	,ñ	0.7208	0.7215	-0-0971	1.2373 1	. 2369	0.0323
5500. 5750.	20.041 19.823	20.041	n. -0.0050	0.7464	0.7479	-0.2010 -0.2643		.2263 .2096	0.0452 0.0909
6000.	19.580	19.581	-0.0051	0.9822	0.9848	-0.2647		1918	0.0922
						k			
JP-4/AIR -	ERA	710= 1.4 MOL WT	<u> АТН</u>			THAN DNE PER		A (S)	
JP-4/AIR - TEMP (K)	ERA GORDON	T10= 1.4 HOL WT BAHN	ATH S		IS OVER			A (S) Bahn	
TEMP (K)	GORDON	HOL WT		CP CI GORDON	BAHN	(K) 38	GORDON	BAHN	
TEMP (K) 500.	GORDON 28.940 28.901	28.940 28.902	0. -0.0035	CP C/ GORDON 0.2838 0.3057	0,2864 0.3051	-0.9161 0.1963	GORDON 1,3212 1 1.8000 1	3174 -3007	0.2476
500. 600.	28.940 28.901 28.771	28.940 28.902 28.772	0. -0.0035 -0.0035	CP C/ GORDON 0.2838 0.3057 0.3581	0.2864 0.3051 0.3555	-0.9161 0.1963 0.7261	GORDON 1,3212 1 1.3000 1 1.2656 1	3174 -3007 -2680	0.2476 -0.0588 -0.1496
TEMP (K) 500. 600. 700. 800. 900.	28.940 28.901 28.771 28.440 27.745	#OL WT BAHN 28,940 28,902 28,772 26,443 27,757	0. -0.0035 -0.0035 -0.0105 -0.0433	CP C/ GORDON 0.2838 0.3057 0.3581 0.4801 0.6300	0,2864 0,3051 0,3555 0,4757 0,6258	-0,9161 0,1963 0,7261 0,9165 0,6667	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.1954 1	3174 .3007 .2680 .2215 .1964	0.2676 -0.0538 -0.1896 -0.1722 -0.0837
500. 600. 700. 800. 900.	28.940 28.901 28.771 28.440 27.745 27.085	8,940 28,940 28,92 28,772 28,443 27,757 27,093	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295	CP C/ GORDON 0.2838 0.3057 0.3561 0.4801 0.6300 0.5039	0,2864 0.3051 0.3555 0.4757 0.6258 0.5070	-0,9161 0,1963 0,7261 0,9165 0,6667 -0,6152	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.1954 1 1.2731 1	3174 .3007 .2680 .2215 .1964 .2228	0,2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245
TEMP (K) 500. 600. 700. 800. 900.	GORDON 28.940 28.901 28.771 28.440 27.745 27.085 26.8890 26.888	#OL WT BAHN 28,940 28,902 28,772 26,443 27,757	0. -0.0035 -0.0035 -0.0105 -0.0433	CP C/ GORDON 0.2838 0.3057 0.3581 0.4801 0.6300	0,2864 0,3051 0,3555 0,4757 0,6258	-0,9161 0,1963 0,7261 0,9165 0,6667	GARM GORDON 1.3000 1 1.2656 1 1.2194 1 1.1954 1 1.2731 1 1.2771 1	8AHN .3174 .3007 .2680 .2215 .1964 .2228 .2774 .2738	0.2676 -0.0538 -0.1896 -0.1722 -0.0837
TEMP (K) 500. 600. 700. 800. 900. 1000. 1250. 1750.	28.940 28.901 28.771 28.775 27.745 27.745 27.689 26.890 26.888	MOL MT BAHN 28.940 28.902 28.772 28.443 27.757 27.093 26.890 26.888 26.888	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.	CP C/ GORDON 0.2838 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3436 0.3485	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3407 0.3487	-0.9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0980 -0.0291 -0.0574	GARM GORDON 3.3212 1 1.3000 1 1.2656 1 1.2194 1 1.1954 1 1.2731 1 1.2771 1 1.2738 1 1.2692 1	3174 .3007 .2680 .2215 .1964 .2228 .2774 .2738 .2690	0,2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.0158
TEMP (K) 500. 600. 700. 800. 1000. 1250. 1500. 1750. 2000.	GORDON 28.940 28.901 28.771 28.440 27.745 27.085 26.8890 26.888	MOL WT BAHN 28,940 28,902 28,772 28,443 27,757 27,093 26,890 26,888 26,888 26,888	5 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.	CP C/ GORDON  0.2838 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3438 0.3485 0.3485	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3487 0.3487 0.3545	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2731 1 1.2738 1 1.2658 1 1.2642 1 1.2642 1	3174 .3007 .2680 .2215 .1964 .2228 .2774 .2738 .2690 .2638	0.2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.0158
TEMP (K)  500. 600. 700. 800. 900. 1060. 1250. 1750. 2000. 2250.	GORDON  28.940 28.901 28.771 28.440 27.745 27.085 26.890 26.888 26.887 26.887 26.881	MOL MT BAHN 28.940 28.902 28.772 28.443 27.757 27.093 26.888 26.888 26.888 26.881 26.881 26.881	5 -0.0035 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.00000000000000000000000000000000000	CP C/ GORDON  1.2838 0.3057 0.3559 0.4801 0.6300 0.5039 0.3410 0.3428 0.3485 0.3541 0.3636	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3407 0.3489 0.3487 0.3545 0.3640 0.3869	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.1035	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2231 1 1.2731 1 1.2738 1 1.2738 1 1.2642 1 1.2642 1 1.2573 1 1.2642 1	8AHN .3174 .3007 .2680 .2215 .1964 .2228 .2734 .2738 .2690 .2638 .2690 .2439	0,2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.00158 0.0316 0.0318
TEMP (K)  500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2570. 2750.	GORDON  28.940 28.971 28.771 28.440 27.745 27.085 26.888 26.888 26.887 26.861 26.859	MOL MT BAHN 28.940 28.902 28.772 28.443 27.757 27.093 26.888 26.888 26.887 24.881 26.8860 26.790	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0. 0. 0. 0. 0. 0. 0.	CP C/ GORDON  0.2838 0.3057 0.3581 0.4801 0.6320 0.5039 0.34410 0.3438 0.3451 0.35541 0.3636 0.3865	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3487 0.3487 0.3640 0.3640 0.469	-0,9161 0,1963 0,7261 0,9165 0,6667 -0,6152 0,0880 -0,0291 -0,0574 -0,1130 -0,1005	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2731 1 1.2738 1 1.2738 1 1.2642 1 1.2642 1 1.2573 1 1.2642 1 1.2573 1 1.2442 1 1.2195 1	8AHN .3174 .3007 .2680 .2215 .1964 .2228 .2774 .2738 .2690 .2688 .2690 .2688 .2439 .2194	0,2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.0316 0.0318 0.0241 0.0082
TEMP (K)  500.  700.  800.  900.  100.  1250.  1750.  2000.  2250.  2510.	GORDON  28.940 28.901 28.771 28.440 27.745 26.890 26.888 26.887 26.887 26.789 26.789 26.789	HOL WT 8AHN 28,940 28,902 28,772 28,443 27,757 27,093 26,880 26,881 26,881 26,881 26,881 26,860 26,790 26,599 26,195	5 -0.0035 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.00000000000000000000000000000000000	CP C/ GORDON 0.2888 0.3057 0.3581 0.4801 0.5039 0.3410 0.3486 0.3485 0.3581 0.3686 0.3865 0.4469 0.5792 0.7666	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3487 0.3545 0.3640 0.3869 0.4469 0.7660	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.1035	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2951 1 1.2771 1 1.2738 1 1.2738 1 1.2642 1 1.2642 1 1.2542 1 1.2542 1 1.2542 1 1.2542 1 1.2542 1 1.2542 1 1.2642 1 1.2738 1	BAHN .3174 .3007 .2680 .2215 .1964 .2228 .2774 .2738 .2690 .2638 .2569 .2439 .2194	0,2676 -0.0538 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.00158 0.0316 0.0318
TEMP (K)  500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2570. 3070. 3250. 3550.	GORDON  28.940 28.971 28.771 28.440 27.745 27.085 26.889 26.888 26.887 26.881 26.859 26.769 26.558	HOL WT BAHN 28.940 28.772 28.772 28.443 27.757 27.093 26.888 26.888 26.888 26.881 26.861 26.860 26.790 26.195 26.195 25.558	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C/ GORDON  9.288 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3488 0.3488 0.3488 0.3564 0.3668 0.3668 0.3668 0.7666 0.7666	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3487 0.3487 0.3488 0.3487 0.3864 0.3864 0.5786	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.1035 0.0783 -0.0106	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2771 1 1.2738 1 1.2771 1 1.2692 1 1.2692 1 1.2642 1 1.2643 1 1.2644 1 1.2646 1 1.2646 1	BAHN .3174 .3007 .2680 .2215 .1964 .2228 .2274 .2738 .2688 .2698 .2439 .2194 .1884 .1686 .1680	0,2676 -0.0538 -0.1896 -0.1792 -0.0837 0,0245 -0.0235 0.00158 0.0318 0.0241 0.0082 0.0082
TEMP (K) 500. 600. 700. 800. 900. 1000. 1250. 1500. 1250. 2510. 2510. 2510. 3250. 3250.	GORDON  28.940 28.901 28.771 28.440 27.745 26.890 26.888 26.887 26.887 26.789 26.789 26.789	HOL WT 8AHN 28,940 28,902 28,772 28,443 27,757 27,093 26,880 26,881 26,881 26,881 26,881 26,860 26,790 26,599 26,195	5 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.00 0.00 0.0037 -0.0037 -0.0037 -0.0038 -0.0076	CP C/ GORDON  0.2838 0.3057 0.3581 0.4801 0.6300 0.5039 0.34410 0.3488 0.3485 0.35541 0.3636 0.3865 0.4469 0.7792 0.7660 0.9431 1.0797 1.1573	0.2864 0.3051 0.3555 0.4757 0.6258 0.550 0.5407 0.3487 0.3540 0.3640 0.3640 0.3640 0.3640 0.3640 0.3640 0.469 0.469	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.1730 -0.1100 -0.1035 0.0783 -0.0783 -0.0106	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2731 1 1.2738 1 1.2738 1 1.2642 1 1.2642 1 1.2642 1 1.2573 1 1.2642 1 1.2642 1 1.2643 1 1.2656 1 1.1630 1 1.1630 1 1.1630 1 1.1630 1	BAHN .3174 .8007 .2680 .2215 .1964 .2228 .2774 .2738 .2690 .2638 .2569 .2439 .2144 .1884 .1686	0.2676 -0.0538 -0.1896 -0.1722 -0.0837 0.0245 -0.0318 0.0318 0.0241 0.0082 0.00
TEMP (K)  500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2570. 2750. 3000. 3250. 3500. 3750. 4000.	GORDON  28.940 28.971 28.440) 27.745 27.085 26.890 26.888 26.888 26.887 26.789 26.789 26.789 26.789 26.789 26.789	HOL WT BAHN 28.940 28.902 28.772 28.443 27.757 27.093 26.888 26.888 26.881 26.861 26.860 26.790 26.195 26.195 25.558 24.741 23.829 22.923	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C/ GORDON  0.288 0.3057 0.3581 0.4801 0.6300 0.5039 0.3418 0.3485 0.3485 0.3541 0.3686 0.3665 0.4469 0.5792 0.7666 0.9441 1.0797 1.1573	0.2849 0.3051 0.3055 0.3555 0.4757 0.6258 0.5070 0.3487 0.3487 0.3489 0.3489 0.4660 0.4660 0.4786 0.7660 0.7660 0.7660 0.4782 1.1581 1.1581	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.1100 -0.1035 0.0783 -0.0106 -0.0463 -0.0693	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2231 1 1.2738 1 1.2738 1 1.2738 1 1.2738 1 1.2642 1 1.2542 1 1.2542 1 1.2542 1 1.2642 1 1.2666 1 1.1686 1 1.1686 1 1.1630 1 1.1630 1 1.1630 1 1.1733 1 1.1733 1	BAHN .3174 .3007 .2680 .2215 .1964 .2228 .2774 .2690 .2638 .2738 .2569 .2194 .1884 .1686 .1630 .1656 .1758 .1848	0.2474 -0.0588 -0.1896 -0.1722 -0.0837 0,0245 -0.0235 0.0158 0.0316 0.0318 0.0241 0.0082 0.0082
TEMP (K) 500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2250. 2350. 3750. 3750. 3750.	28.940 28.940 28.901 28.771 28.440 27.745 26.889 26.888 26.887 26.881 26.859 26.789 26.598 26.598 26.598 26.598 26.789 26.598	HOL WT 8AHN 28,940 28,902 28,772 28,443 27,757 27,093 26,889 26,888 26,887 26,881 26,860 26,599 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199 26,199	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP C/ GORDON  0.2888 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3486 0.3486 0.3686 0.3686 0.3686 0.4469 0.7792 1.1573 1.1573 1.0766	0.2864 0.3051 0.3555 0.4557 0.6258 0.5070 0.3487 0.3487 0.3467 0.3467 0.3469 0.4469 0.469 0.766 0.9432 1.1581 1.1580	-0,9161 0.1963 9.7261 0.9165 9.6667 -0.6165 0.0580 -0.0291 -0.0574 -0.1130 -0.1130 -0.1035 0.0783 -0.0106 -0.0463 -0.0691 -0.0693 -0.0372	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.1954 1 1.2731 1 1.2731 1 1.2738 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2643 1 1.2643 1 1.2644 1 1.2195 1 1.1686 1 1.1680 1 1.1680 1 1.1681 1 1.1683 1 1.1684 1	BAHN .3174 .3007 .2680 .2215 .1964 .2228 .2774 .2788 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .2638 .26	0.2676 -0.0536 -0.1896 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0158 0.0316 0.0316 0.0316 0.0082 0.000000000000000000000000000000
TEMP (K)  500. 600. 700. 800. 900. 1060. 1250. 1750. 2250. 2250. 2350. 3500. 3750. 4000. 4250. 4500. 4500.	GORDON  28.940 28.901 28.771 28.440 27.745 27.085 26.889 26.888 26.887 26.861 26.859 26.769 26.769 26.793 25.555 24.738 23.827 29.922 22.116 21.465	MOL WT 8AHN 28.940 28.902 28.772 28.4772 27.757 27.093 26.888 26.888 26.887 26.880 26.790 26.195 25.558 24.741 23.829 22.116 21.464 21.464 20.972	5 -0.0035 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0040 -0.0121 -0.0121 -0.0044 -0.0044 -0.0044 -0.0047	CP C/GORDON  0.2838 0.3057 0.3591 0.4801 0.6300 0.5039 0.3410 0.3495 0.3485 0.3541 0.3636 0.4469 0.792 0.7666 0.9431 1.0797 1.1573 1.0766 0.99573 0.84336	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3487 0.3489 0.3489 0.3489 0.469 0.469 0.469 0.1581 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660 0.7660	-0,9161 0.1963 9,7261 0.9165 0.6667 -0.6165 0.0880 -0.0291 -0.0574 -0.1180 -0.1180 -0.1180 -0.0376 0.0783 -0.0106 -0.0463 -0.0463 -0.0491 -0.0693 -0.0329 -0.0356	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2738 1 1.2771 1 1.2652 1 1.2642 1 1.2733 1 1.2642 1 1.2733 1 1.2195 1 1.1684 1 1.1686 1 1.1630 1 1.1686 1	8AHN 3174 3007 2680 2215 1964 2228 2774 2738 2690 2439 2439 2439 2194 1686 1636 1636 1636 1738 2928 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938 2938	0.2676 -0.0538 -0.1896 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0158 0.0316 0.0318 0.0241 0.0082 0.0.0081
TEMP (K) 500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2250. 3750. 3000. 3250. 4000. 4250. 4500. 4750. 5000. 5250.	GORDON  28.940 28.901 28.771 28.440 27.745 27.085 26.889 26.888 26.887 26.881 26.859 26.789 26.598 26.193 25.555 24.738 23.827 22.922 22.116 21.465 20.607	HOL WT 8AHN 28,940 28,902 28,772 28,443 27,757 27,093 26,889 26,888 26,888 26,887 26,860 26,790 26,195 26,195 24,195 25,558 24,741 23,829 22,136 21,464 20,972 21,464 20,607	5 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0047 -0.0117 -0.0121 -0.0121 -0.0044 -0.0047 0.0047	CP C/ GORDON  0.2808  0.3057  0.3581  0.4801  0.5030  0.3438  0.3485  0.3485  0.35841  0.3686  0.3686  0.469  0.7792  0.7697  1.1572  1.1572  1.0797  0.8436  0.9573  0.8436	0.2840 0.3051 0.3555 0.4757 0.6258 0.550 0.5407 0.3487 0.3487 0.3467 0.3469 0.4469 0.5786 0.766 0.9432 1.0802 1.1581 1.1560 0.9575 0.8439	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.1130 -0.1130 -0.1135 0.0136 0.0783 -0.0106 -0.0463 -0.0463 -0.0693 -0.0209 -0.0326 -0.0209	GARM GORDON 1.3212 1.3000 1.2656 1.2194 1.2731 1.2731 1.2738 1.2771 1.2642 1.2642 1.2573 1.2642 1.2573 1.2642 1.2642 1.2573 1.2642 1.2642 1.2656 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630 1.1630	8AHN 3174 3007 2685 12215 1964 2228 2778 2638 2638 2569 2439 2194 11884 11686 11636 11733 11992 2148 2248 2248 2248 2369	0.2676 -0.0536 -0.1896 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0158 0.0316 0.0316 0.0324 0.0082 0.0.0082 0.0.0082
TEMP (K) 500. 600. 700. 800. 900. 1060. 1250. 1500. 2250. 2250. 2250. 3000. 3250. 3750. 4000. 4250. 4750. 5000. 5250. 5000.	GORDON  28.940 28.901 28.771 28.440 27.745 26.890 26.888 26.887 26.789 26.789 26.789 26.789 26.789 26.789 26.193 25.555 24.738 23.827 22.2116 21.465 20.807 20.807 20.807	HOL WT 8AHN 28,940 28,902 28,772 26,443 26,890 26,888 26,887 26,880 26,790 26,599 26,195 25,558 24,741 23,829 22,123 22,116 21,464 21,464 20,67 20,087	5 -0.0035 -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	CP CC GORDON  0.2838 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3438 0.3485 0.3685 0.3685 0.3665 0.4469 0.5792 1.1573 1.1552 1.0766 0.9573 1.0767 0.9573 0.8436 0.7677 0.77423 0.7663	0.2864 0.3051 0.3555 0.4757 0.6258 0.5070 0.3439 0.3469 0.3469 0.3469 0.469 0.786 0.786 0.786 0.786 0.786 0.746 0.7441 0.724	-0,9161 0.1963 9,7261 0.9165 9,6667 -0,6165 0.0580 -0,0291 -0,0574 -0,1130 -0,1130 -0,11035 0.0783 -0,0106 -0,0463 -0,0691 -0,0693 -0,0356 -0,0356 -0,0356 -0,0356 -0,0356 -0,0356	GARM. GORDON  1.3212 1.3000 1.2656 1.2194 1.1954 1.2731 1.2731 1.2738 1.2771 1.2738 1.2692 1.2642 1.2573 1.2642 1.2692 1.2642 1.2692 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2650 1.1733 1.1630 1.1650 1.1733 1.1630 1.1655 1.1733 1.1630 1.1655 1.1733 1.1630 1.1655 1.1235 1.2656 1.12355 1.2266 1.2365 1.2365 1.2365 1.2365	8AHN 3174 3007 2269 2215 1964 2228 2774 2778 2690 2638 2774 1884 1686 1656 1733 1848 1992 2148 2285 2285 2360 2345	0.2676 -0.0536 -0.1896 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0316 0.0316 0.0316 0.0316 0.0082 0.0.0081 0.0082 0.0081 0.0089 0.0081
TEMP (K)  500. 600. 700. 800. 1000. 1250. 1750. 2000. 2250. 2570. 3070. 3250. 3750. 4000. 4250. 4750. 5000. 5250.	GORDON  28.940 28.901 28.771 28.440 27.745 27.085 26.880 26.888 26.887 26.859 26.789 26.799 26.798 26.798 26.193 25.555 24.738 23.827 22.2116 21.465 20.607	HOL WT 8AHN 28.940 28.772 28.443 27.757 27.093 26.888 26.888 26.881 26.881 26.861 26.790 26.599 26.195 25.558 24.741 23.829 22.923 22.116 21.464 20.972 20.607 20.326	5 -0.0035 -0.0035 -0.0035 -0.0433 -0.0295 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0047 -0.0047 -0.0049	CP CC GORDON  0.2858 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3438 0.3485 0.35641 0.3666 0.4469 0.75792 0.7666 0.9431 1.0797 1.1573 1.1592 1.0766 0.9431 1.0797 1.1573 0.8436 0.7677	0.2864 0.3051 0.3055 0.3555 0.4757 0.6258 0.5070 0.3467 0.3467 0.3469 0.466 0.766 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786 0.5786	-0,9161 0,1963 0,7261 0,9165 0,6667 -0,6152 0,0880 -0,0291 -0,0574 -0,1130 -0,1035 0,0783 -0,0106 -0,0463 -0,0463 -0,0463 -0,0463 -0,0356 -0,0356 -0,0356 -0,0356 -0,0172	GARM. GORDON  1.3212 1.3000 1.2656 1.2194 1.1954 1.2731 1.2731 1.2738 1.2771 1.2738 1.2692 1.2642 1.2573 1.2642 1.2692 1.2642 1.2692 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2642 1.2733 1.2650 1.1733 1.1630 1.1650 1.1733 1.1630 1.1655 1.1733 1.1630 1.1655 1.1733 1.1630 1.1655 1.1235 1.2656 1.12355 1.2266 1.2365 1.2365 1.2365 1.2365	8AHN 3174 3007 2607 2215 1964 2215 2228 2774 2738 2638 2568 2569 2194 1636 1630 1630 1636 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948 1948	0.2674 -0.0538 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0158 0.0316 0.0318 0.0241 0.0082 0.0.0000000000000000000000000000
TEMP (K) 500. 600. 700. 800. 1000. 1250. 1500. 1750. 2000. 2250. 2570. 3010. 3250. 3590. 3750. 4500. 4500. 4500. 5750. 5000. 5750. 6000.	GORDON  28.940 28.901 28.771 28.440 27.745 27.085 26.889 26.888 26.887 26.789 26.789 26.789 26.789 26.789 26.789 26.789 26.193 25.555 24.738 23.827 22.2116 21.465 20.607 20.325 20.085	HOL WT 8AHN 28,940 28,902 28,772 28,443 27,757 26,889 26,888 26,888 26,887 26,887 26,887 26,887 26,599 26,199 26,199 24,195 24,741 23,829 22,923 22,116 21,464 20,972 20,607 20,326 20,087 19,856	0. -0.0035 -0.0035 -0.0105 -0.0433 -0.0295 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CP CF GORDON  0.288 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3438 0.3485 0.3686 0.3686 0.3686 0.17697 1.1573 1.1572 1.0766 0.9573 0.8436 0.7677 0.7423 0.8436 0.7693 0.84392	0.2864 0.3051 0.3555 0.4757 0.6258 0.550 0.5407 0.3487 0.3487 0.3487 0.3469 0.469 0.766 0.9432 1.0802 1.1581 1.1560 1.1581 1.1570 0.9432 1.0802 1.0802 1.0802 1.0802 1.0802	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.1130 -0.1100 -0.1035 0.0783 -0.0106 -0.0463 -0.0463 -0.0693 -0.0209 -0.0356 -0.1172 -0.2425 -0.4357	GARM GORDON 1.3212 1 1.3000 1 1.2656 1 1.2194 1 1.2731 1 1.2731 1 1.2731 1 1.2638 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2642 1 1.2630 1 1.1686 1 1.1680 1 1.1686 1 1.1630 1 1.	BAHN 3174 3007 2269 2215 1964 2273 2738 2690 2215 2738 2690 2439 2439 2439 2439 1686 1630 1656 1733 1848 1948 2219 2219 2329 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2439 2448 2448 2448 2448 2448 2448 2448 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449 2449	0.2676 -0.0538 -0.1896 -0.1722 -0.0837 0.0245 -0.0235 0.0158 0.0316 0.0316 0.0324 0.0082 0.0.0081 0.0082 0.0081 0.0809 0.1142 0.1403
TEMP (K)  500. 600. 700. 800. 900. 1000. 1250. 1750. 2250. 2250. 2350. 3350. 4000. 4250. 4500. 4750. 5000. 5250. 5750. 6000.	28.940 28.901 28.971 28.440 27.745 26.890 26.888 26.887 26.887 26.789 26.789 26.789 26.783 27.782 28.116 21.465 24.738 23.827 22.922 22.116 21.465 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.601 20.605 20.601	HOL WT 8AHN 28.940 28.902 28.772 28.443 26.890 26.888 26.888 26.888 26.888 26.887 26.890 26.790 26.599 26.195 25.558 24.741 23.829 22.116 21.464 20.972 20.407 20.407 20.407 20.407 20.407 20.407 20.407 20.407	5 -0.0035 -0.0035 -0.0035 -0.0433 -0.0295 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0037 -0.0049 -0.0047 -0.0049 -0.0049 -0.0050 -0.0050	CP C/GORDON  0.2838 0.3057 0.3581 0.4801 0.6300 0.5039 0.3410 0.3485 0.3561 0.3665 0.4469 0.75792 0.7666 0.9431 1.0797 1.1573 1.1552 1.0766 0.9753 0.8436 0.76793 0.7693 0.7693	0.2844 0.3051 0.3555 0.3555 0.4757 0.6258 0.5070 0.3487 0.3489 0.3489 0.4469 0.4469 0.4469 0.4766 0.7666 0.9786 0.7666 0.9786 0.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1581 1.1582 1.1582 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583 1.1583	-0,9161 0.1963 0.7261 0.9165 0.6667 -0.6152 0.0880 -0.0291 -0.0574 -0.1130 -0.11035 0.0783 -0.0106 -0.0463 -0.0463 -0.0463 -0.0463 -0.0209 -0.0356 -0.0209 -0.0356 -0.1172 -0.0297 -0.1356	GARM.  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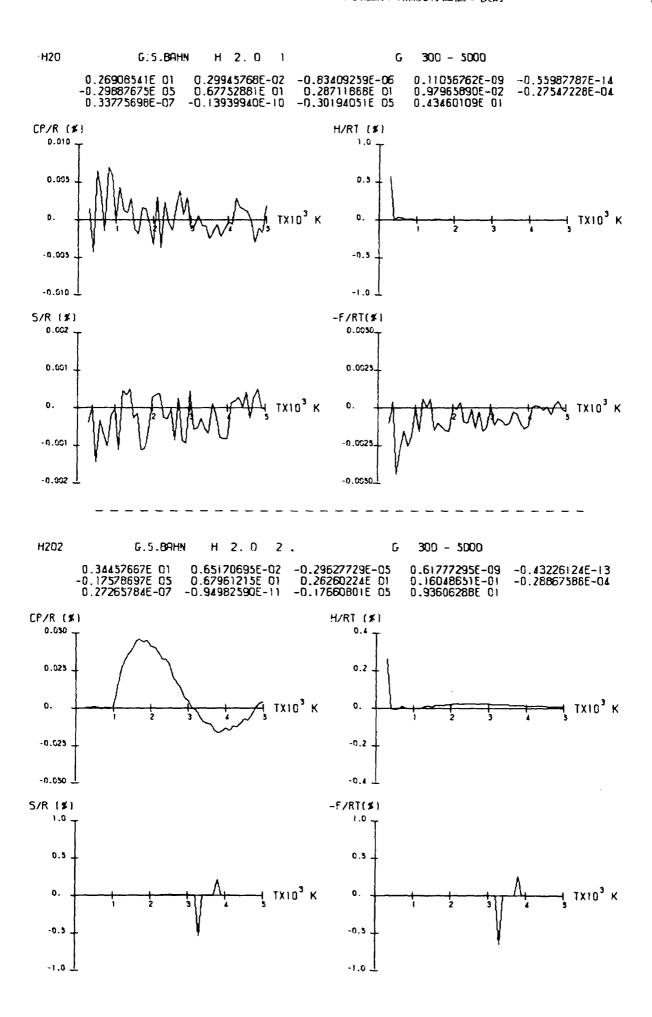
## 付録 - D-

