

Sixth Aerodynamics Prediction Challenge (APC-6)
2020/09/28, Online



1A15

Aerodynamic prediction of NASA-CRM cruising configuration at low speed and high angle of attack using UTCart

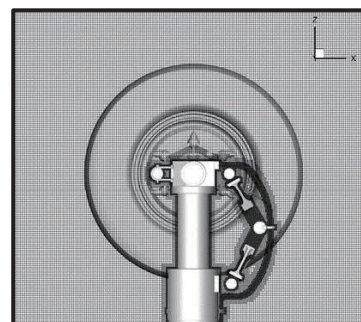
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Objective



- Low-speed and high-AoA flow predictions for NASA-CRM cruising configuration
steady flow simulation + unsteady flow simulation
- UTCart (The University of Tokyo Cartesian grid based automatic flow solver)
 - Unstructured hierarchical Cartesian grid
 - Automatic grid generation
 - The immersed boundary method with a wall function ⁽¹⁾



Imamura and Tamaki, AIAA AVIATION, 2020

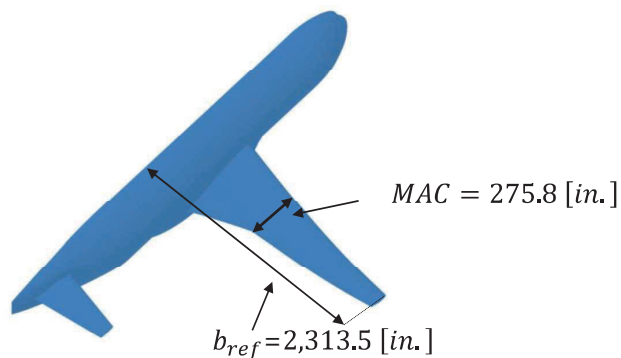
1) Tamaki, and Imamura, AIAA J., Vol 56, 2018.



Computational Condition

• NASA CRM cruising configuration

	Steady	Unsteady
Reynolds number ($C_{ref} = 275.8$ [in.])	1.06×10^6	
Mach number	0.168	
Reference temperature [K]	310	
Angle of attack [deg]	$-3.22 \sim 18.08$	13.08



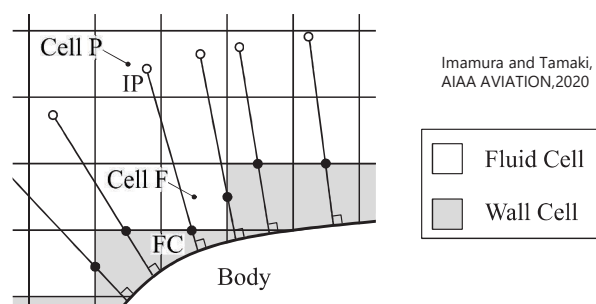
3



Numerical Methods

	Steady	Unsteady
Governing Equation	RANS	DDES⁽¹⁾
Turbulence Model	SA-noft2-R ⁽²⁾	
Inviscid Flux	SLAU+MUSCL($\kappa=1/3$)	
Viscous Flux	2 nd order central difference	
Time Integration	MFGS(Local Time Stepping)	MFGS(Constant dt)
Wall Boundary Condition	IB+SA wall model	
Distance between IP and wall (d_{IP})	$2\Delta x$	

- 1) 玉置 *et al.*, 第49期 年会講演会講演集, 2018
- 2) Dacles-Mariani *et al.*, AIAA J, 1995.

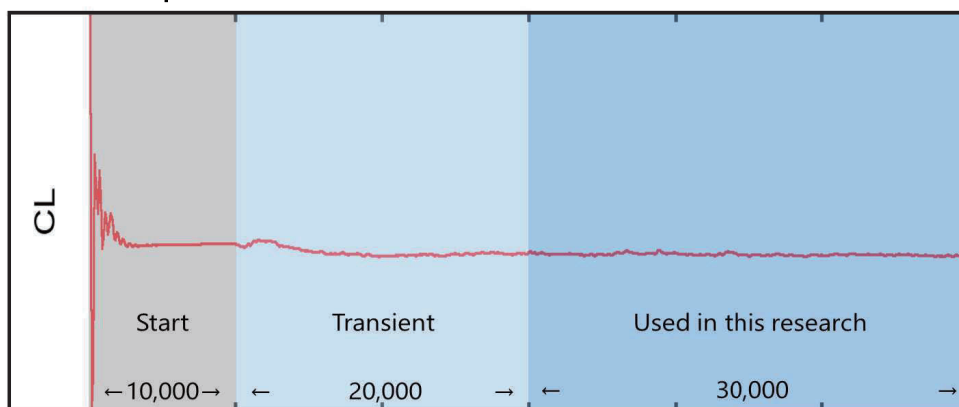


4



Time Integration(MFGS)

