

**21KT009601****APC-7 (講演番号:1A16)****CflowによるNASA巡航CRMの  
低速高迎角剥離流れの予測 [課題1]****Prediction of Low-speed, High-angle-of-attack Separated Flows  
for the NASA-CRM Cruise Configuration using Cflow****上野 陽亮、安田 英将、澤木 悠太**

Yosuke Ueno, Hidemasa Yasuda, Yuta Sawaki

川崎重工業(株) 航空宇宙システムカンパニー

2021年6月30日(水)

第53回流力講演会/第39回ANSS@オンライン

**Outline****■ Outcome of APC-6**

- Effect of **grid** (Provided vs Cflow)

**■ Focus of APC-7**

1. Effect of **turbulence model** (SA-noft2 vs SA-neg\*)
2. Effect of **time integration** (Local vs Global time step)
3. Effect of **initial condition** (Impulsive vs Lower AoA)

**■ Summary**

\* The reason for using SA-neg in APC-7 is that SA-neg is used in another CFD workshop (AIAA HLPW-4) and has already been verified in our Cflow solver.

## Outcome of APC-6

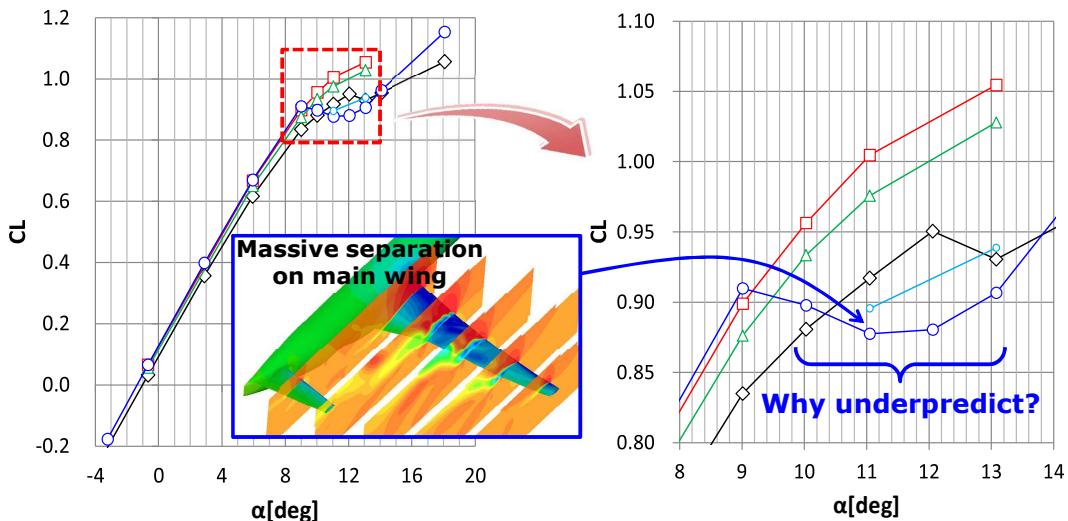
$M=0.168$   
 $Re=1.06 \times 10^6$

### ● Effect of grid

- ✓ Provided grids overpredict stall angle and  $CL_{max}$ .
- ✓ Cflow grids underpredict stall angle and  $CL_{max}$ .