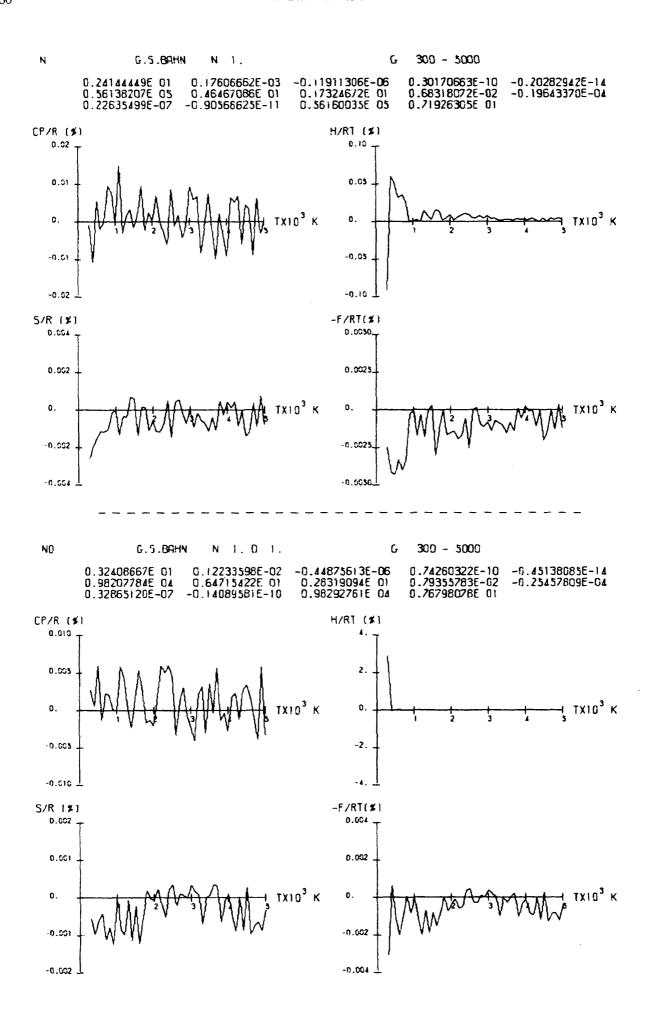
G. S. Bahn熱化学近似テーブル化学種の多頂係数値と、多頂近似式による計算値とテーブル値の偏差図