- Local time stepping
 - Local courant number : 100
- Constant dt
 - Δt : 3 [-] (about 550 steps for a uniform flow to flow through the MAC)
 - Total steps : 60,000 (Sub iterations : 5)

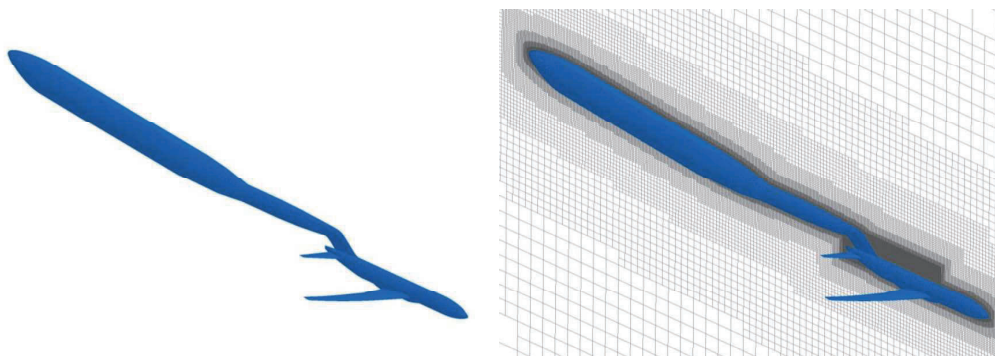


5



Grid Settings

	Steady		Unsteady	BOXFUN (reference)
	w/o sting	w/ sting		
Total cell number	68.5×10^6	81.4×10^6	55.2×10^6	42.5×10^6
Domain size [in.]	2.76×10^4	2.76×10^4	2.76×10^4	2.76×10^4
Minimum grid size [in.]	0.421	0.421	0.421	3.37
RB grid size [in.]	3.37	3.37	3.37	3.37
MAC / Minimum grid size (Real size scale)	655	655	655	81.8

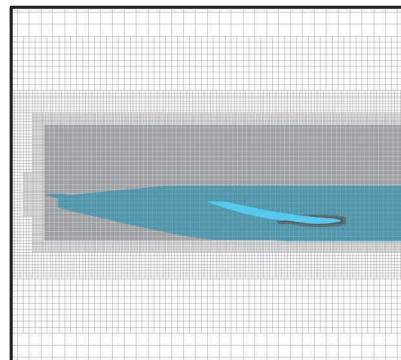
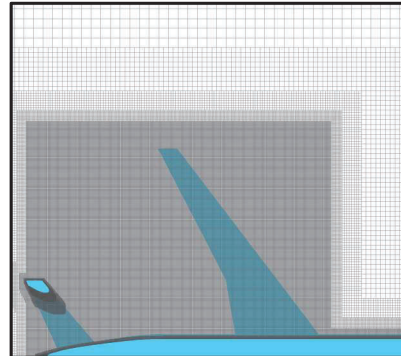
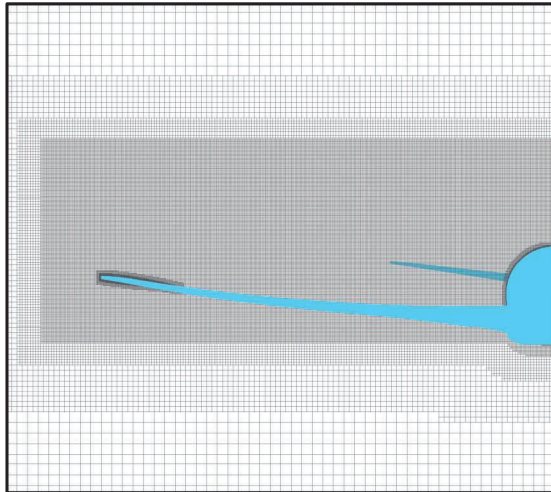