APC-7

- JAXA Exp.
- HexaGrid
- BOXFUN
- Cflow-Coarse
- Cflow-Medium



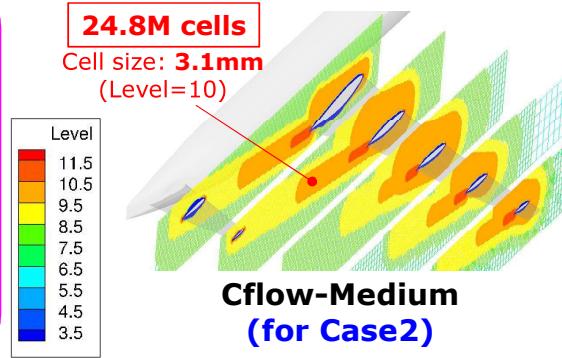
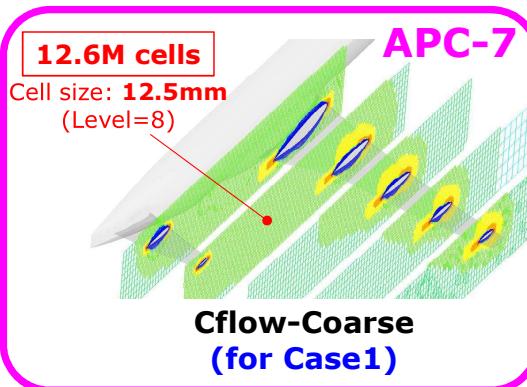
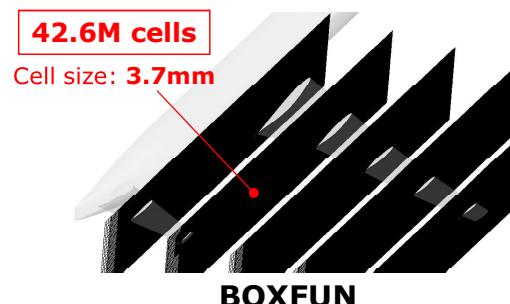
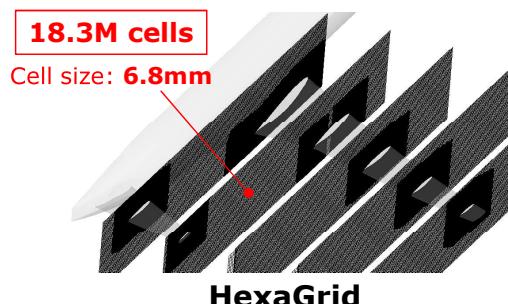
© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

21KT009601

Kawasaki  
Powering your potential

3

## Grid Comparison



© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

21KT009601

Kawasaki  
Powering your potential

4

## Numerical Method

CFD tool	Cflow (KHI in-house)
Governing Equations	<b>Three-dimensional compressible Navier-Stokes equations</b>
Spatial Discretization	Cell-centered finite volume method with 2 <sup>nd</sup> -order accurate reconstruction based on MUSCL
Inviscid Flux	<b>SLAU</b> (Simple Low-dissipation AUSM scheme)
Viscous Flux	2 <sup>nd</sup> -order accurate central difference
Turbulence Modeling	<b>SA-neg</b> (Negative Spalart-Allmaras One-Equation Model) * <b>SA-noft2@APC-6</b>
Time Integration	<b>MFGS implicit method with local/global time stepping</b>
Parallelization	Domain decomposition method with MPI

### References for **Cflow** details

- Ueno, Y. and Ochi, A., "Airframe Noise Prediction Using Navier-Stokes Code with Cartesian and Boundary-fitted Layer Meshes," 25th AIAA/CEAS Aeroacoustics Conference, (AIAA 2019-2553).
- Atsushi Hashimoto, Takashi Aoyama, Yuichi Matsuo, Makoto Ueno, Kazuyuki Nakakita, Shigeru Hamamoto, Keisuke Sawada, Kisa Matsushima, Taro Immura, Akio Ochi, and Minoru Yoshimoto, "Summary of First Aerodynamics Prediction Challenge (APC-I)," 54th AIAA Aerospace Sciences Meeting, AIAA SciTech, (AIAA 2016-1780).
- Yasushi Ito, Mitsuhiro Murayama, Atsushi Hashimoto, Takashi Ishida, Kazuomi Yamamoto, Takashi Aoyama, Kentaro Tanaka, Kenji Hayashi, Keiji Ueshima, Taku Nagata, Yosuke Ueno and Akio Ochi, "TAS Code, FaSTAR and Cflow Results for the Sixth Drag Prediction Workshop," Journal of Aircraft, Vol. 55, No. 4, pp. 1433-1457, 2018.
- Yasushi Ito, Mitsuhiro Murayama, Yuzuru Yokokawa, Kazuomi Yamamoto, Kentaro Tanaka, Tohru Hirai, Hidemasa Yasuda, Atsushi Tajima and Akio Ochi, "Japan Aerospace Exploration Agency's and Kawasaki Heavy Industries' Contribution to the Third High Lift Prediction Workshop," 2018 AIAA Aerospace Sciences Meeting, AIAA SciTech, (AIAA 2018-1034).

© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

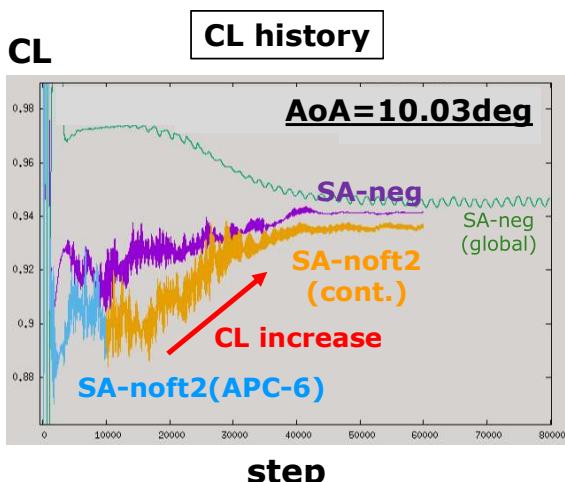
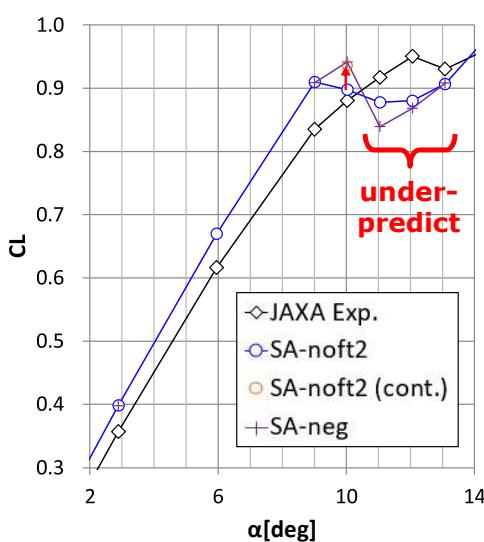
21KT009601

Kawasaki  
Powering your potential

5

## Focus of APC-7 (1) Effect of turbulence model

**M=0.168**  
**Re=1.06 × 10<sup>6</sup>**



\*APC-6: SA-noft2, only 10,000 steps  
\*APC-7: SA-neg, more than 50,000 steps

- SA-neg and SA-noft2 bring similar results for this case
- Further investigation on QCR and RC effects is needed

© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

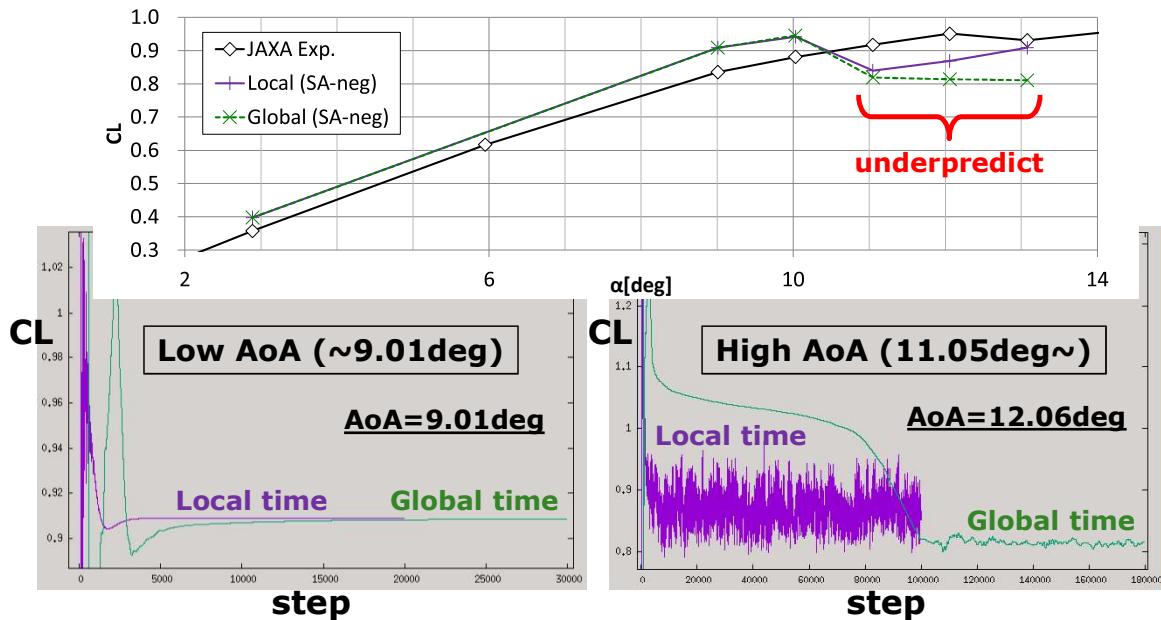
21KT009601

Kawasaki  
Powering your potential

6

## Focus of APC-7 (2) Effect of time integration

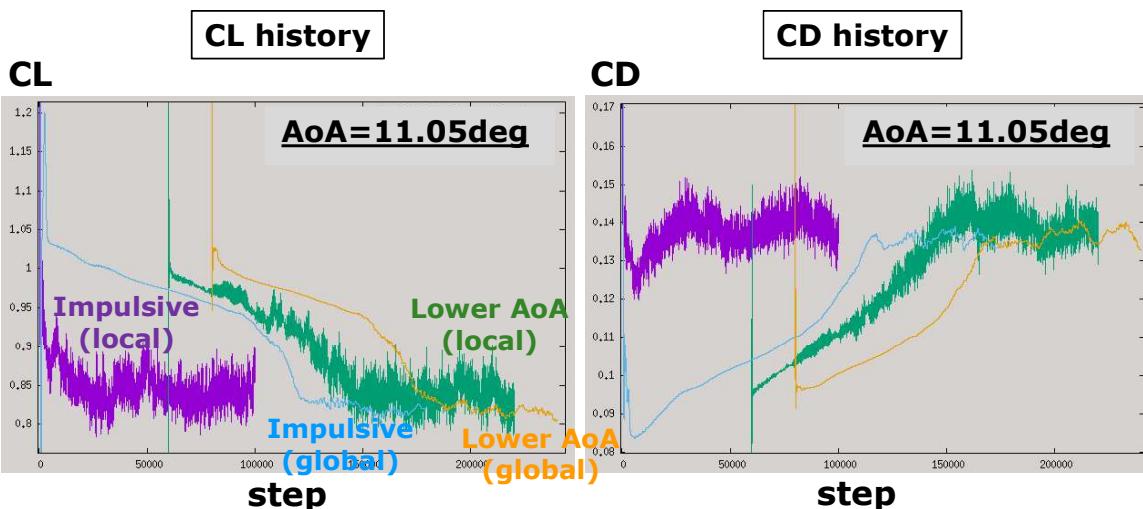
$M=0.168$   
 $Re=1.06 \times 10^6$



- Converge to same result (steady flow)
- Global needs more time steps
- Not converge (unsteady flow)
- Global needs more time steps

## Focus of APC-7 (3) Effect of initial condition

$M=0.168$   
 $Re=1.06 \times 10^6$



- Restart from the lower-AoA result (warm start) brings the same result as impulsive (cold start) both in local and global time steps

## Summary

- For steady-state RANS computations with Cflow-Coarse grid used in APC-6, **the effects of several computational parameters** were investigated to improve predictive capability in low-speed high-angle-of-attack aerodynamics.
- **Lessons Learned: not improved...**
  - ✓ **Effect of turbulence model (SA-noft2 vs SA-neg):**  
little effect, need further investigation on QCR and RC effects
  - ✓ **Effect of time integration (Local vs Global time step):**  
similar results, global needs more time steps
  - ✓ **Effect of initial condition (Impulsive vs Lower AoA):**  
similar results (investigated only for AoA=11deg)
- Future work
  - ✓ Establish “**best practices**” (trade-off between **accuracy** and **cost**)
  - ✓ More complicated high-lift configuration (**CRM-HL**, see **2C09**)

Kawasaki, working as one for the good of the planet

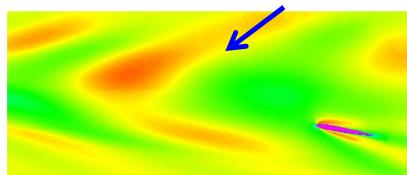
**“Global Kawasaki”**

## 【補足】提出データについて

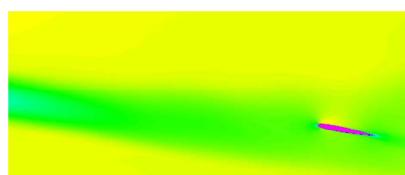
- ローカルタイムステップの定常解析結果は、高迎角( $\geq 11\text{deg}$ )で解が収束せずに振動しているが、APC-6同様に今回事務局に提出したデータ(カデータ、可視化図)は最終ステップの瞬時値である。
- 一方、本資料に示したカデータ(CL, CD, Cm)は、圧力分と摩擦分を足し合わせたものであり、Cflowの解析ログから平均化して求めたものである。
- よって、APC事務局作成のまとめ資料と本資料のカデータは若干異なる。