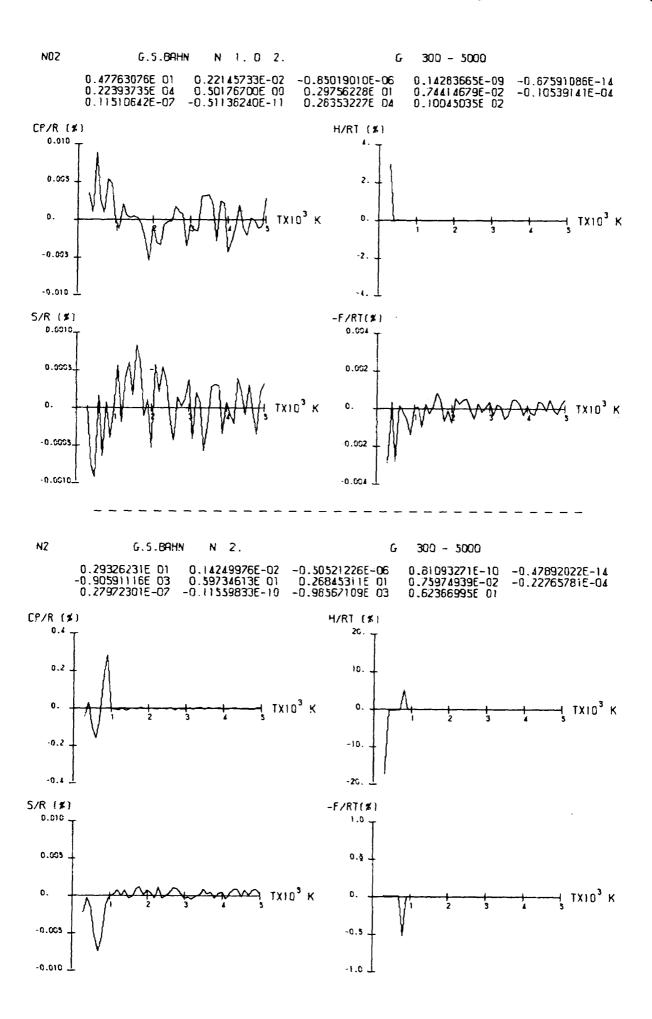


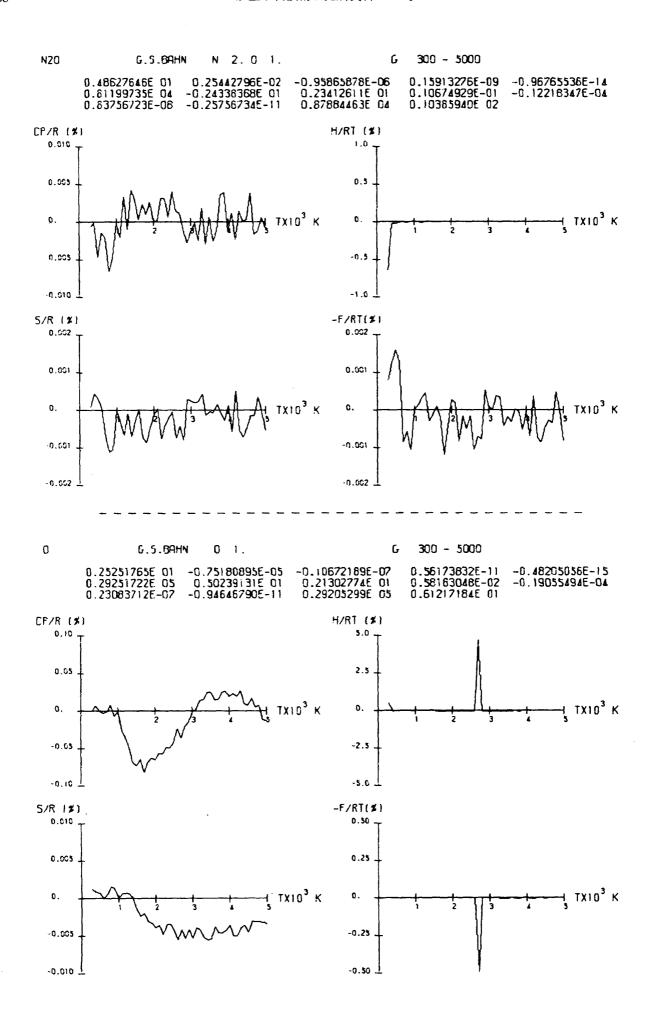


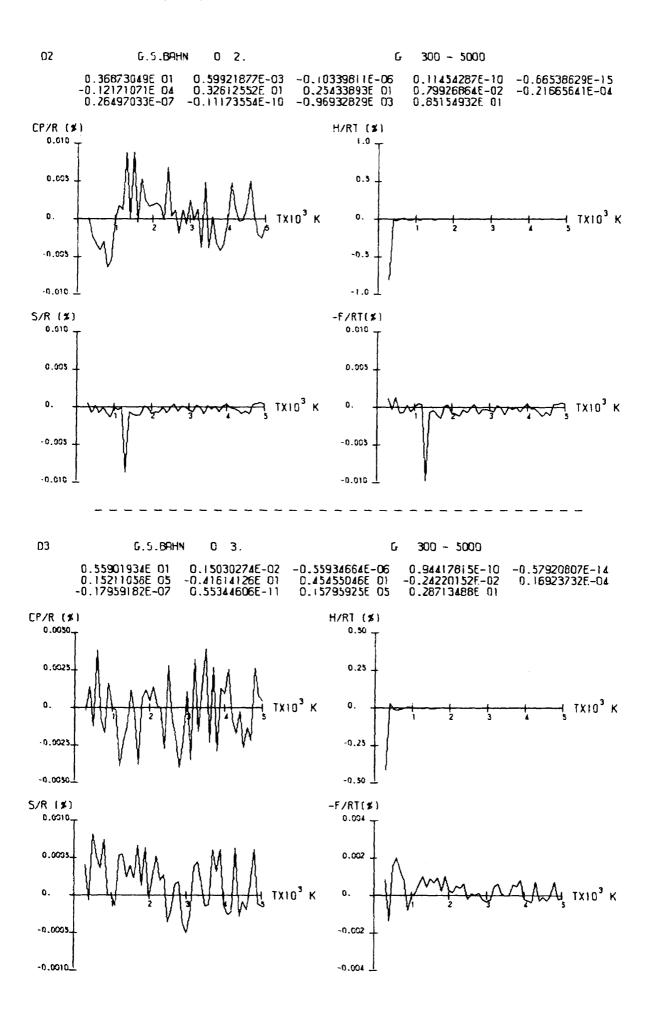


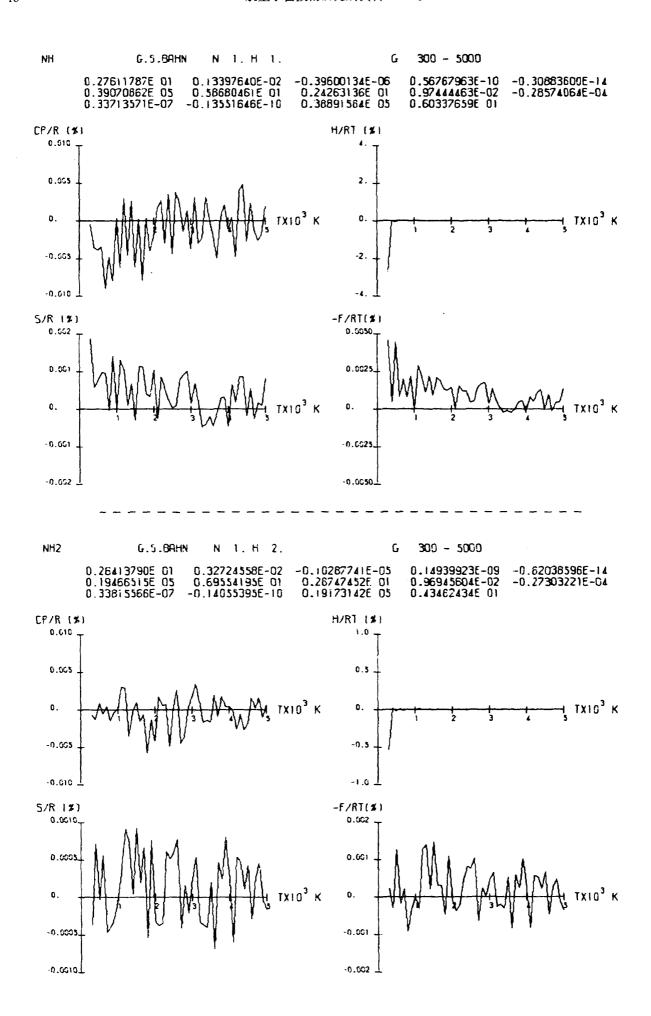


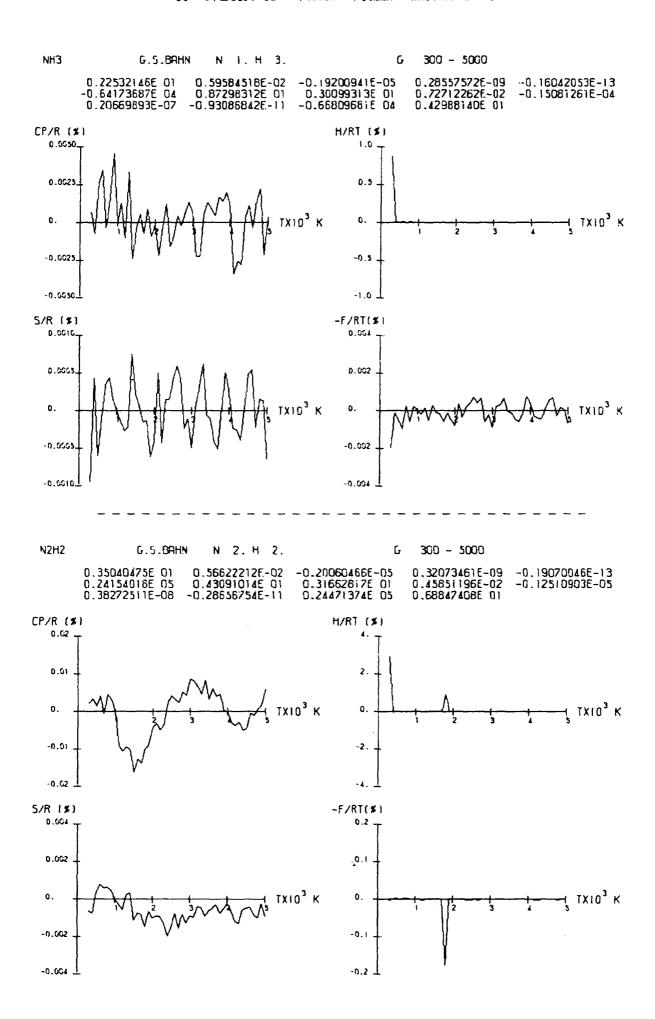


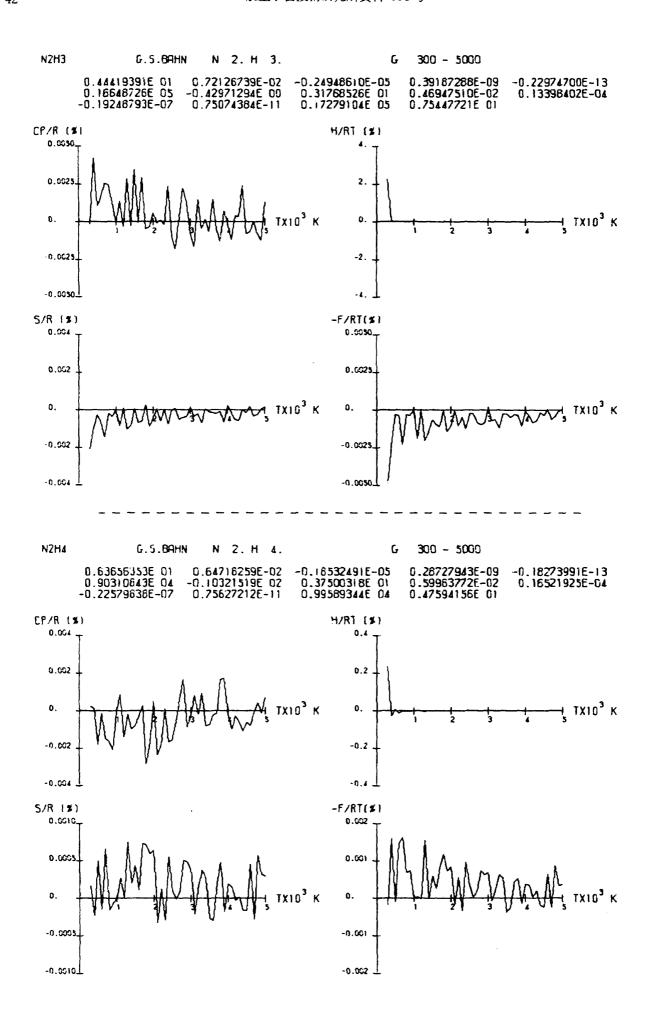


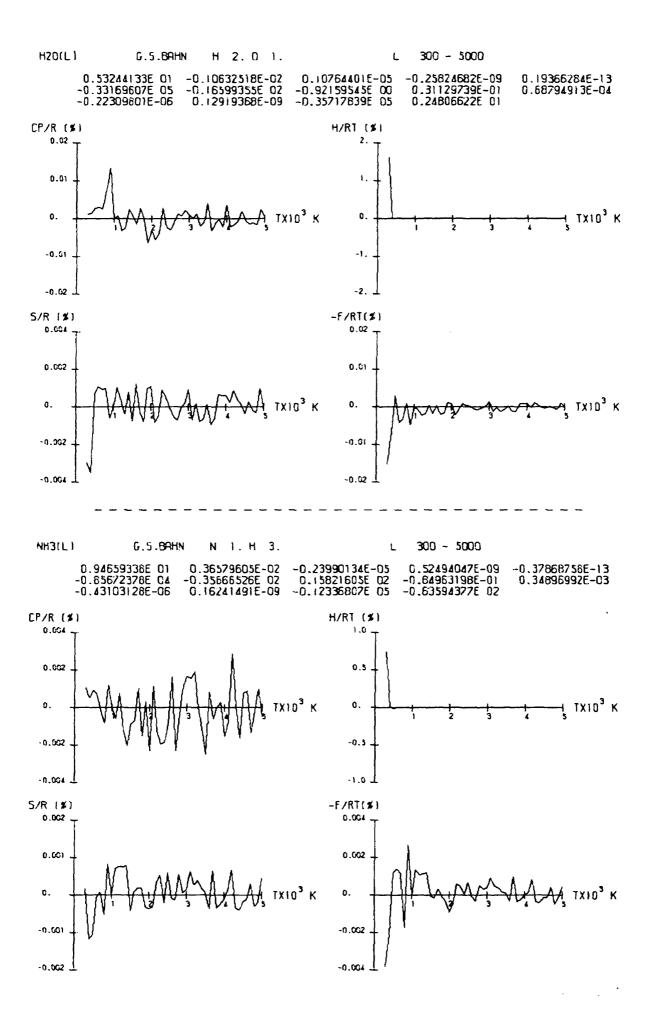


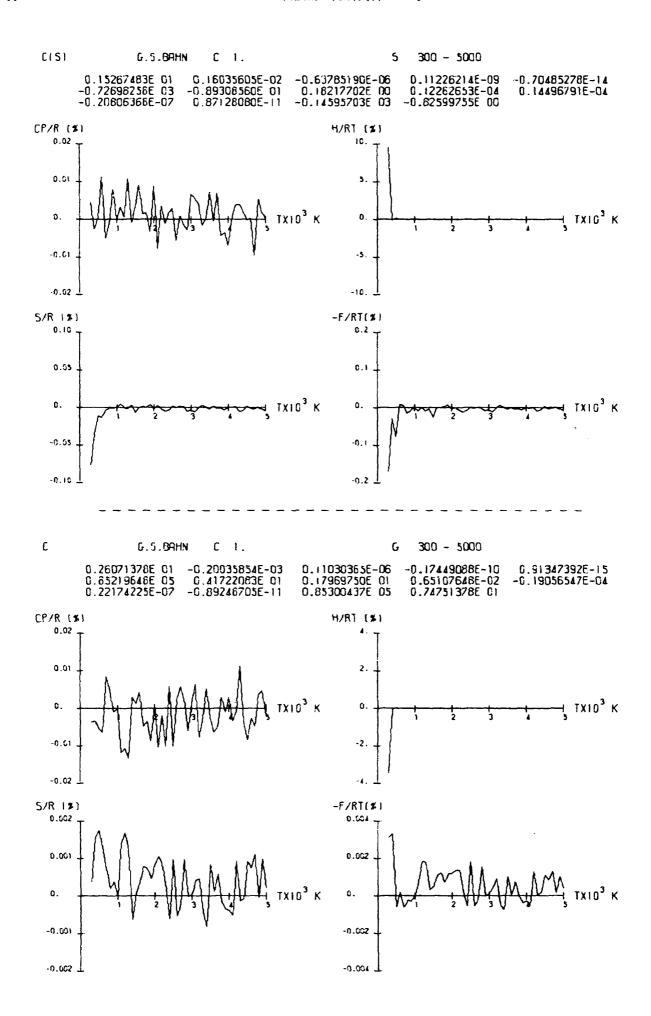


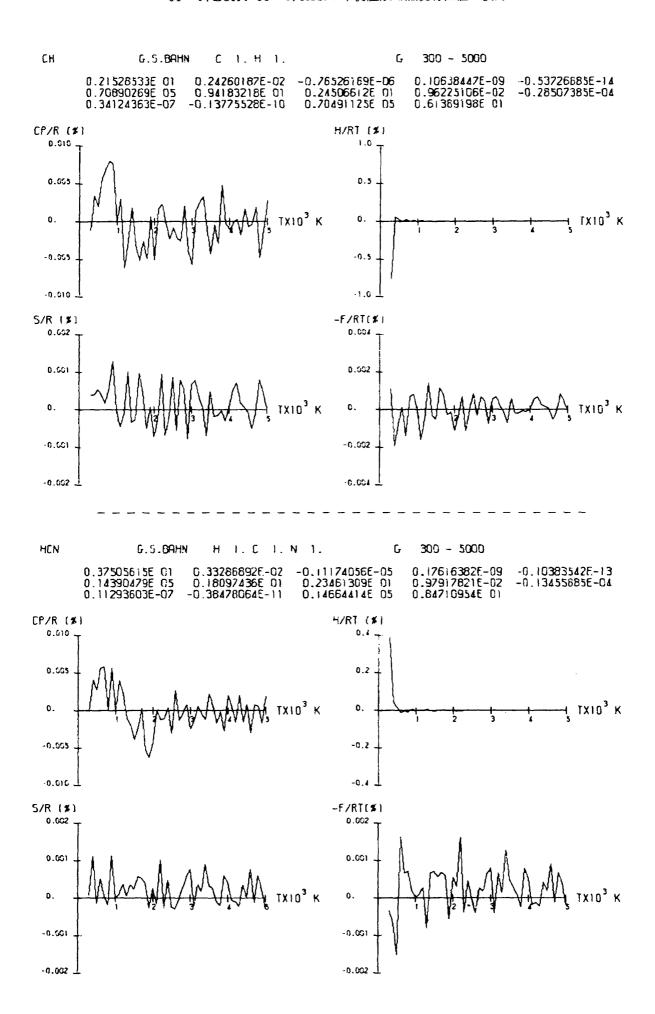


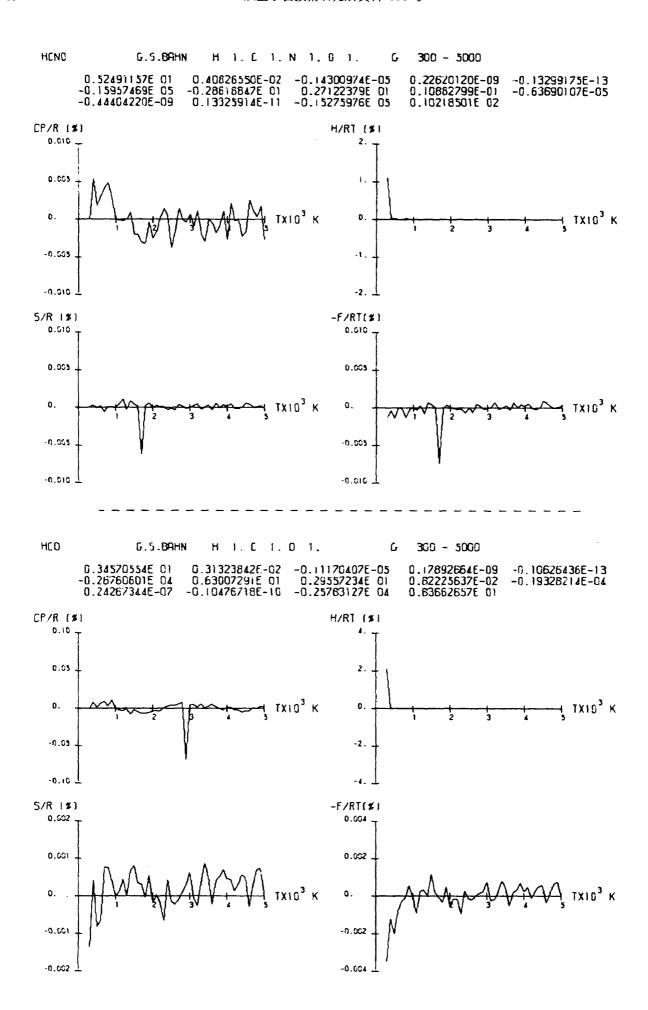


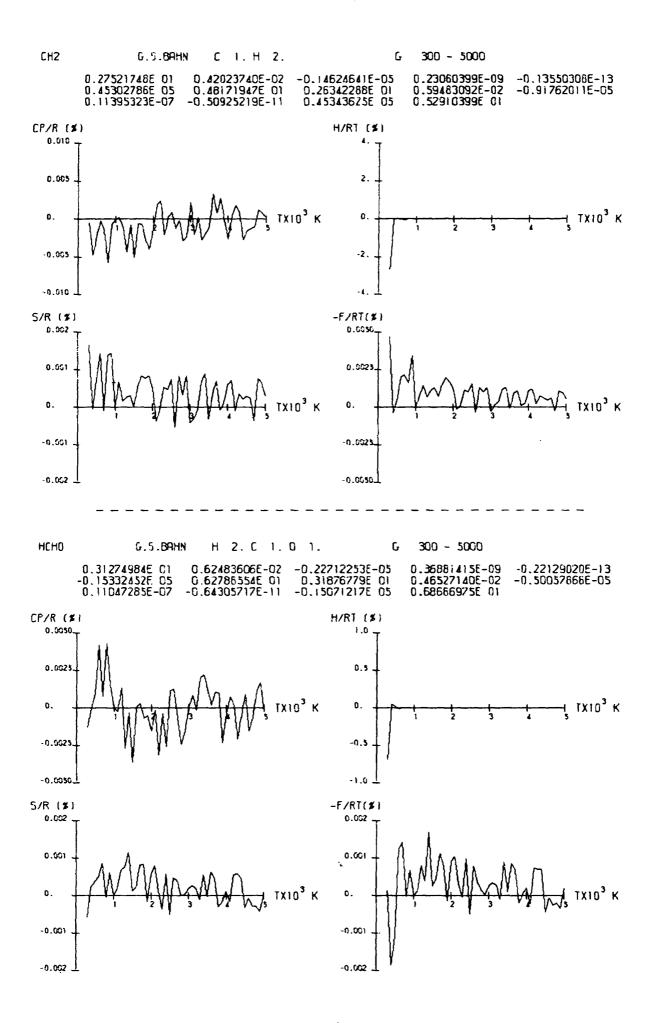


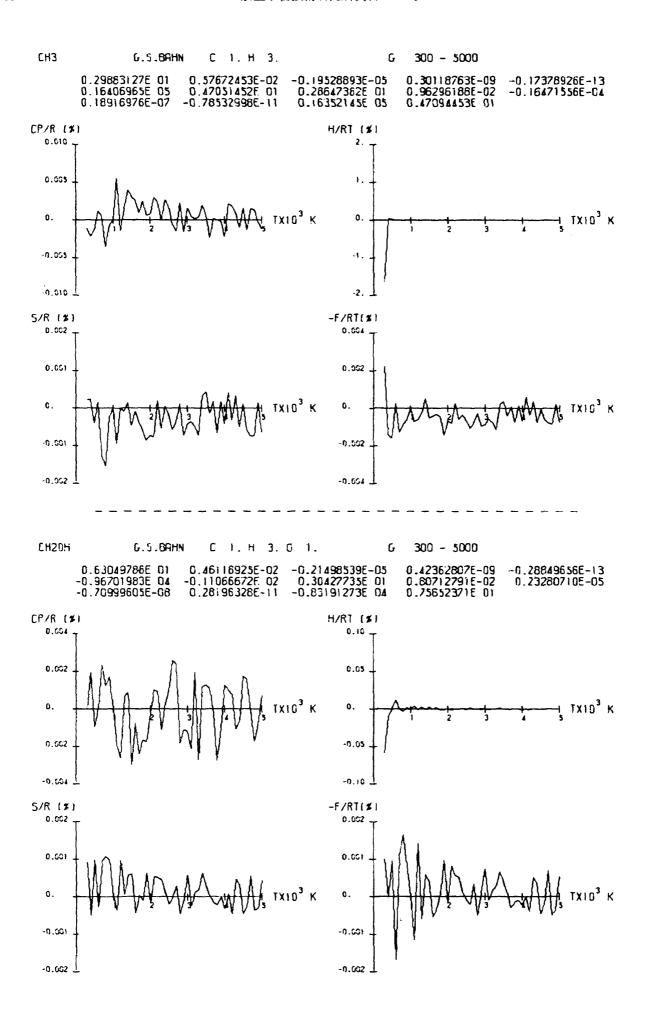


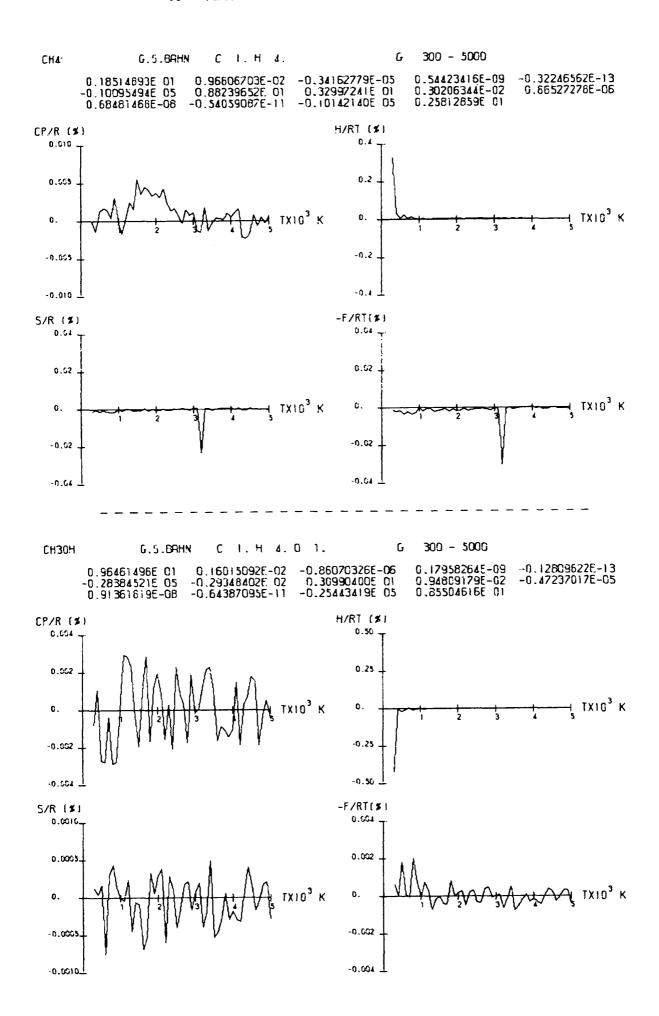