6



Grid Settings

- Refinement Box for steady flow based on BOXFUN

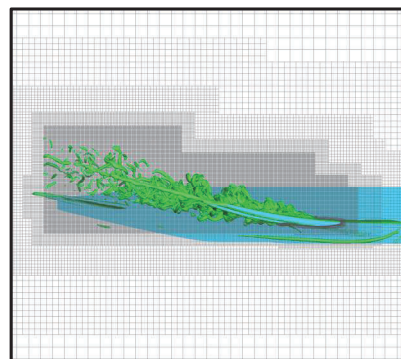
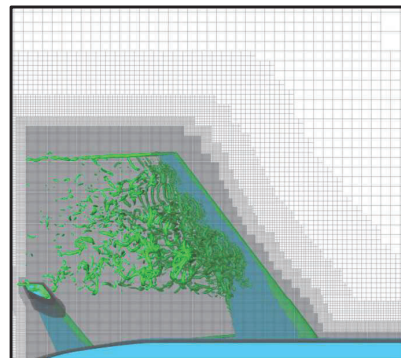
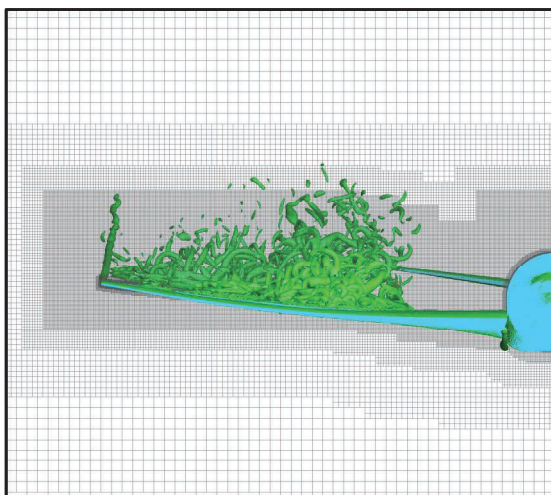


7



Grid Settings

- Refinement Boxes for unsteady flow
 - Total cells reduce from 69M to 55M



8



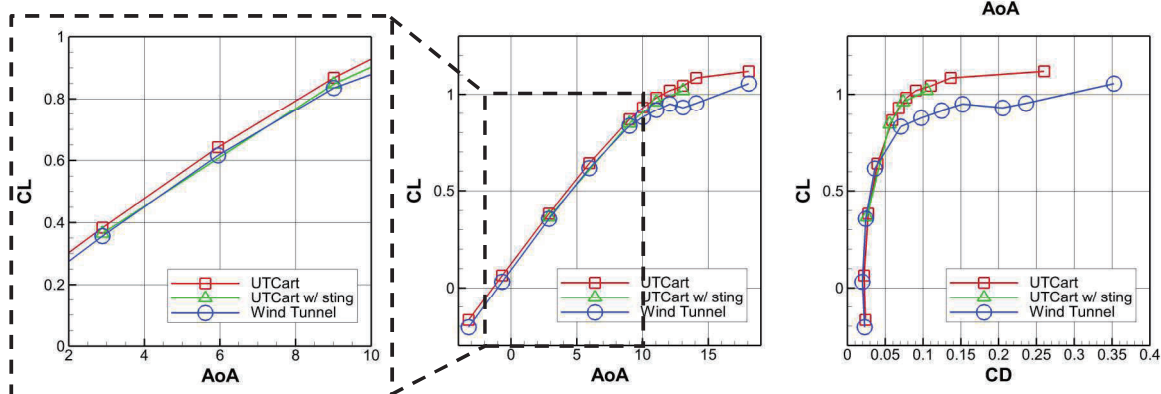
Steady simulation

9



α -sweep (steady flow)

- Good agreement between the results of UTCart and experiment at low AoA
 - Sting has effects on the wind tunnel experiment

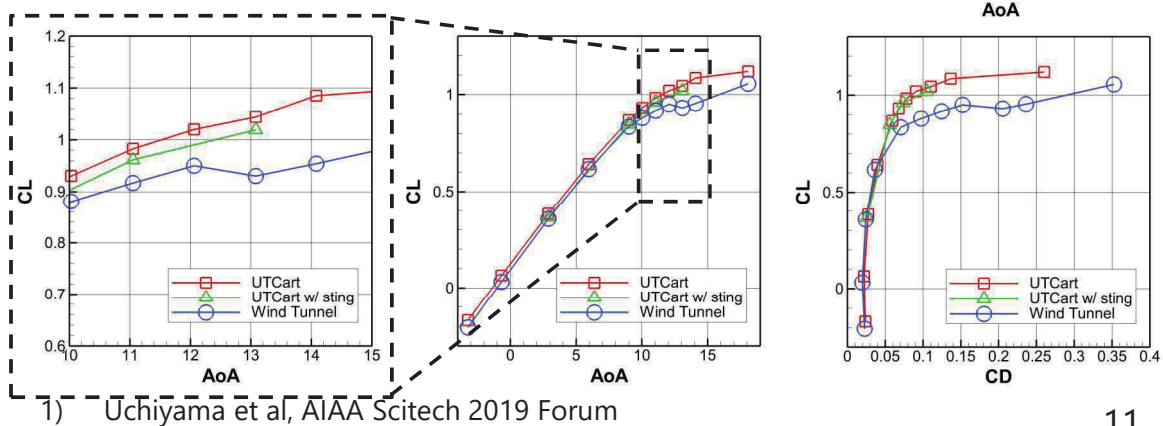


10



α -sweep (steady flow)