提出データの一例

収束していない結果(p.8のCL履歴参照)の  
最終ステップの瞬時値であるため斑な分布



Local time step

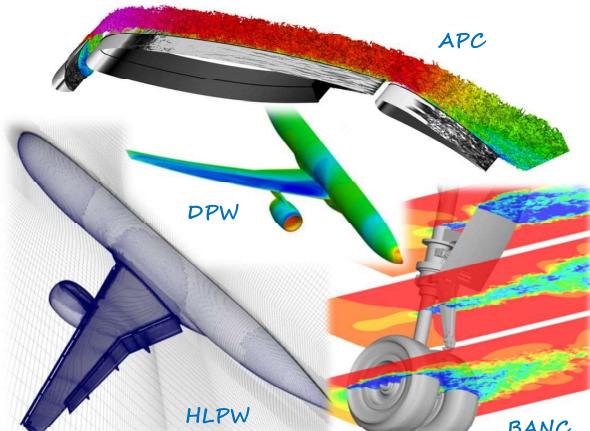


Global time step

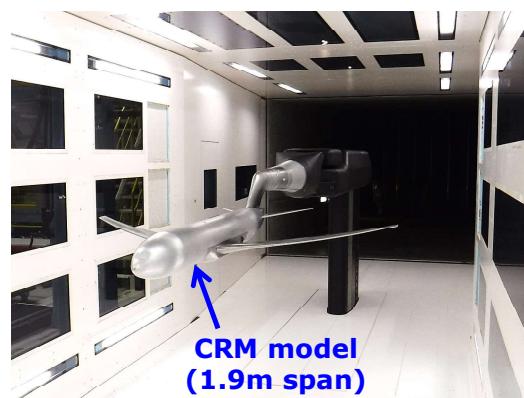
断面流速分布(Section YB, AoA=11.05deg)

## Motivation

- Practical use of CFD in the aircraft design
- Validation of KHI in-house CFD tool for low-speed aerodynamics
- Facilitation of CFD-WTT collaboration



**KHI in-house CFD tool "Cflow"**  
**(highly complicated geometry,  
unsteady, large-scale)**



**KHI new wind tunnel**  
**(low-speed, low-noise)**

## Cflow (KHI in-house CFD tool)

- ✓ Kawasaki originally developed "Cflow"

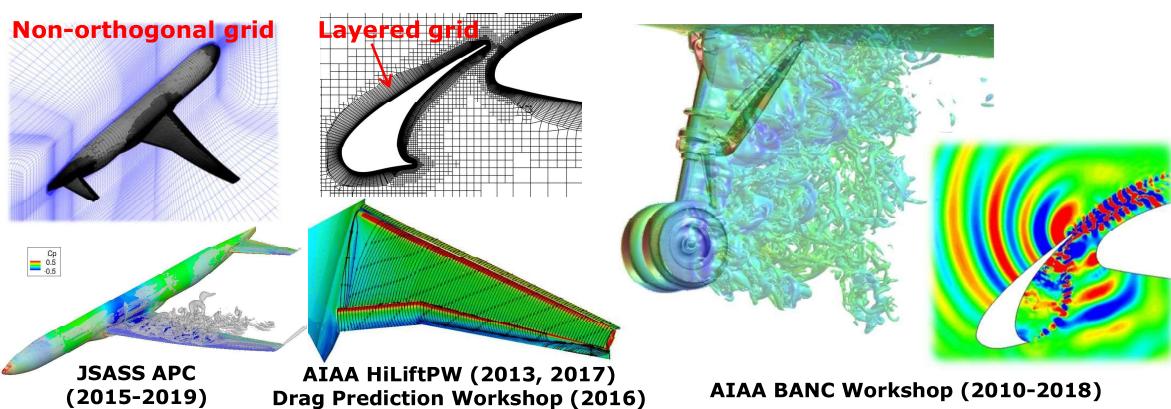
$$\text{Cflow} = \boxed{\text{Grid Generator}} + \boxed{\text{Flow Solver}}$$

highly complicated

large-scale

unsteady

- ✓ Cflow has been validated in various workshops.