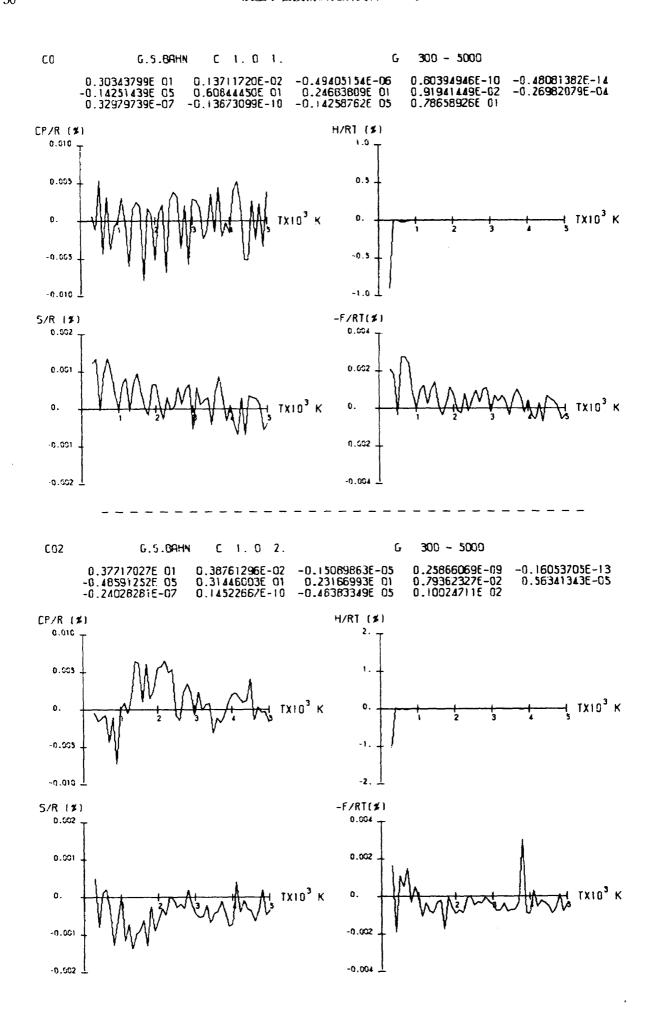


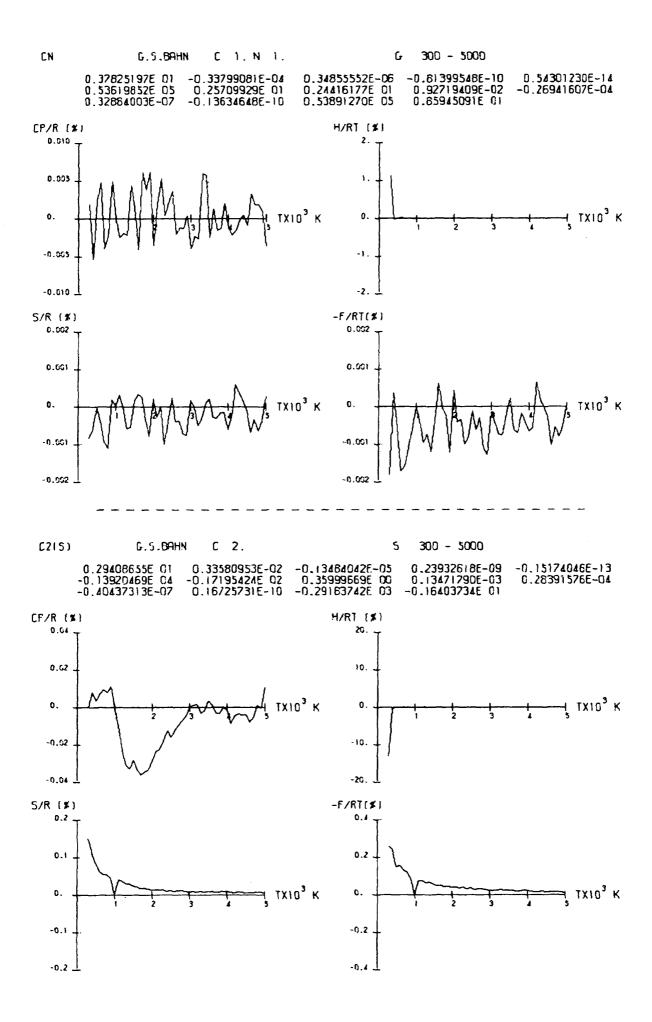


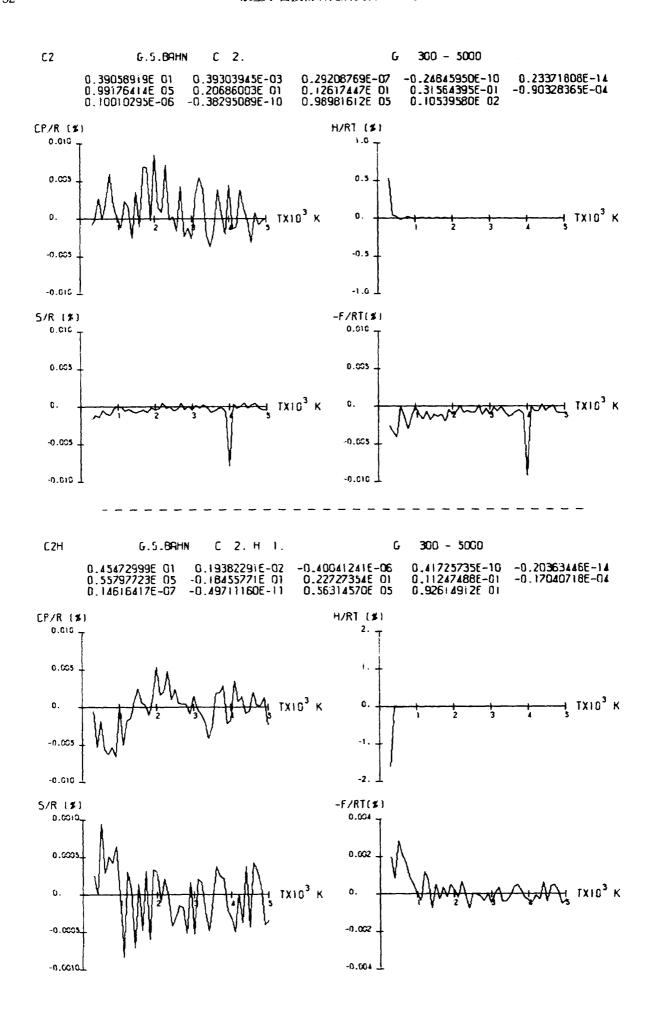


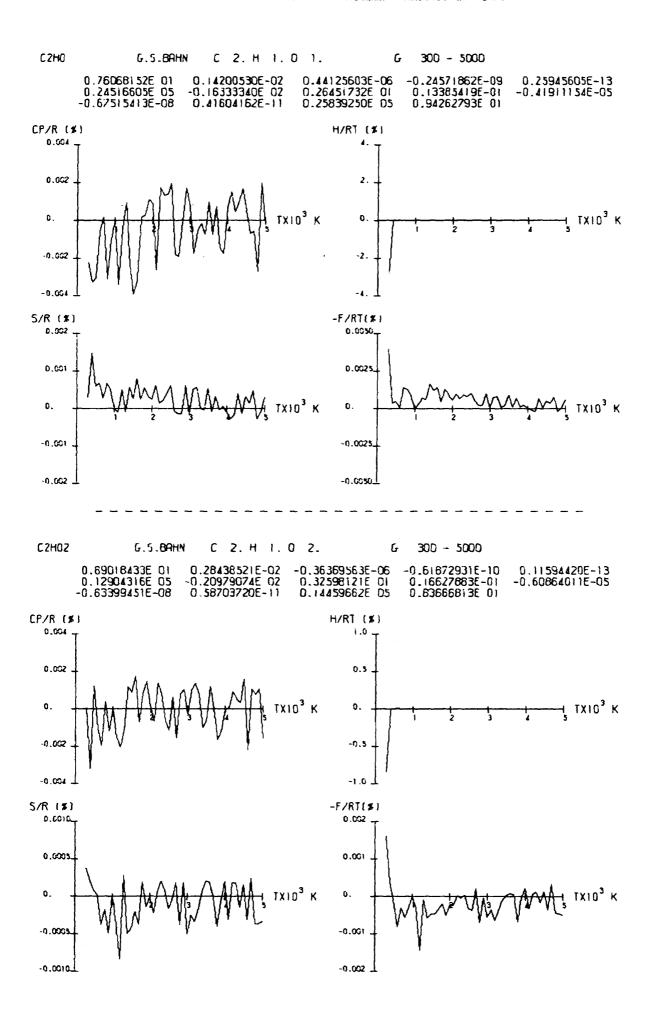


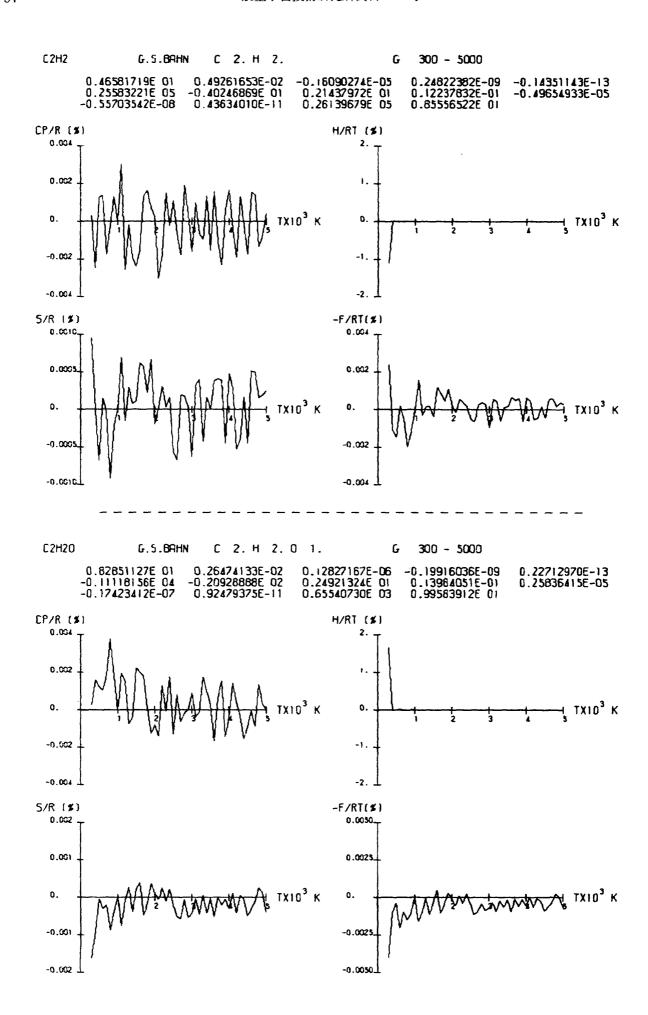


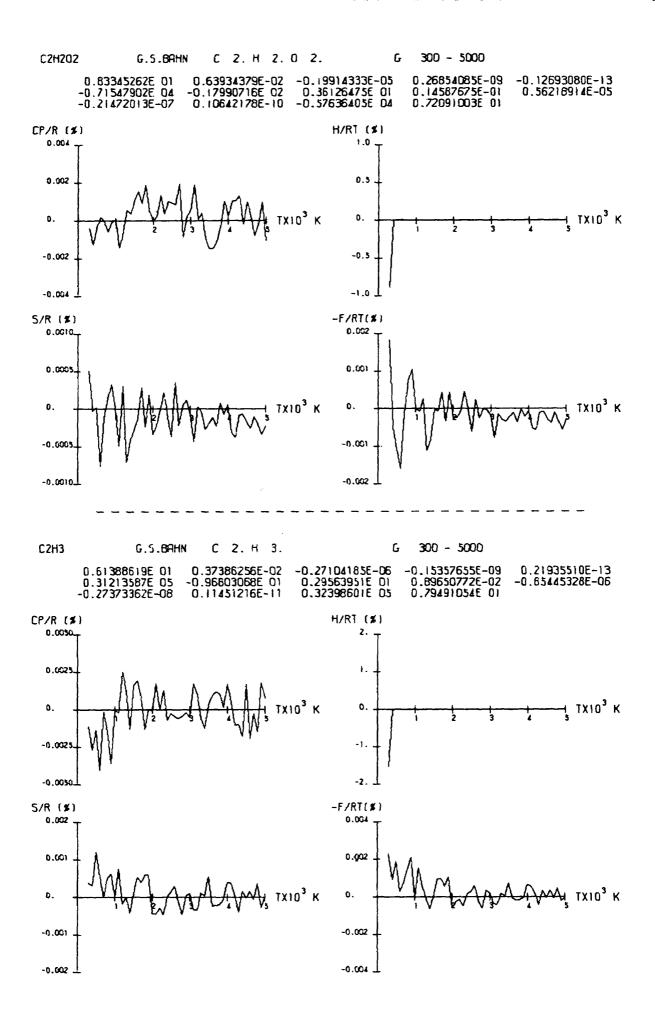


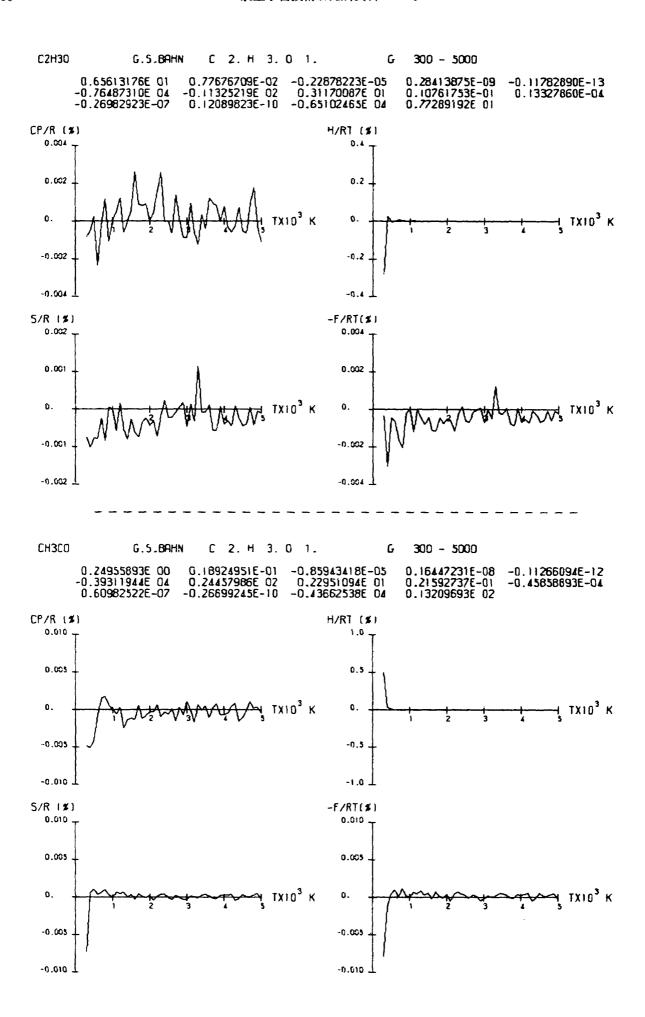


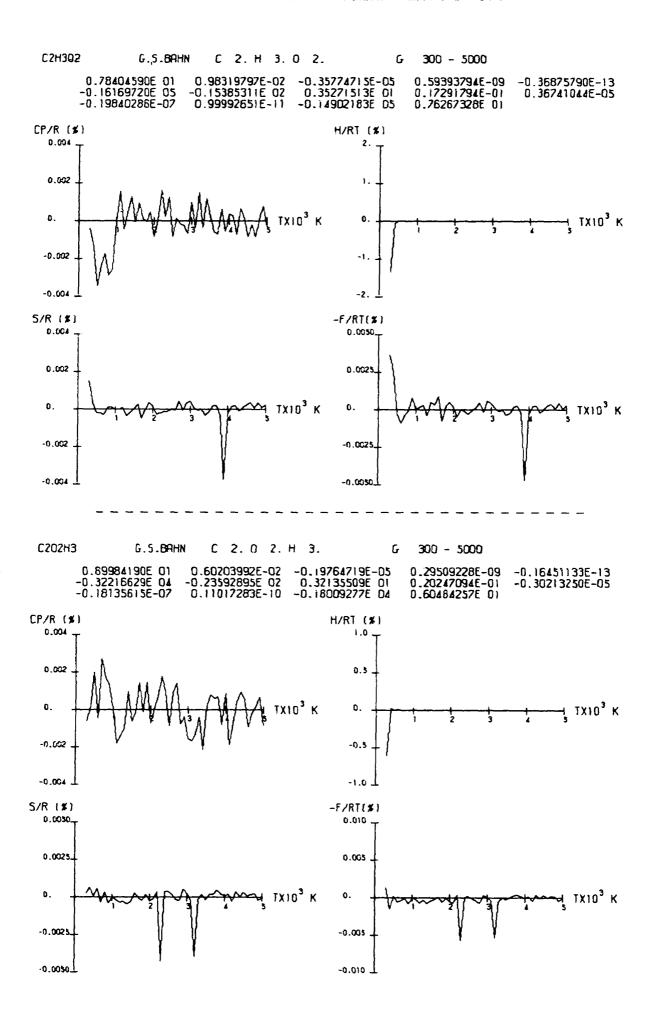


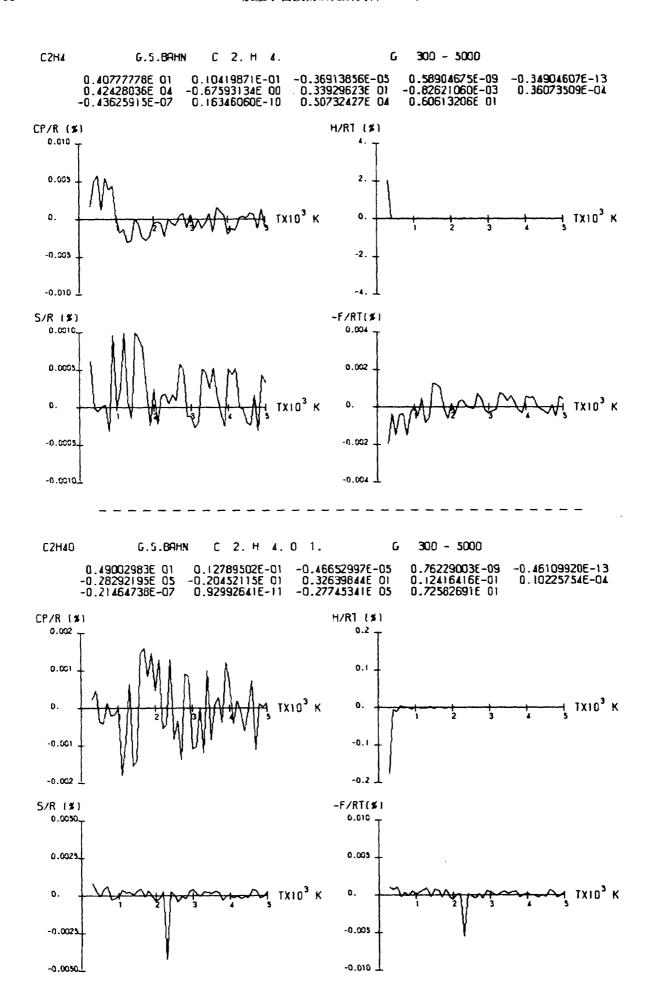


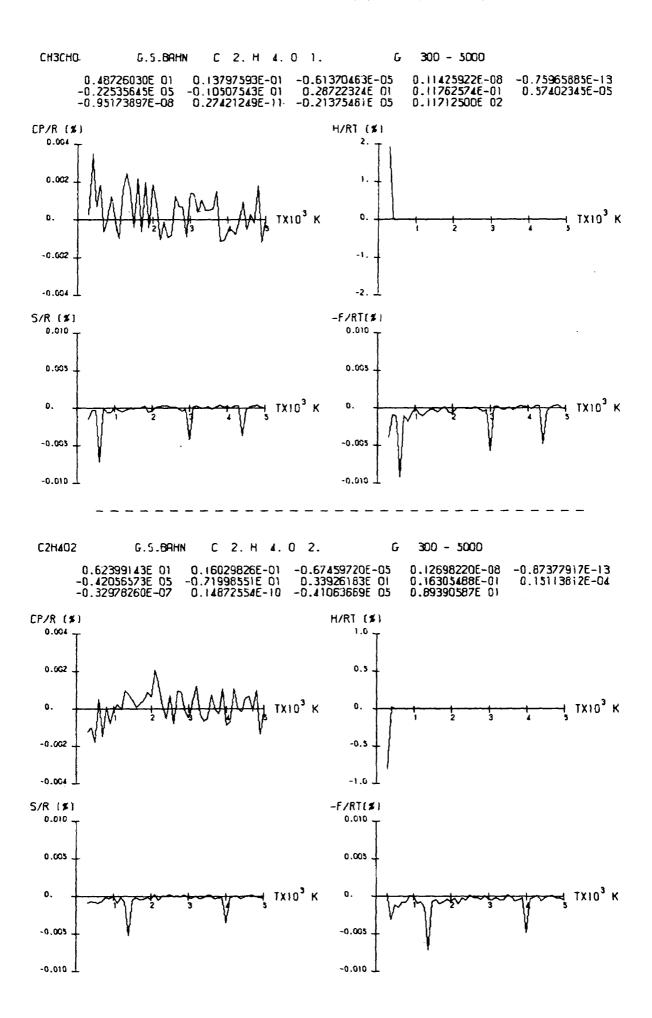


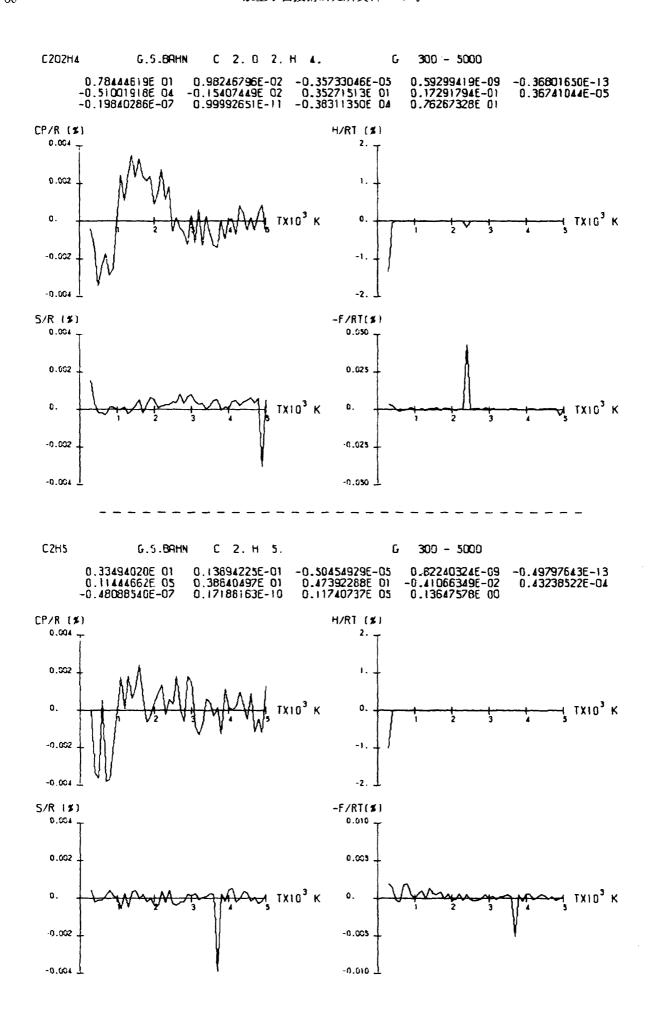


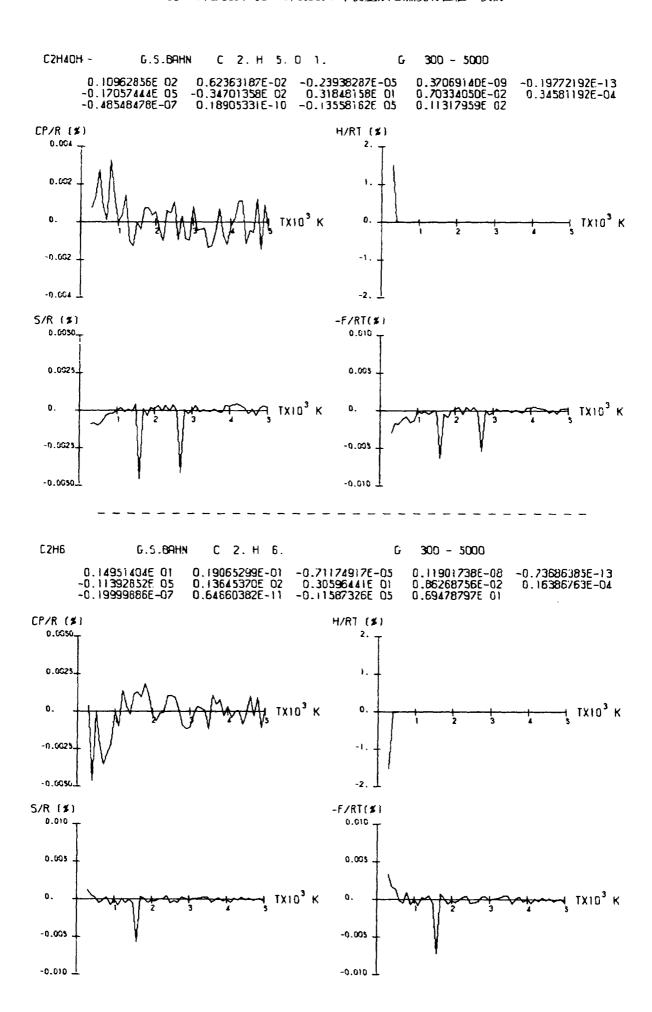


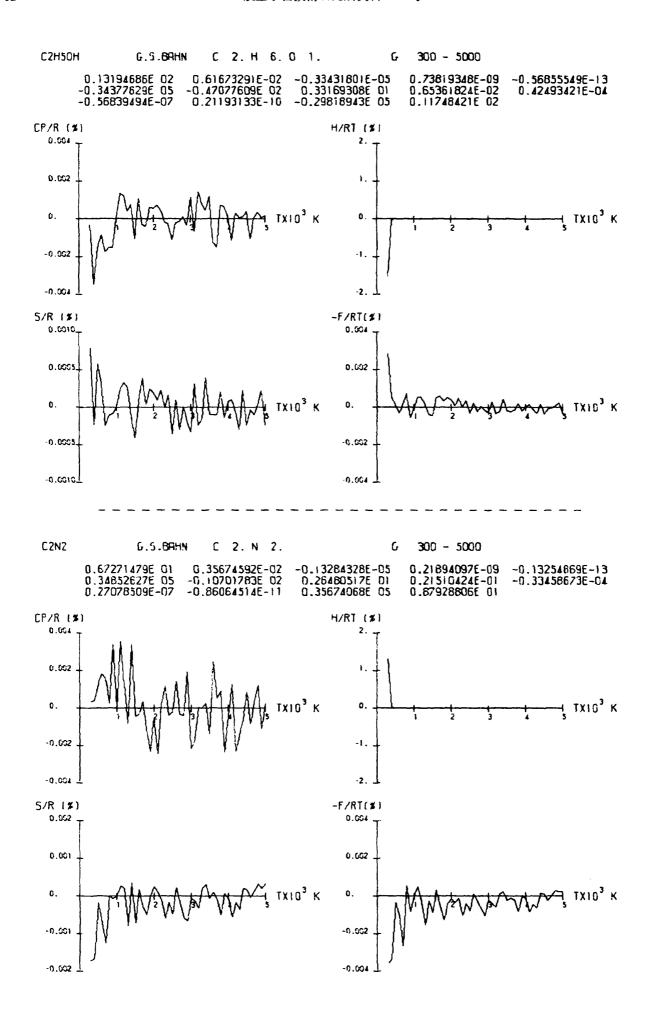


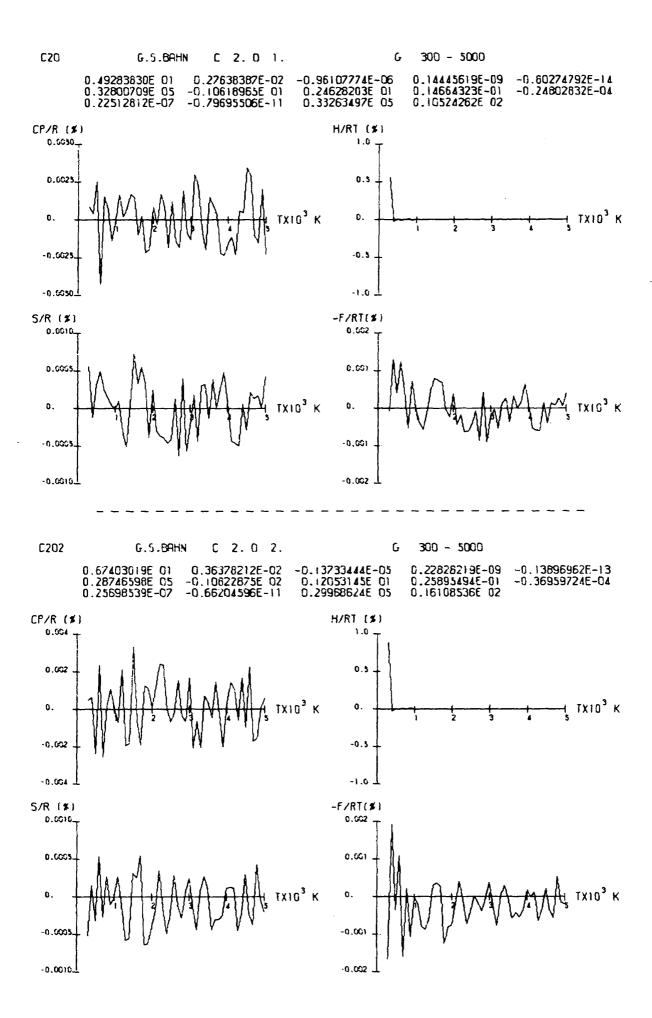