- Larger CL and smaller CM of UTCart than those of experiment at high AoA
 - separation occurs on the wingtip and trailing edge from 9.01 [deg] in the wind tunnel experiment. ⁽¹⁾



11



Unsteady simulation

12



CL, CD, CM (unsteady flow)

- The results in unsteady simulation are closer to the ones in experiment than steady simulation.

13.08 [deg]	Experiment	Steady		Unsteady
		w/o sting	w/ sting	
CL	0.9305	1.0444	1.0196	0.9789
(error)	(0)	(11×10^{-2})	(9.0×10^{-2})	(4.8×10^{-2})
CD	0.2053	0.1103	0.1051	0.1240
(error)	(0)	(9.4×10^{-2})	(10×10^{-2})	(8.1×10^{-2})
CM	0.0186	-0.0844	-0.0262	-0.0396
(error)	(0)	(10×10^{-2})	(4.5×10^{-2})	(5.8×10^{-2})

$$\text{error} := |CX_{\text{experiment}} - CX|$$

13

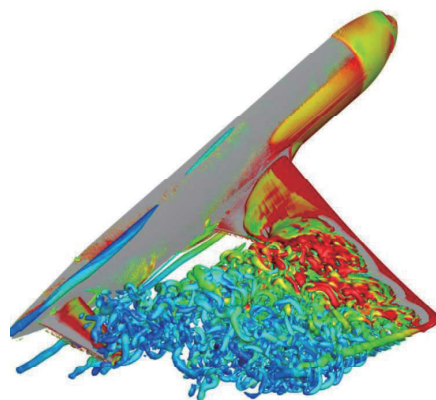


Wake from main wing

- Separation occurs in unsteady simulation



Density Gradient Magunitude at y = 400[in.]



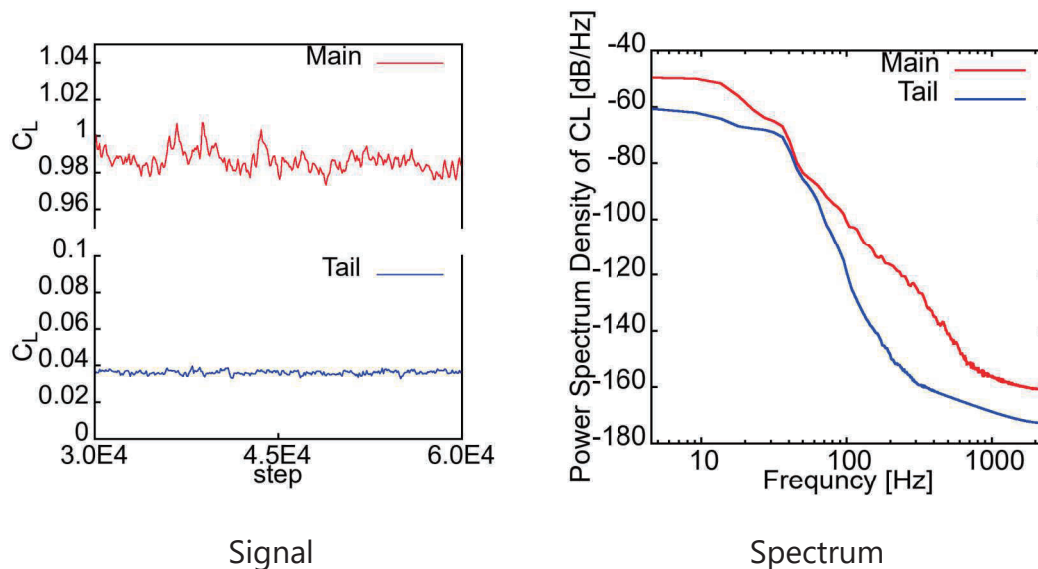
Isosurface of q-criterion = 10^{-6} ,
colored by density gradient.

14



Unsteady Forces Spectrum

- Lift coefficient of main and tail wing
 - No noteworthy periodicity can be observed in this simulation



15

Conclusion



- Steady / Unsteady flow are simulated by UTCart
 - The trend of each aerodynamic coefficients is consistent with the reference experimental data at low angles of attack.
 - The results in unsteady simulation are closer to the experimental results at high angle of attack.

16