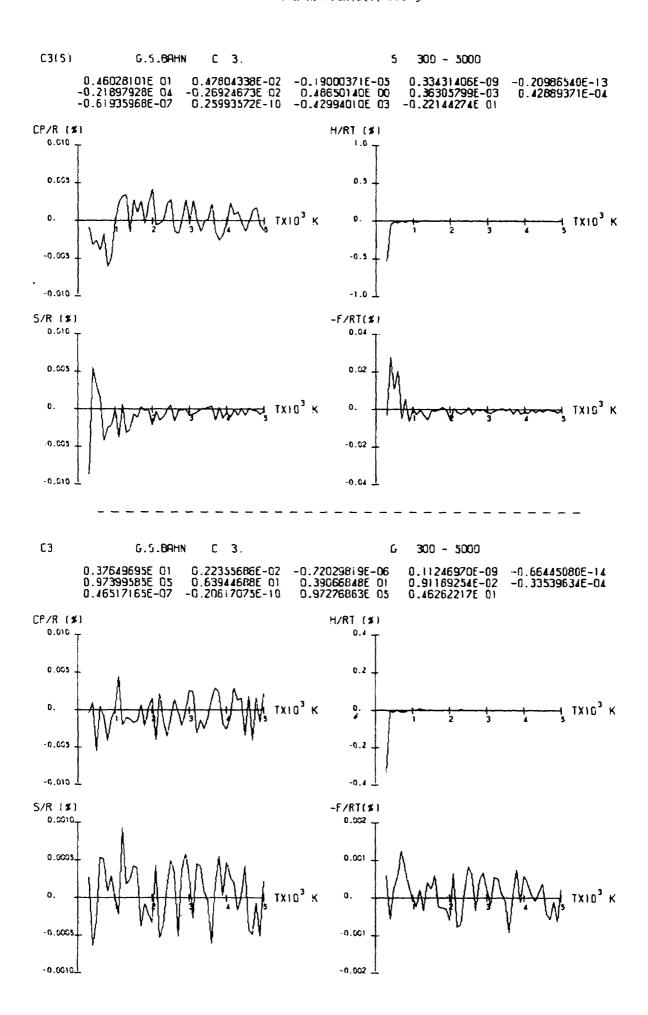


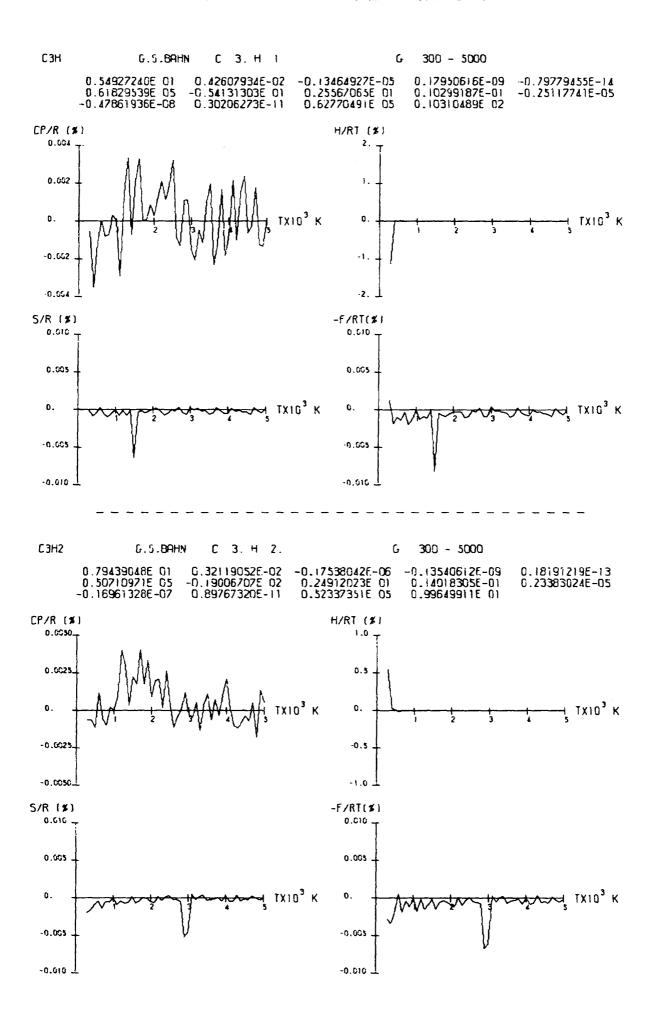


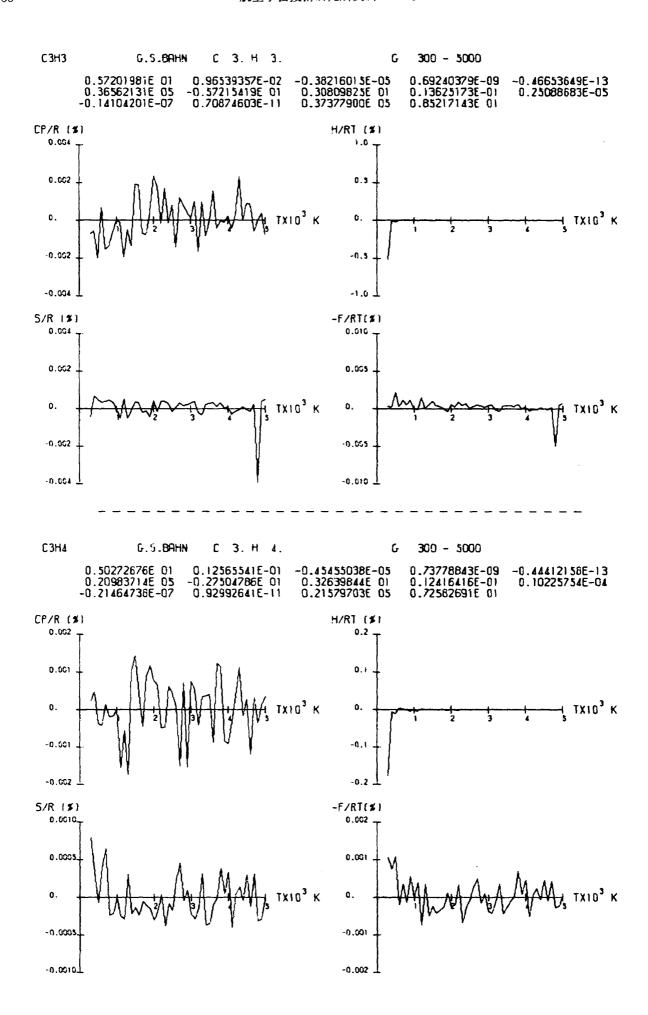


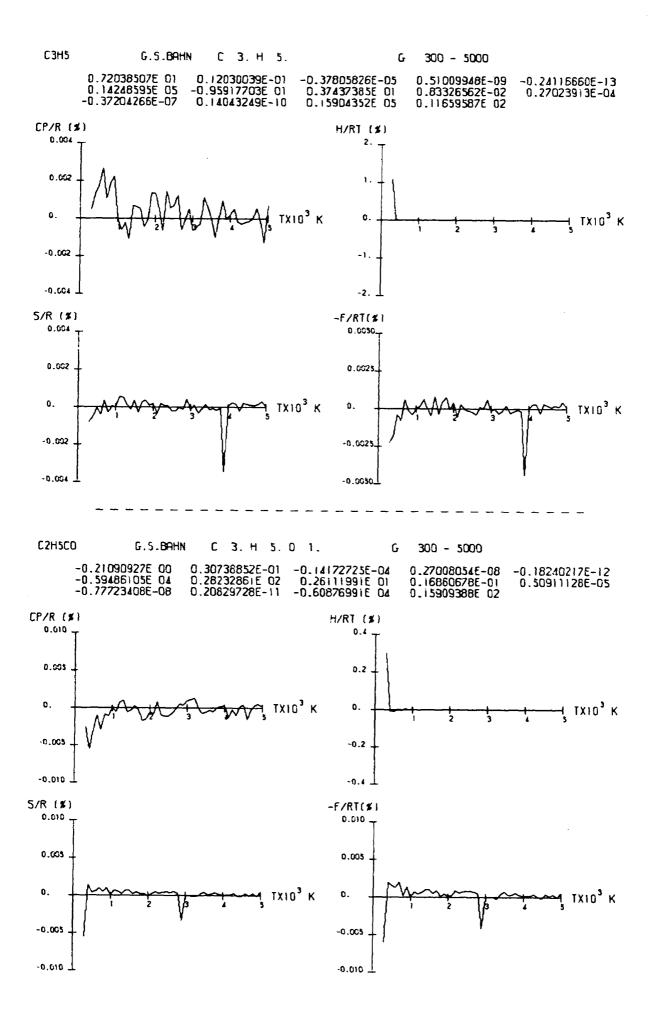


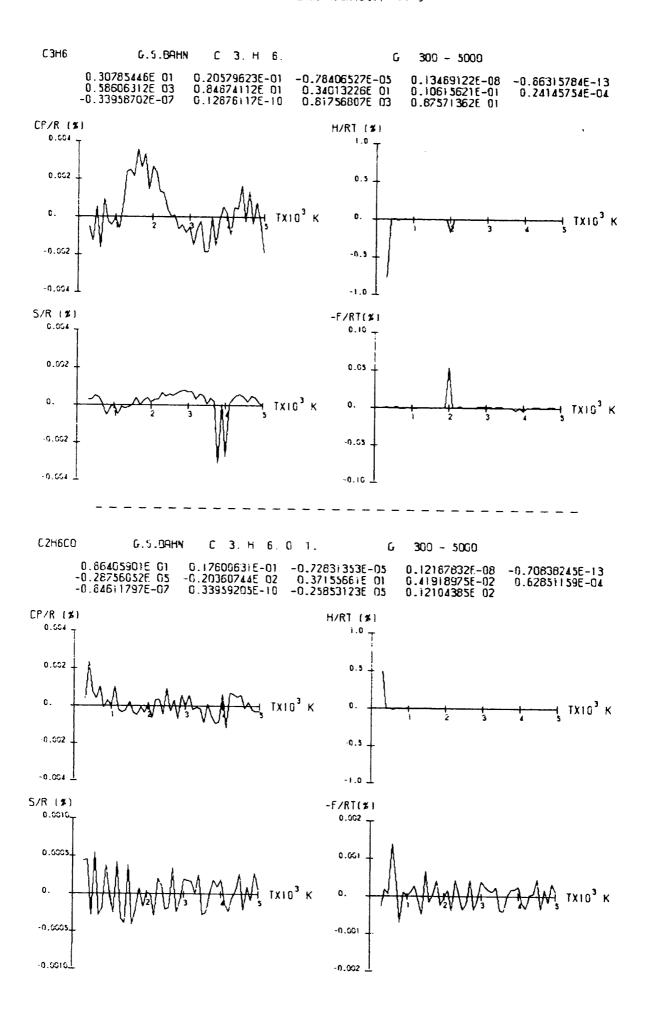


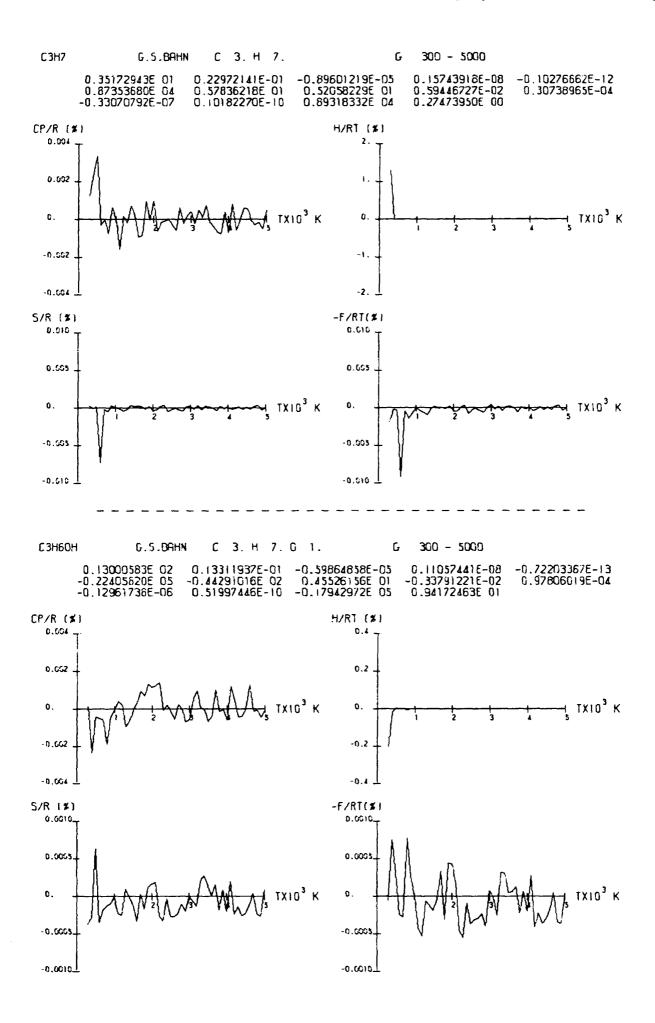


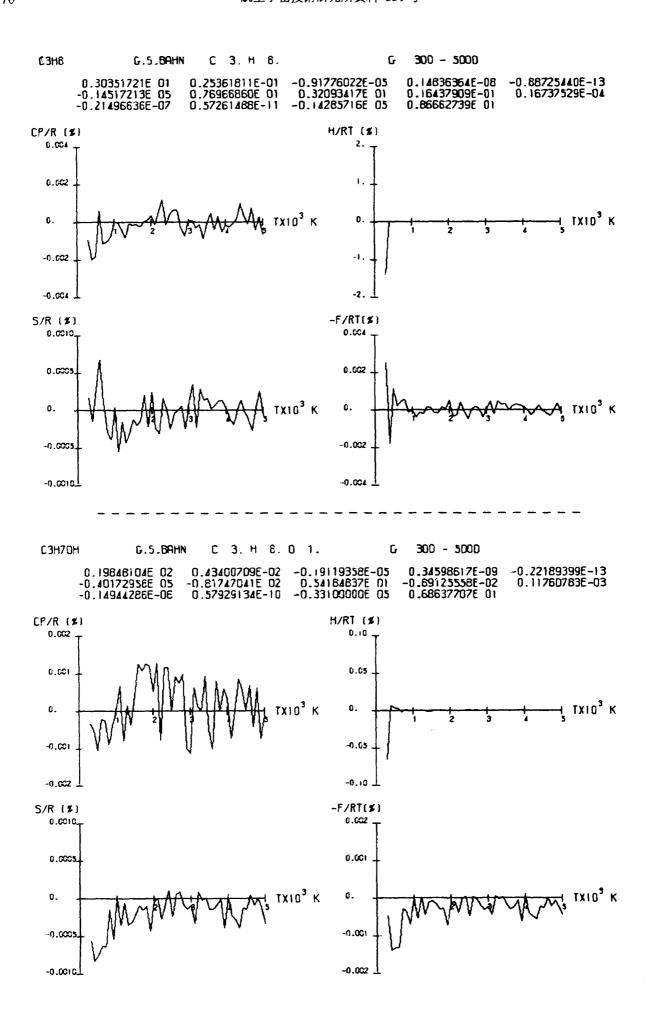


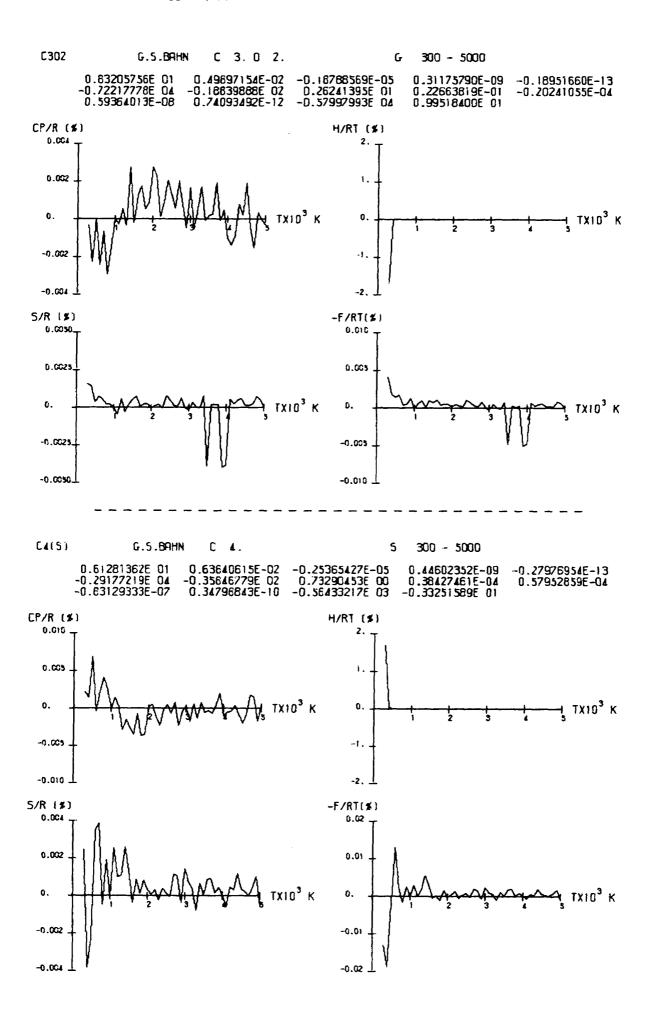


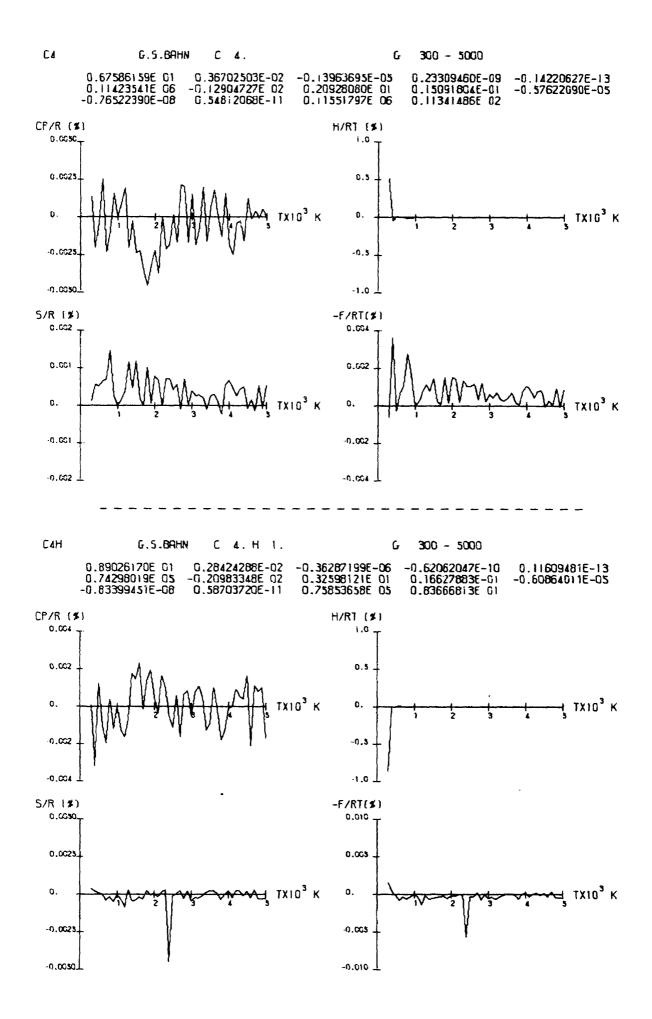


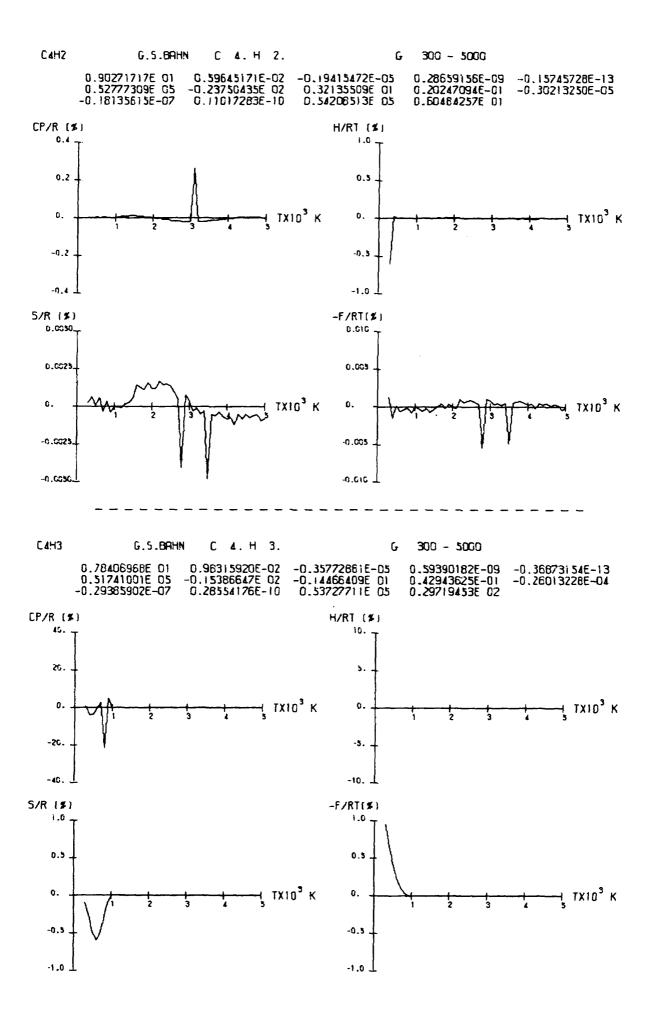


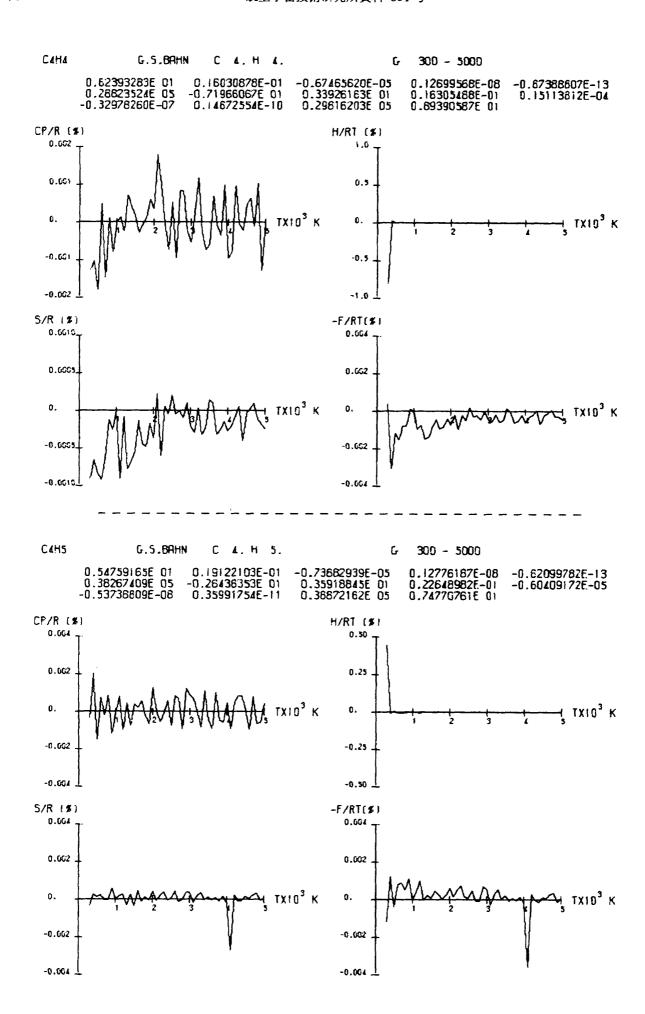


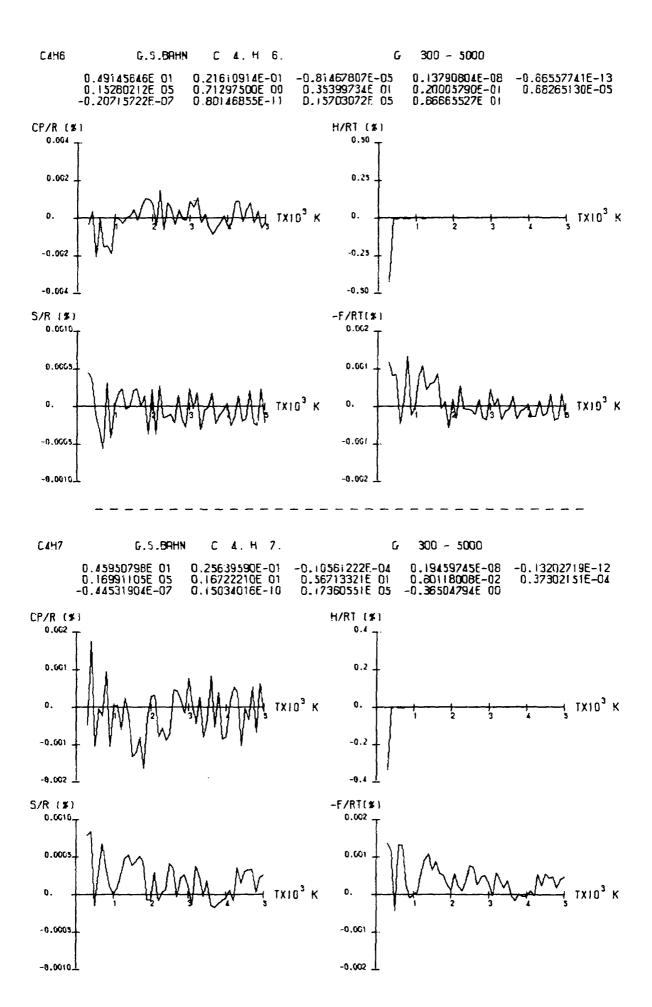


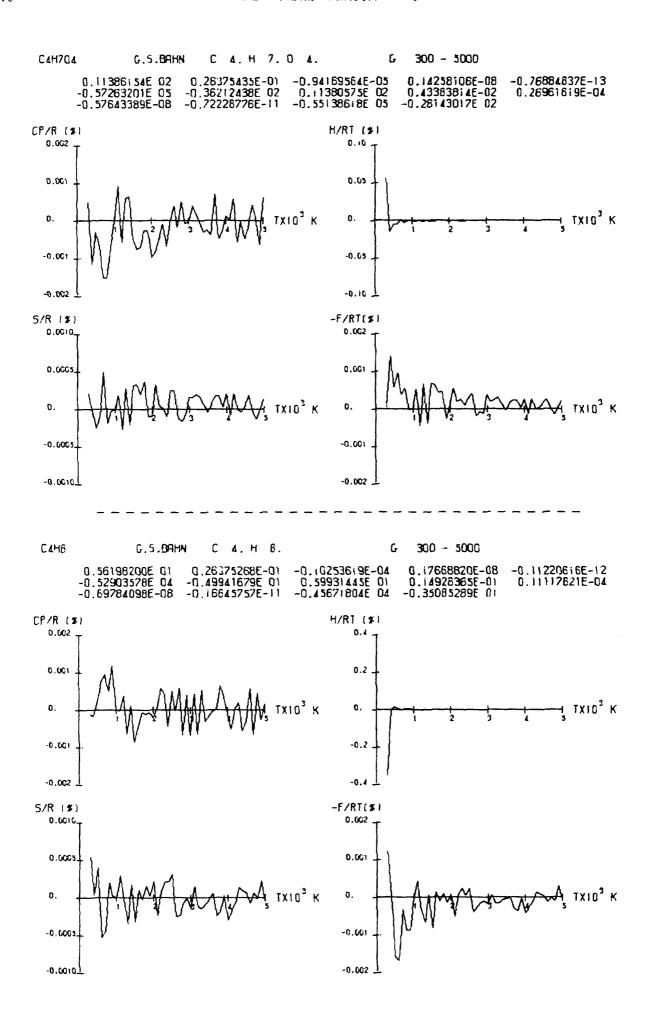


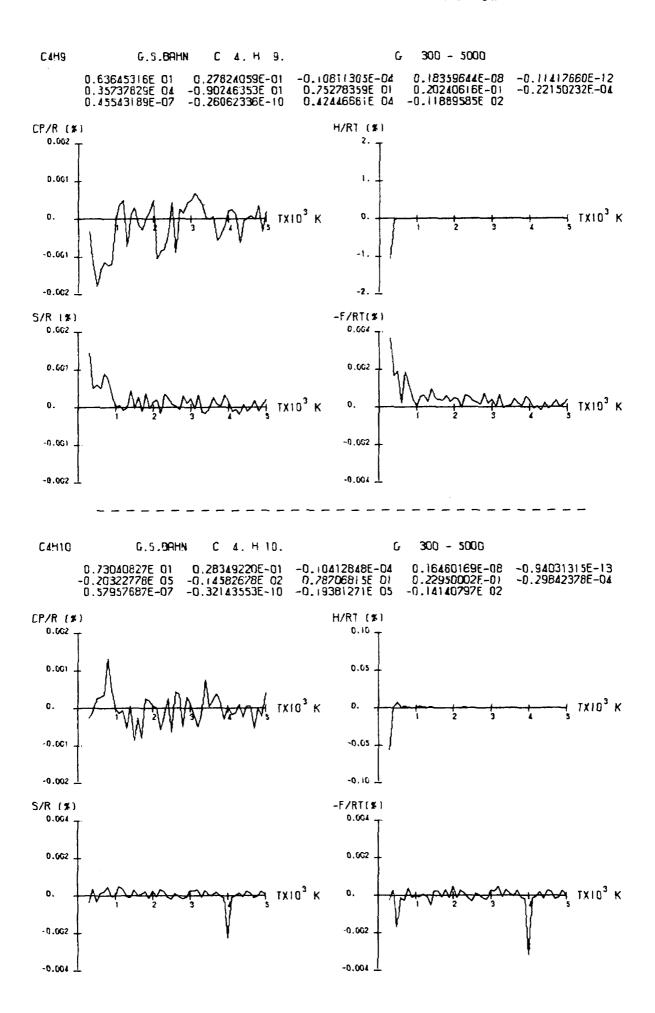


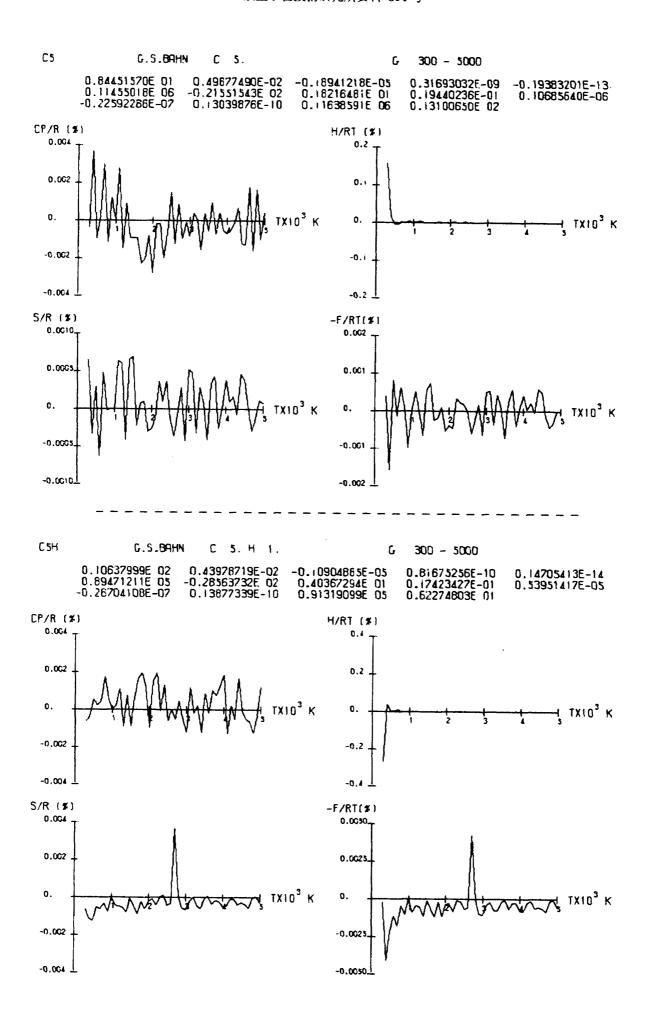


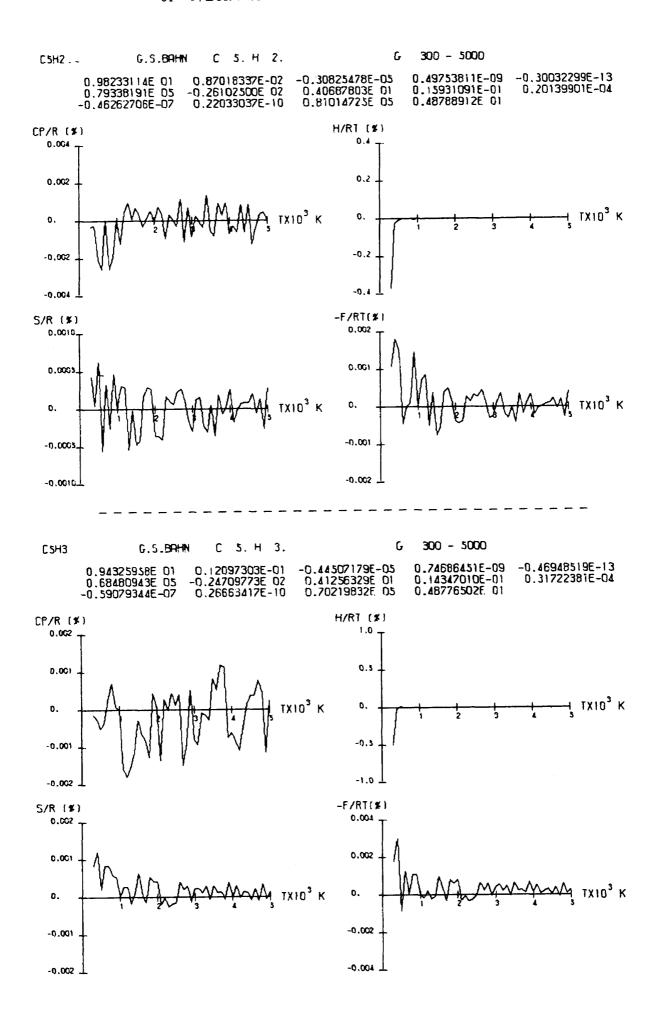


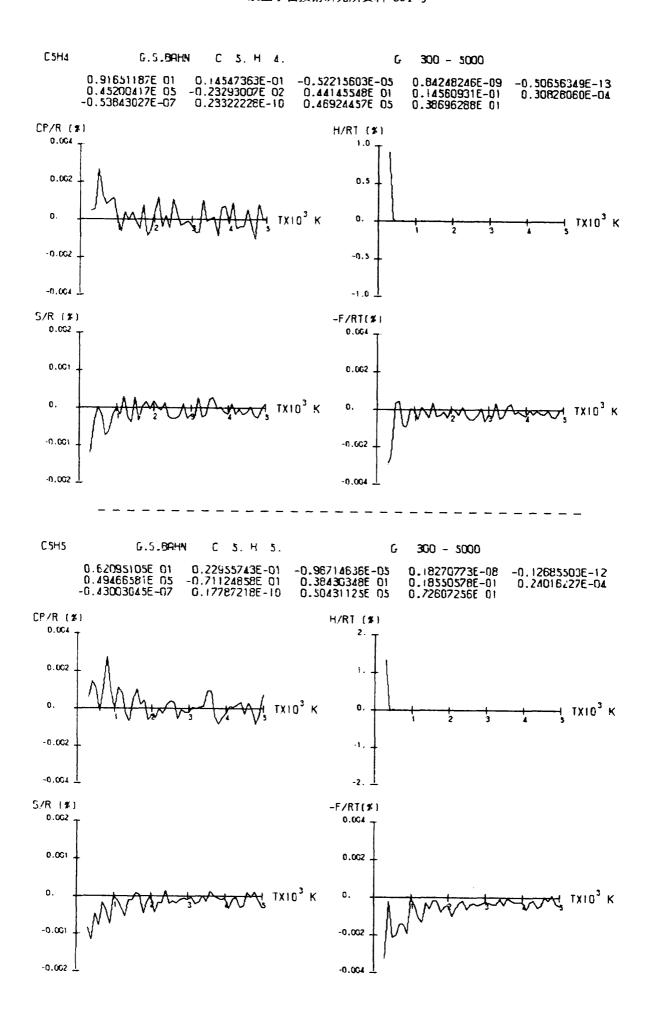


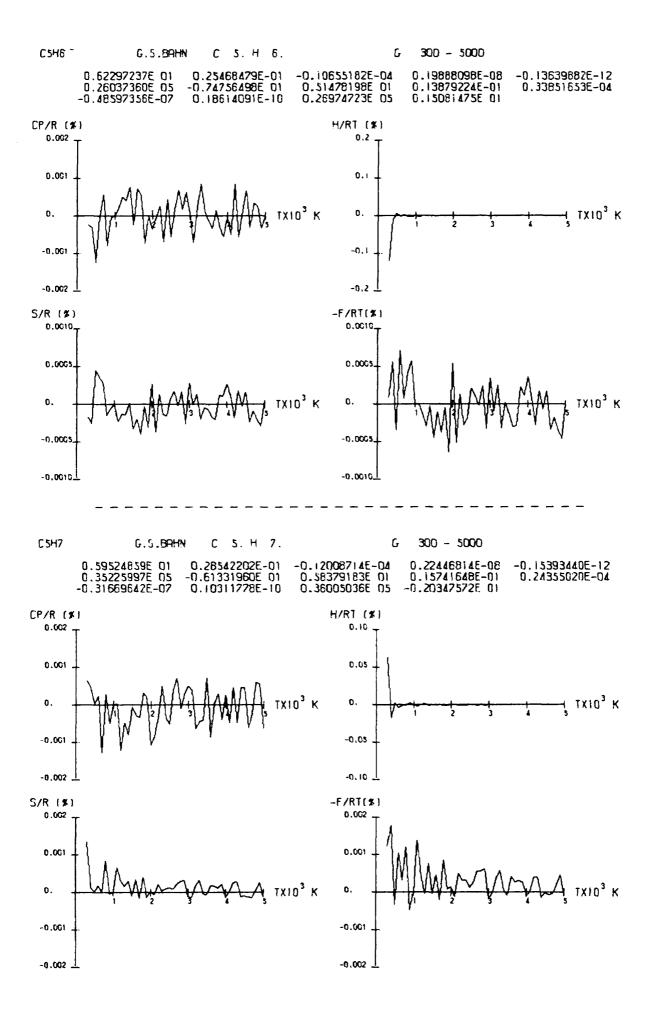


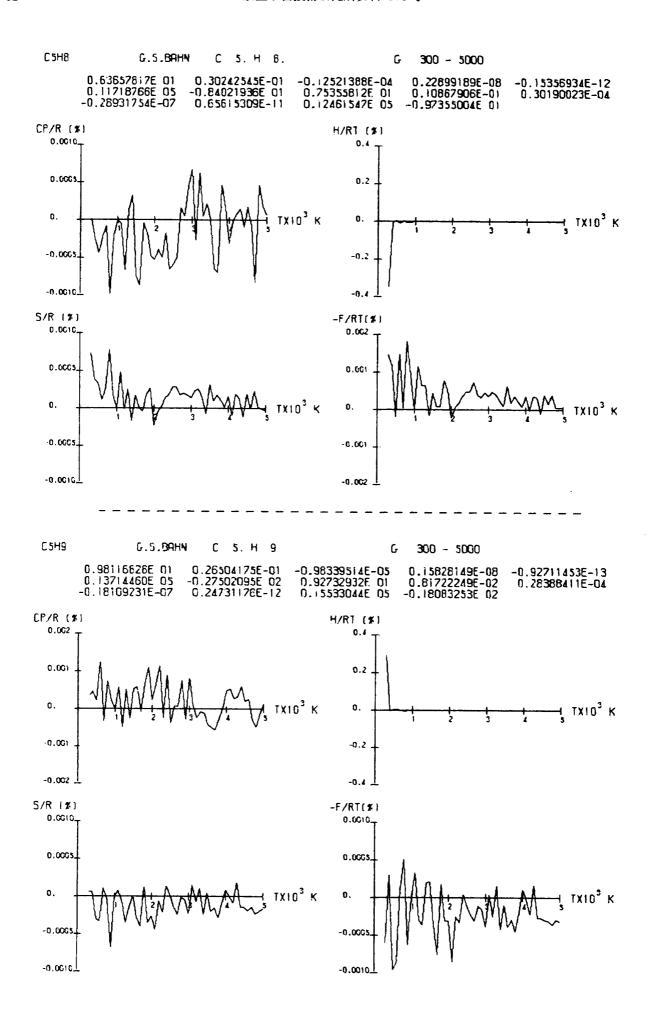


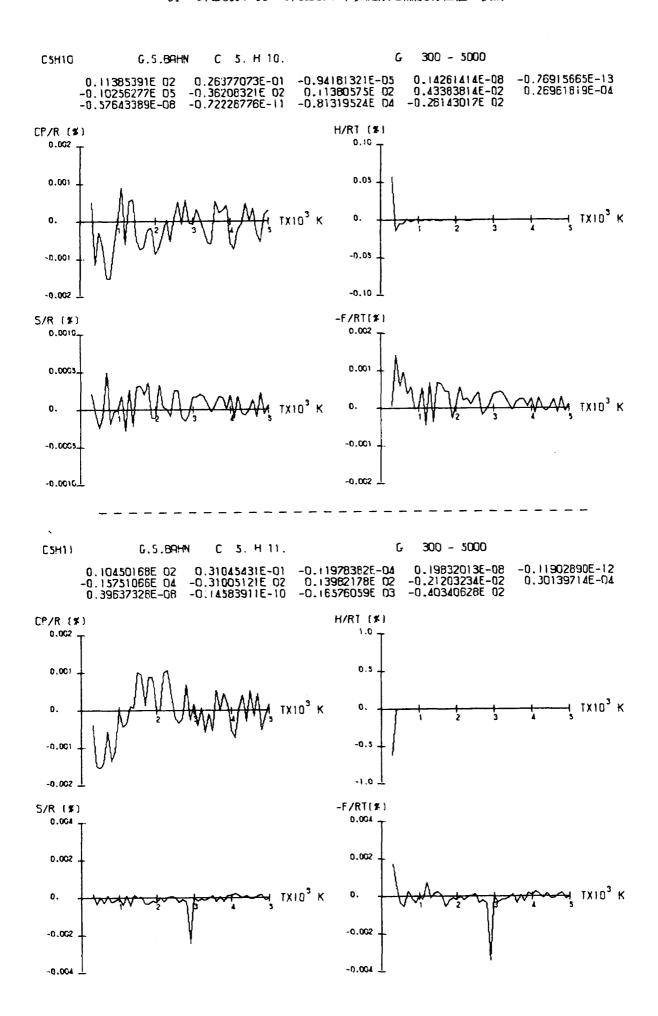


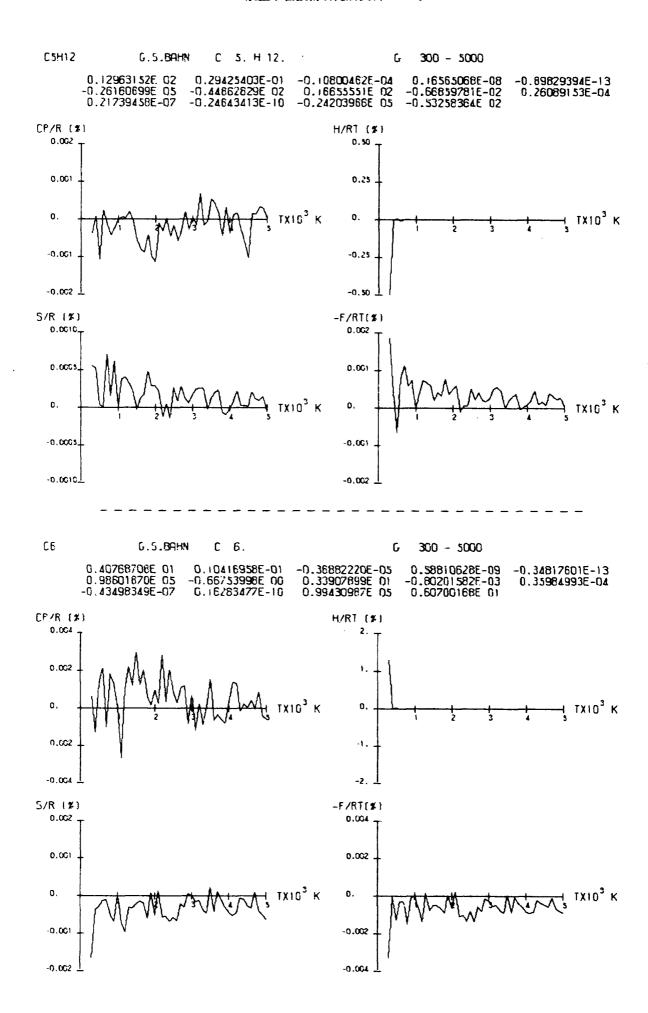


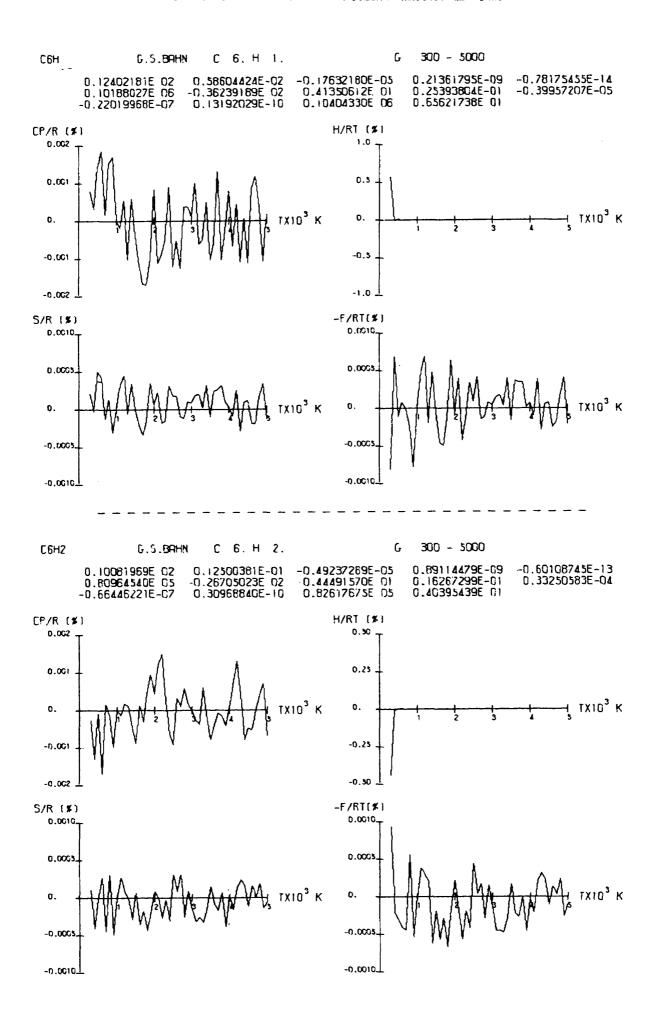


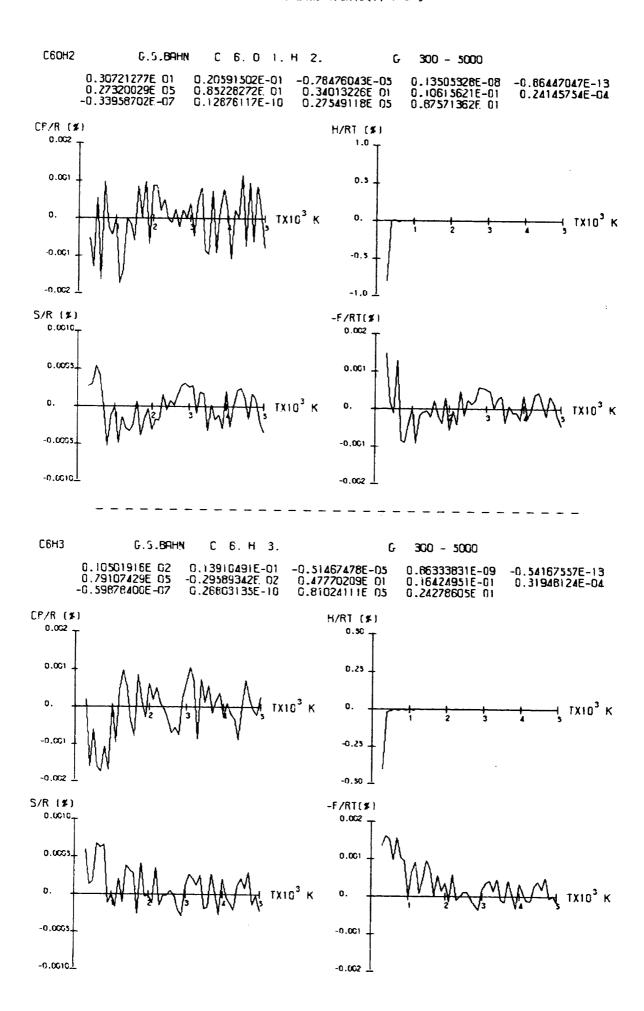


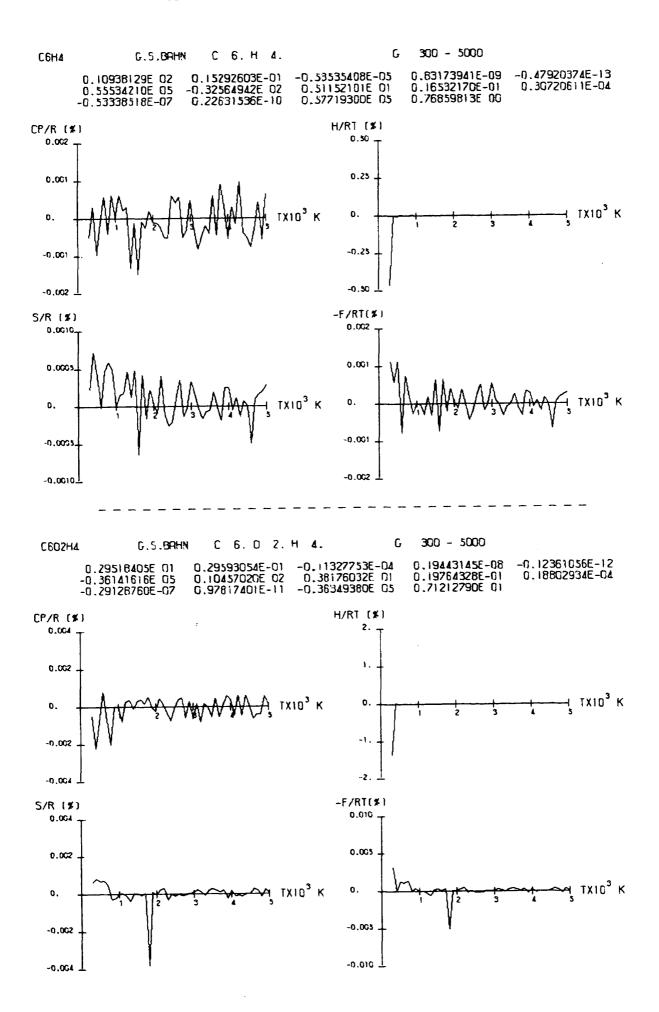


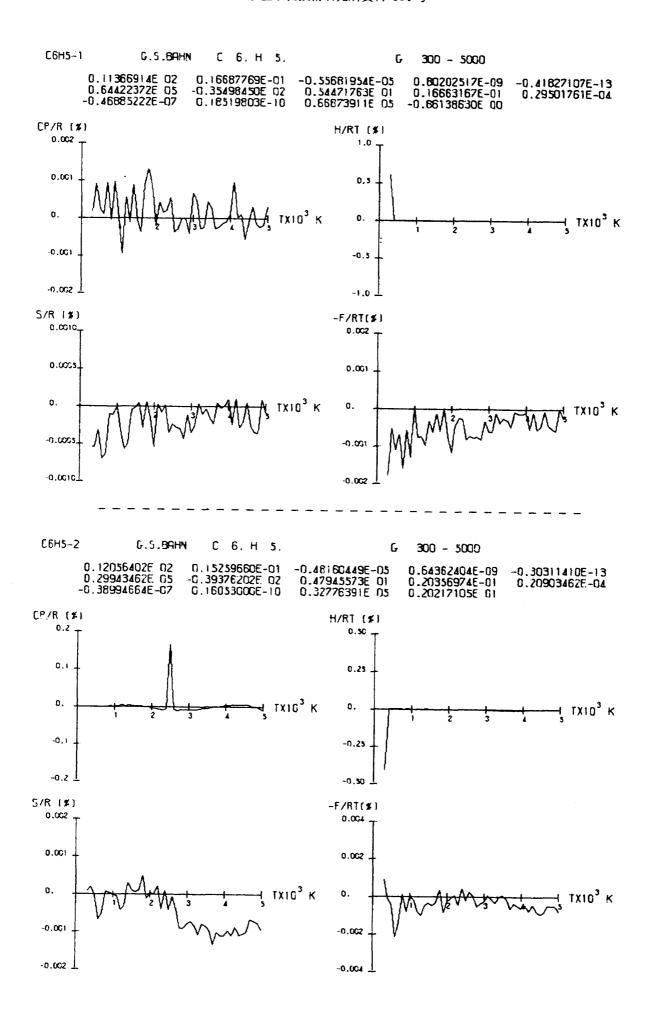


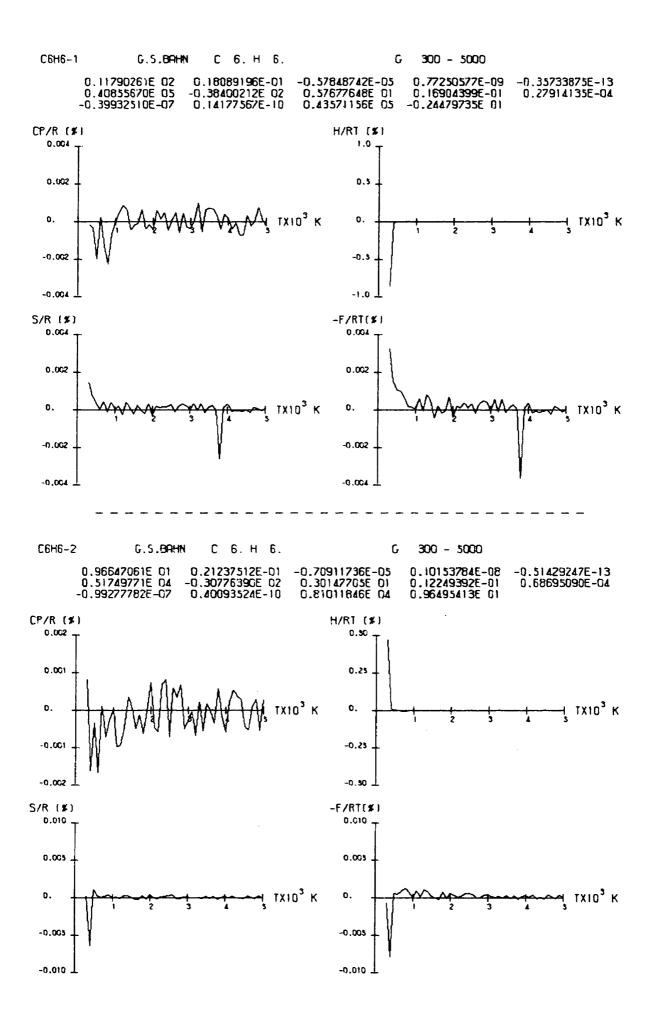


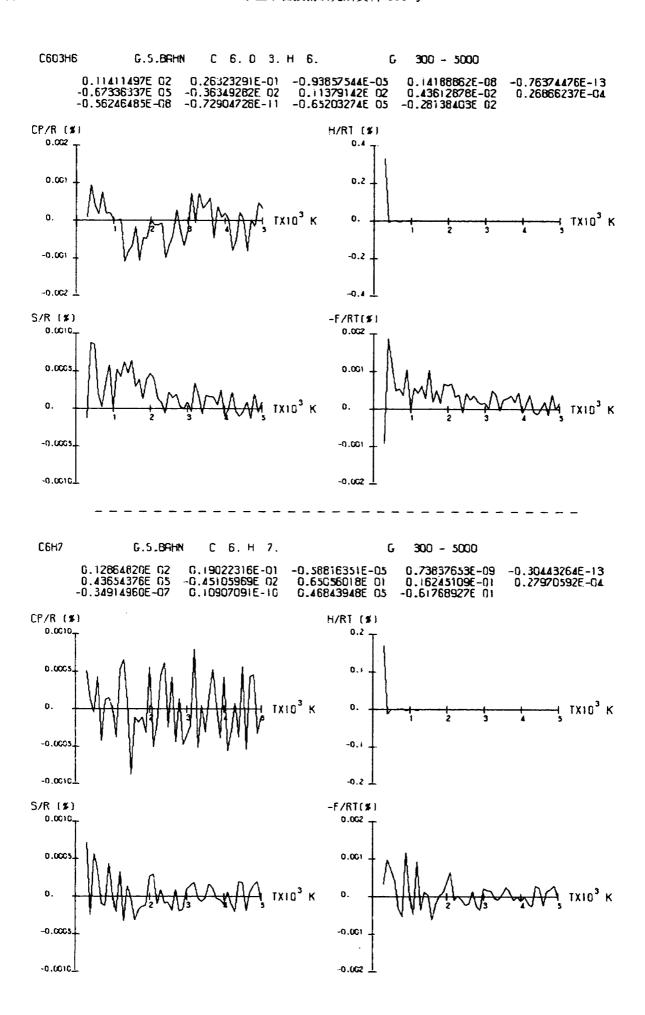


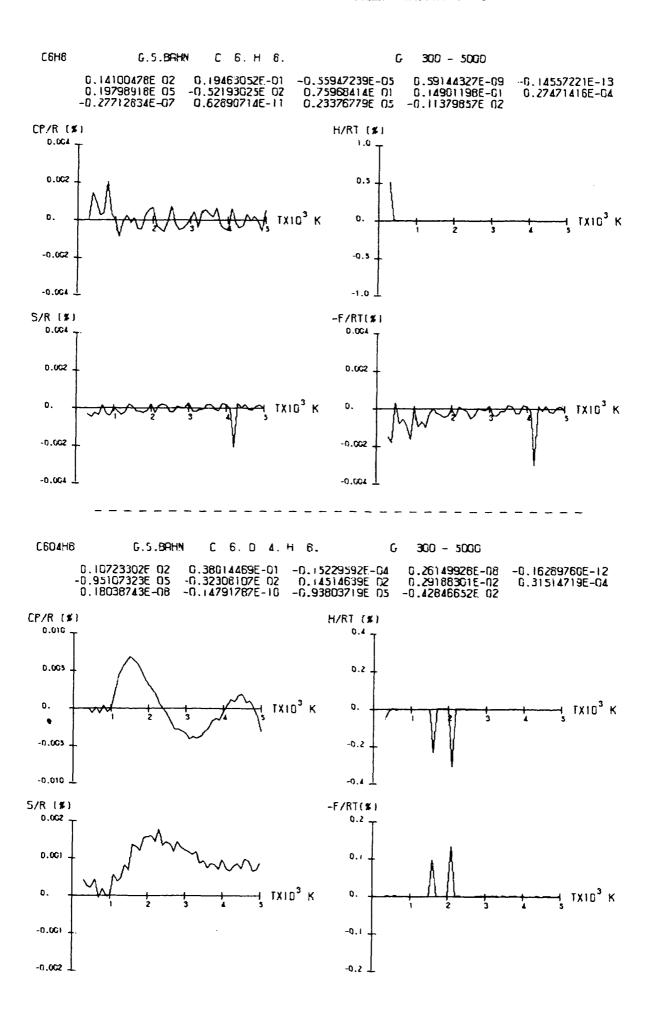


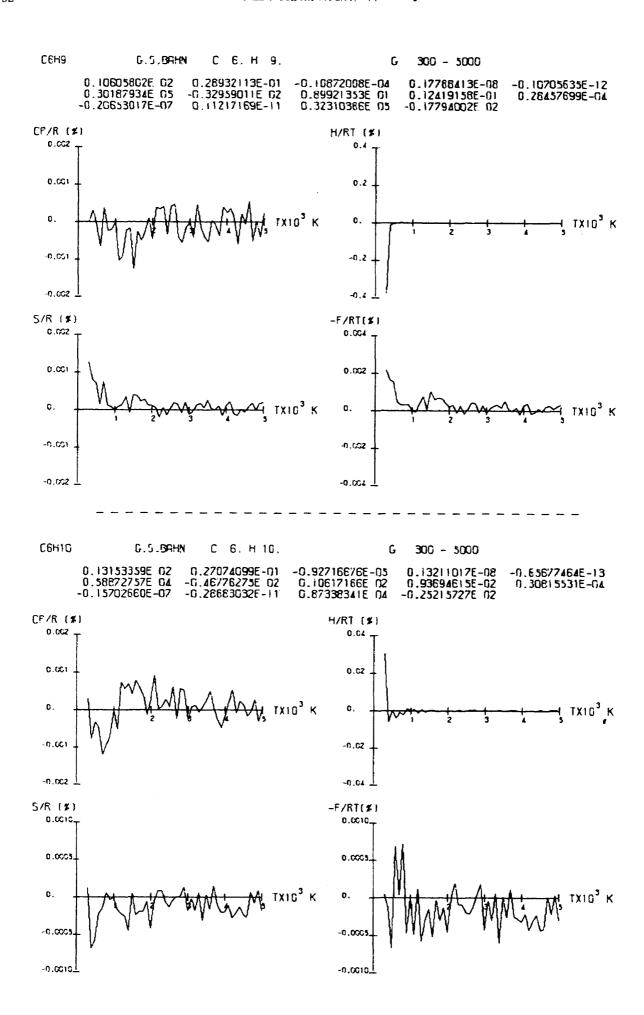


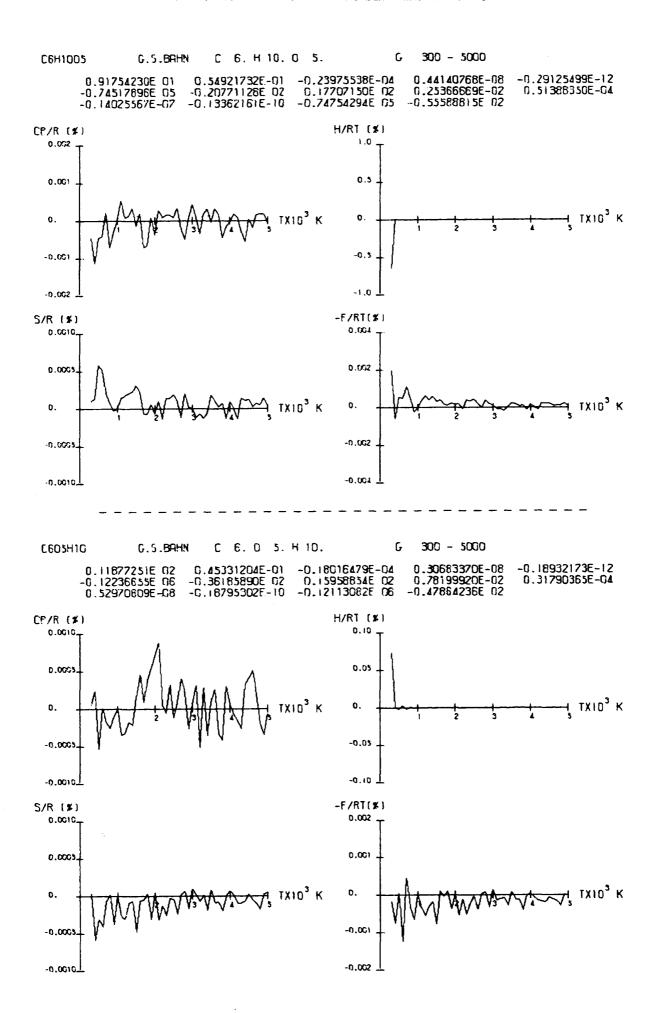


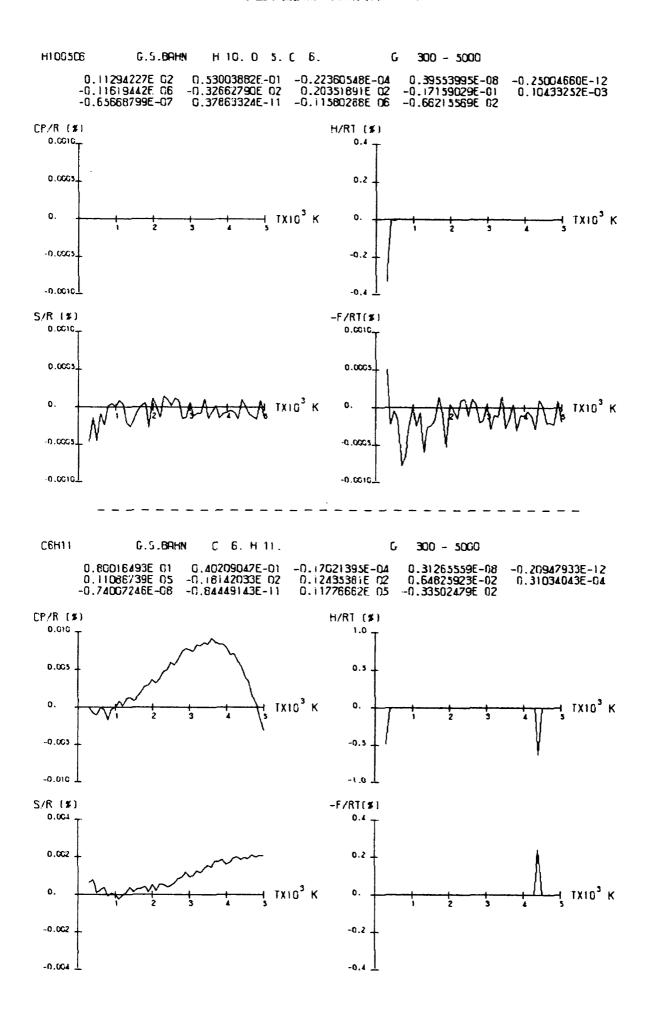


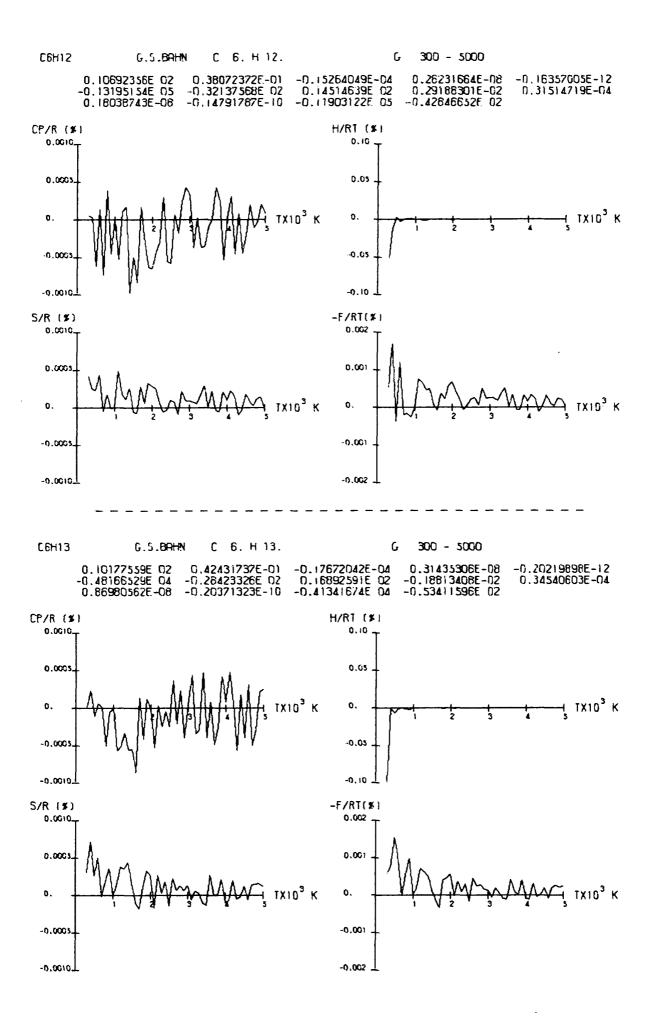


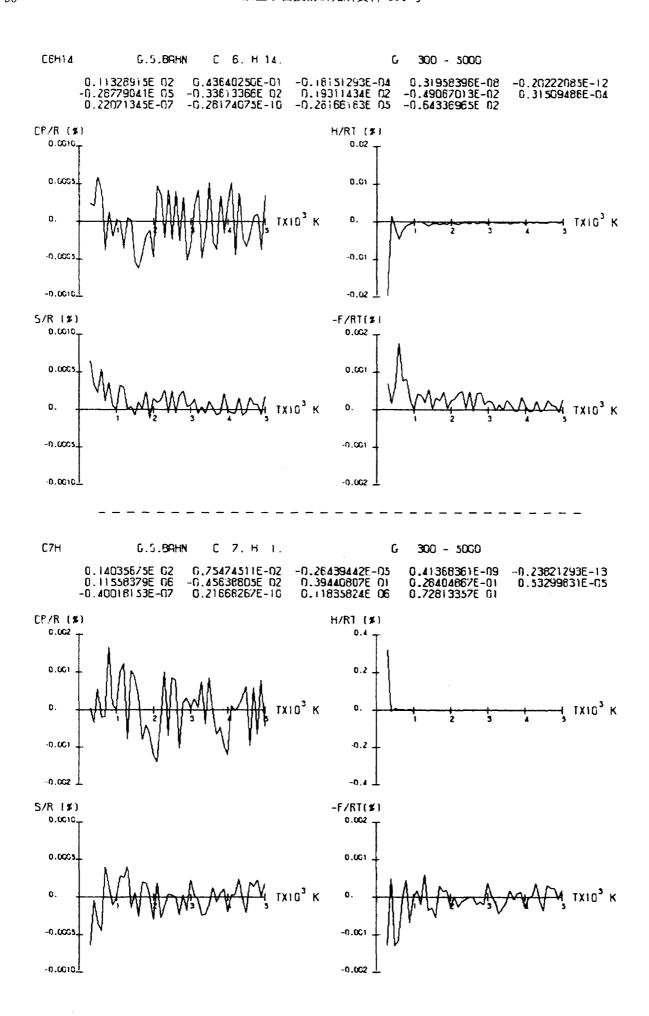


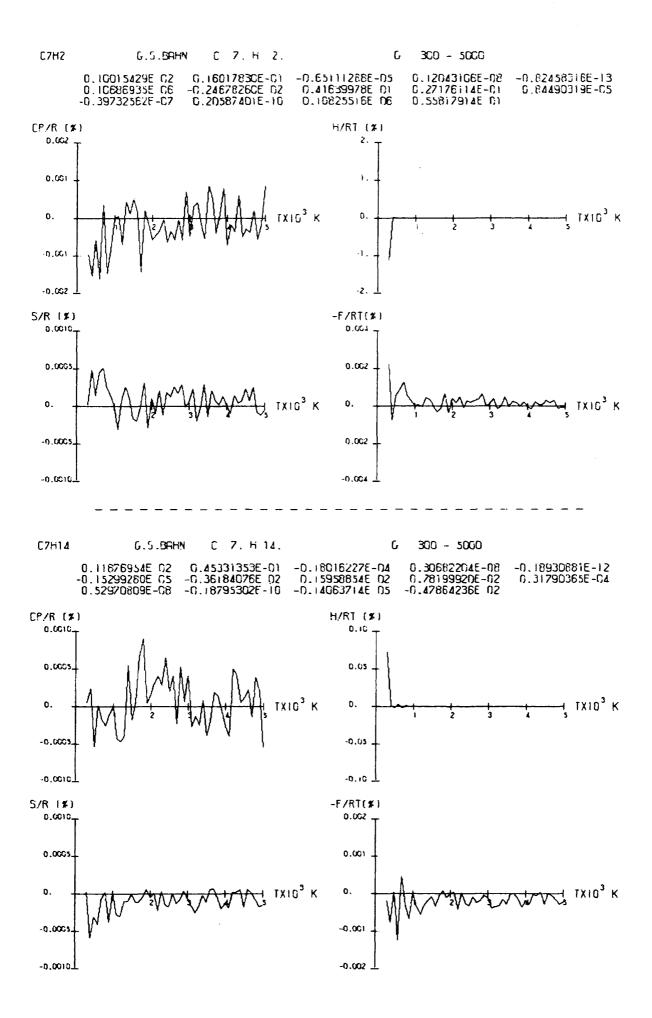


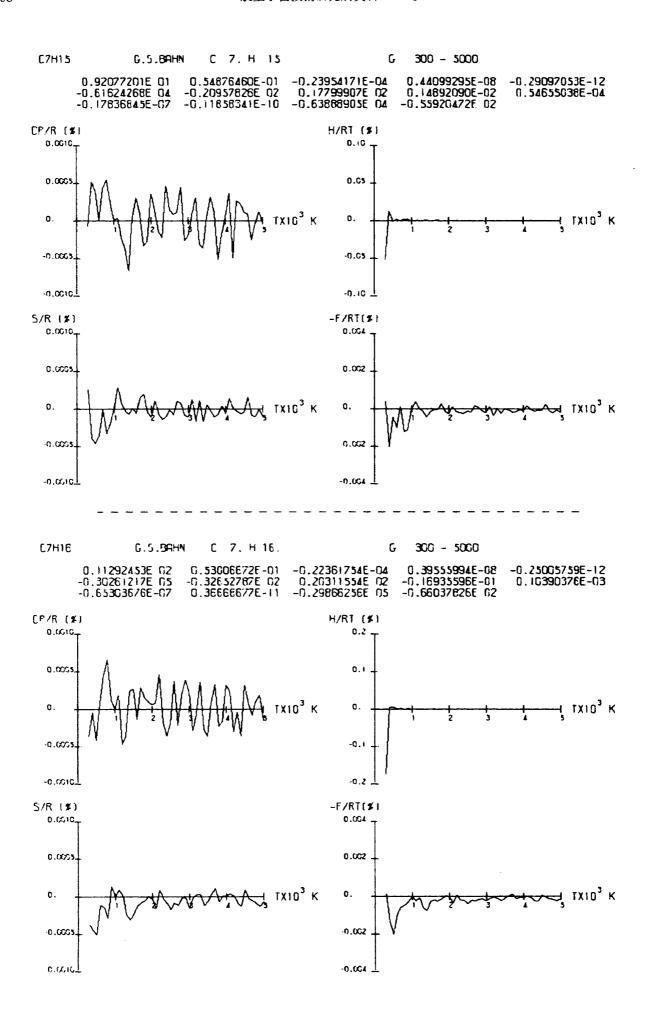


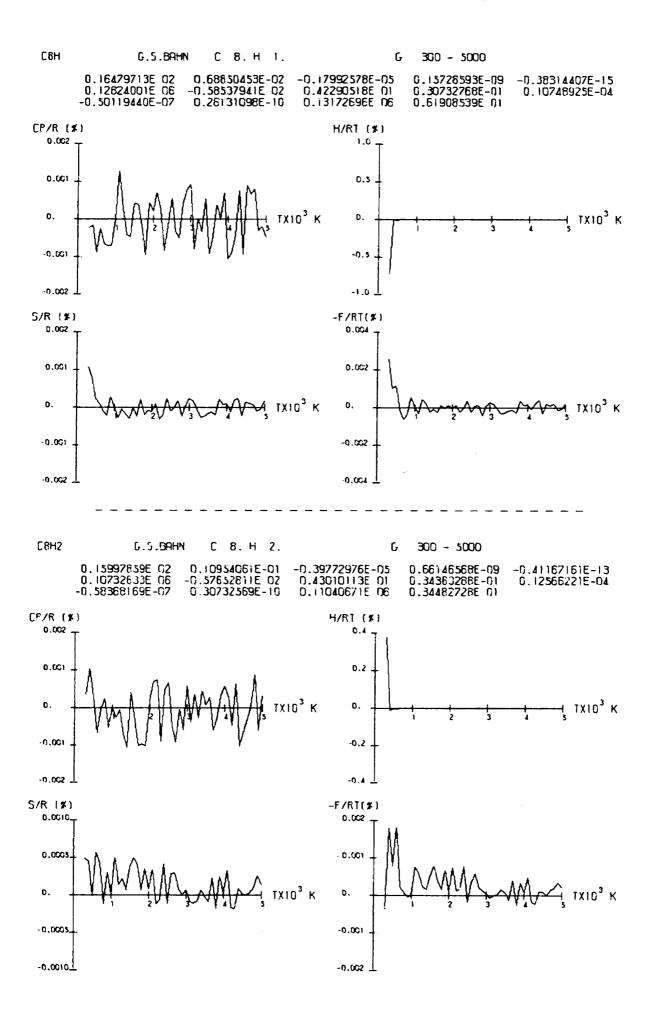


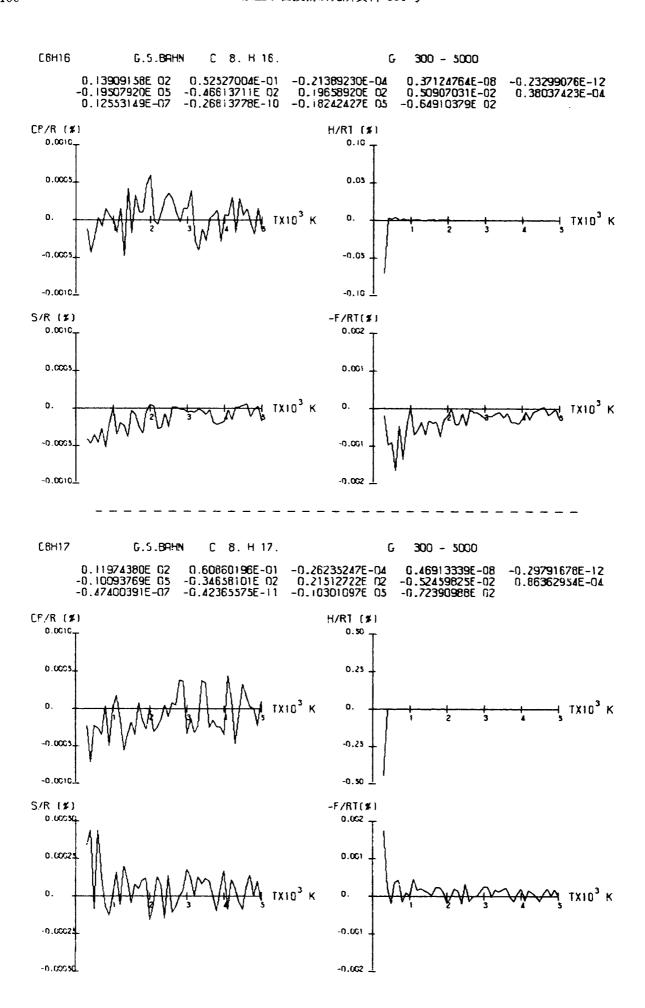


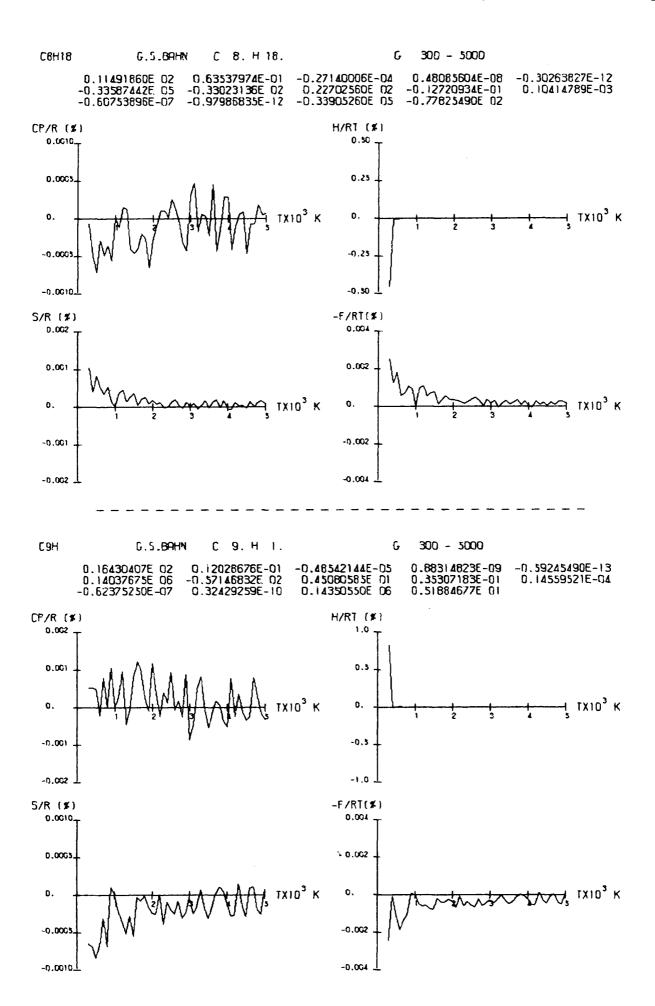


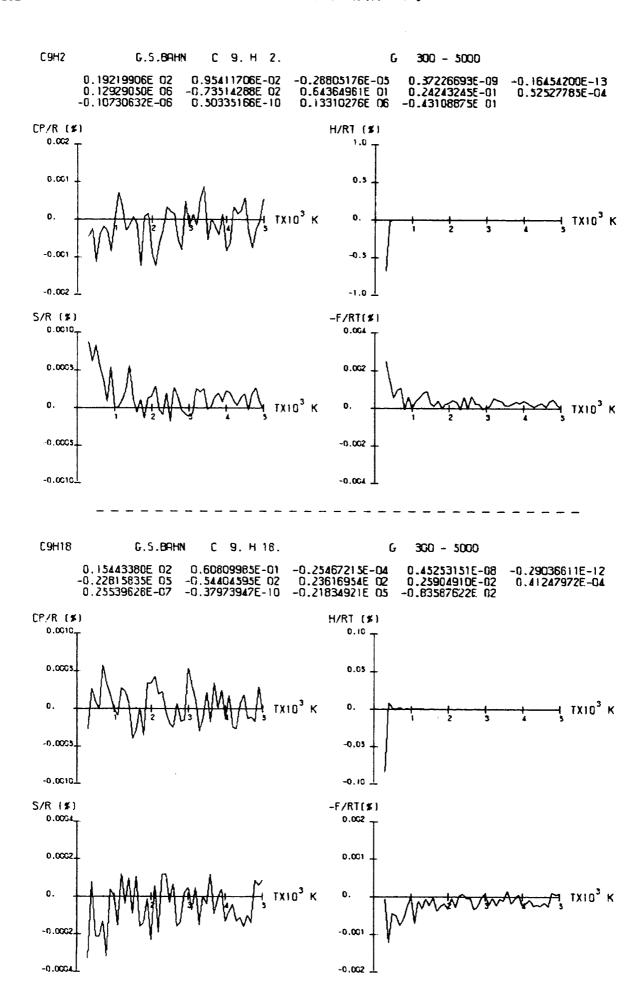


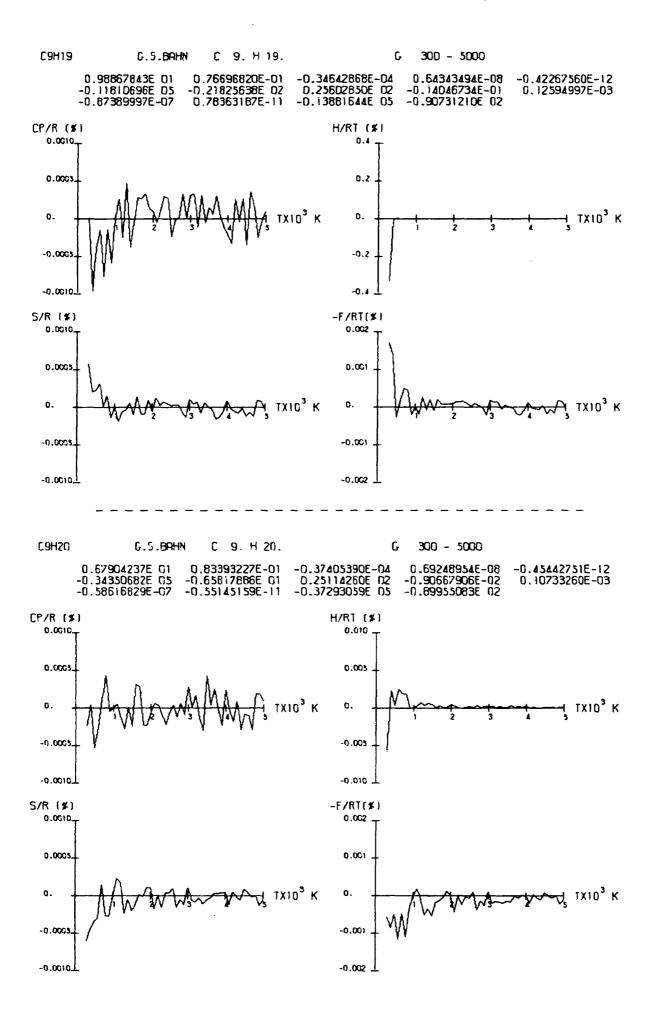


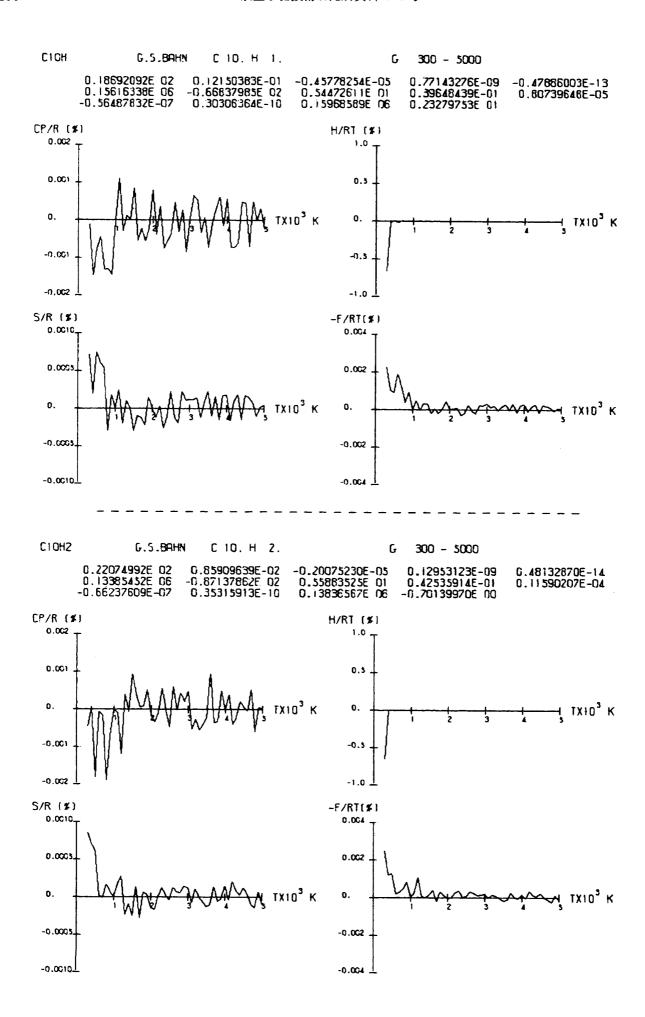


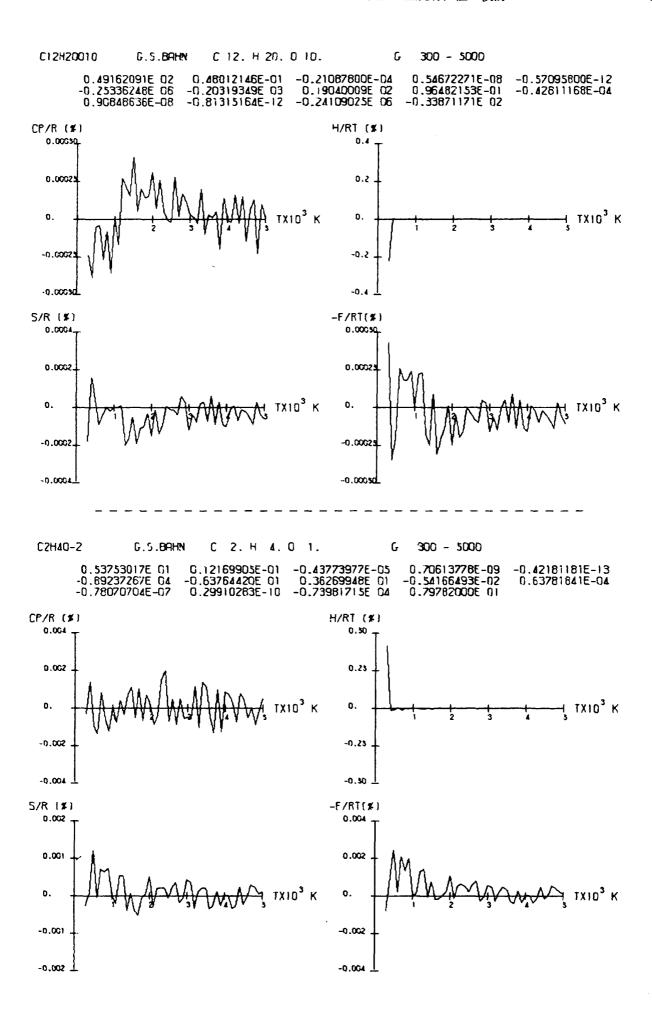


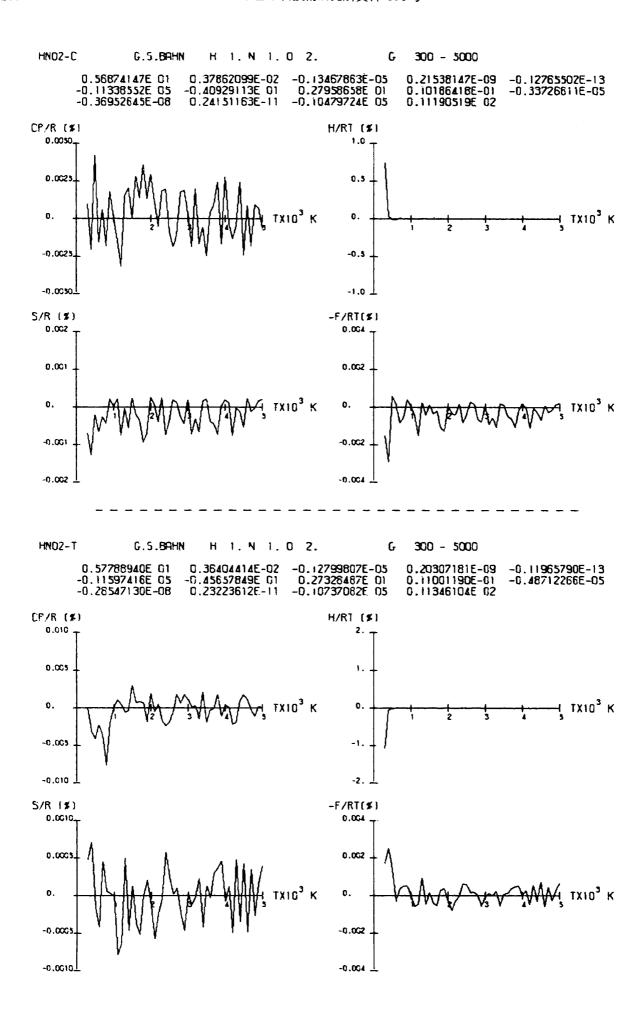


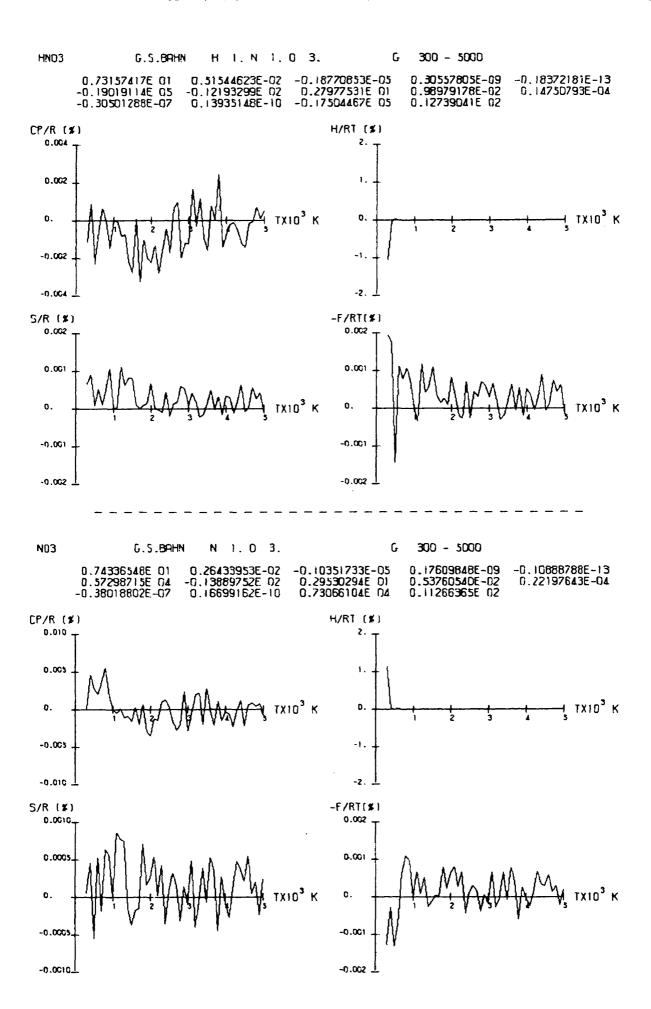


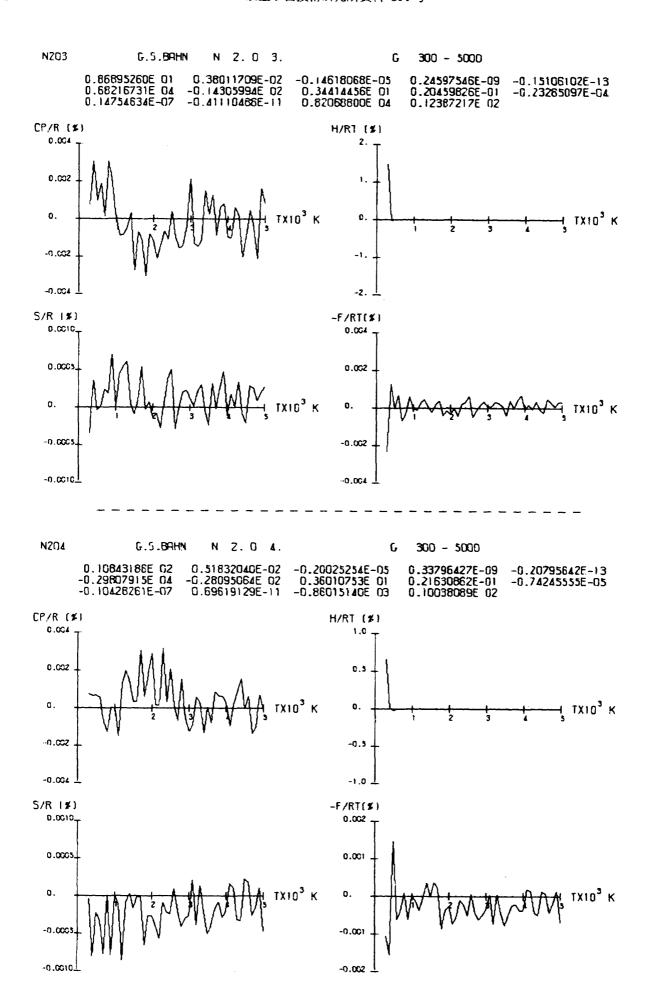


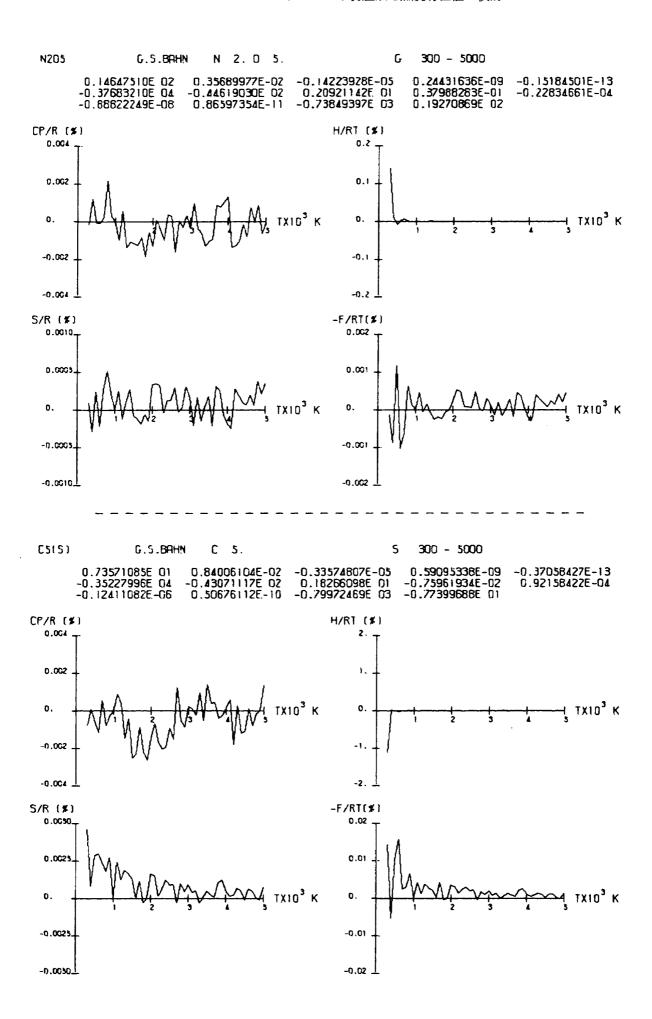


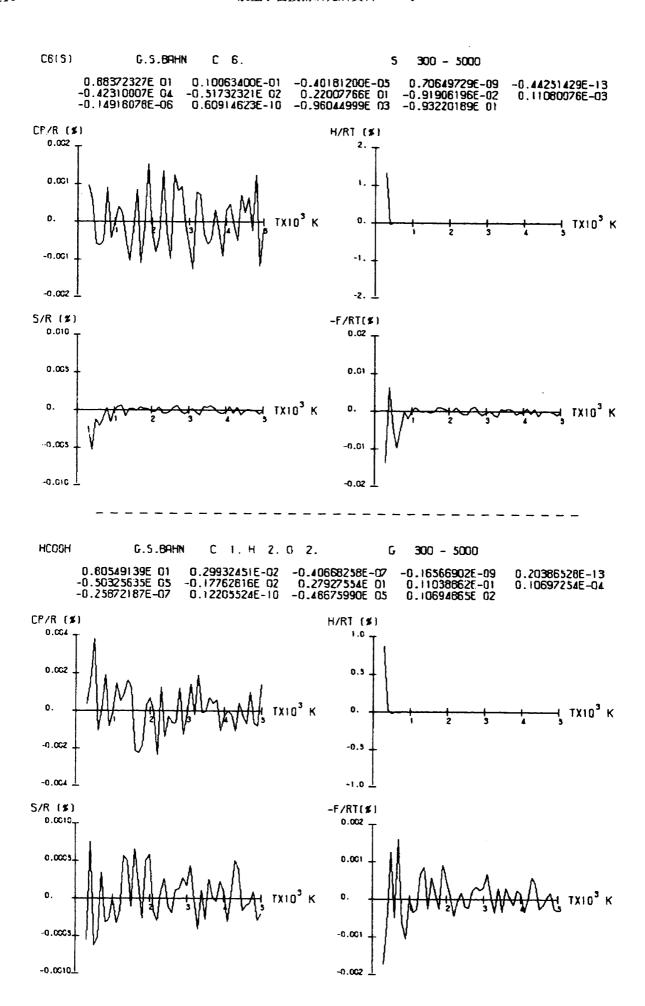


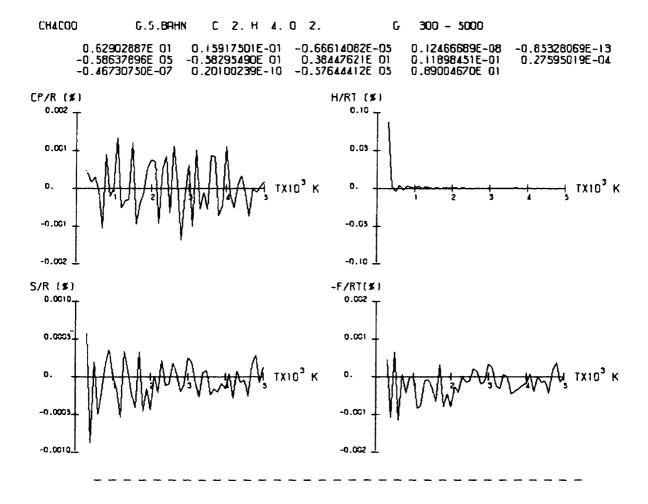












TM-354 正 誤 表

頁	誤	ΙE
P1,左側7行目	JANAF (Joint Arm-	JANAF (Joint Army
	Nary-Airforce)	Navy Airforce)
P 2, 表1		·
P3,表3	データ・リース	データ・ソース
P3,表4-2		

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