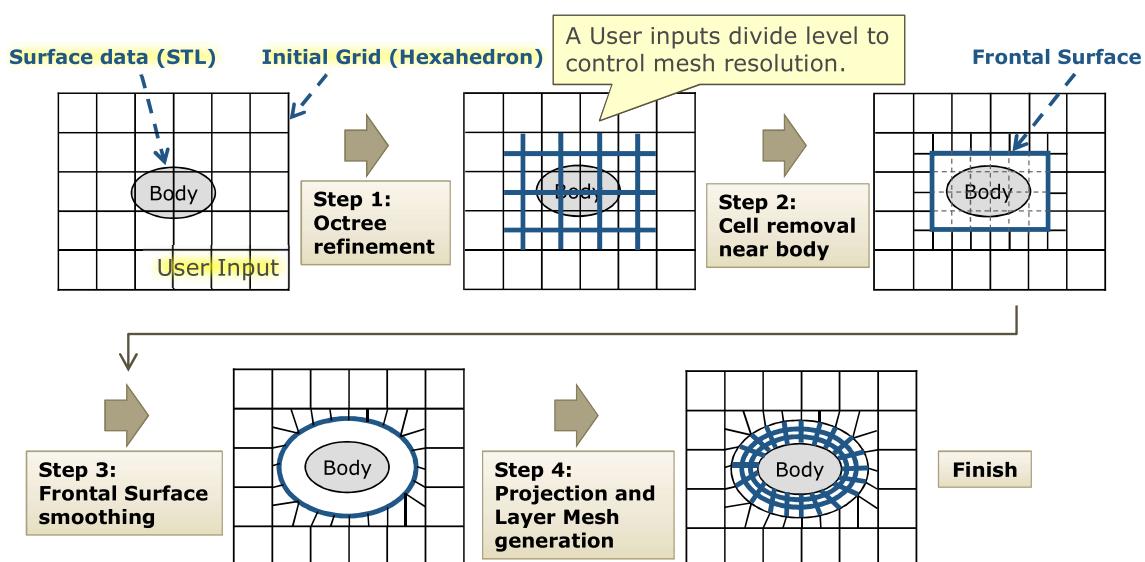
© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

21KT009601



13

## Grid Generation Procedure in Cflow



Cflow automatically generates body-fitted layered grids on no-slip walls to resolve boundary layers and hexahedral grids in the other regions.

© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

21KT009601

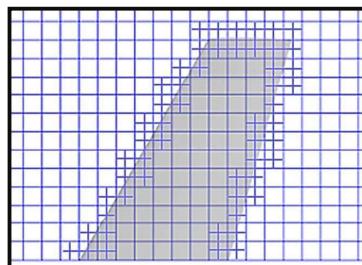


14

## Initial Grid of Cflow

**There are 2 options for initial grid of Cflow.**

**Cartesian Grid**

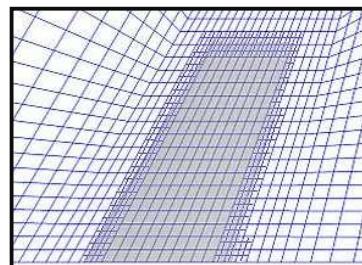


- grid generation robustness
- unsteady simulation  
(resolving vortices)
- acoustic wave propagation

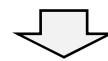


**Noise prediction from complicated geometry**

**Non-orthogonal Grid**



- reduction of total cells  
(high aspect ratio)
- sweptback cells
- oblique shock wave



**Steady simulations**

© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

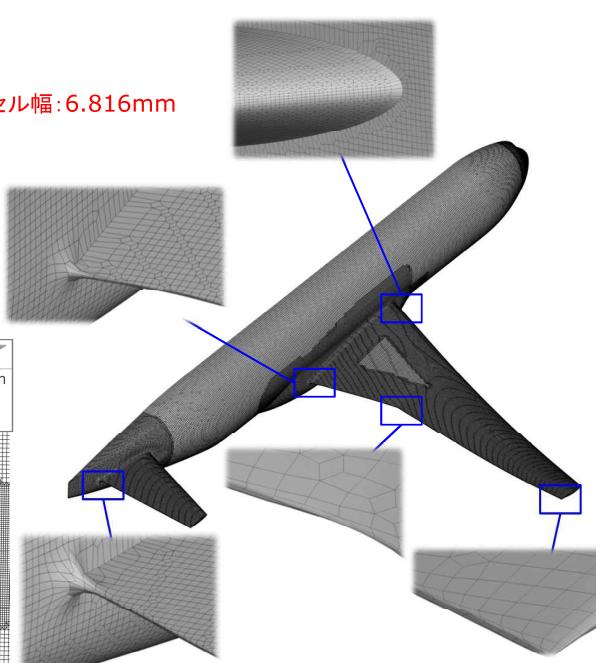
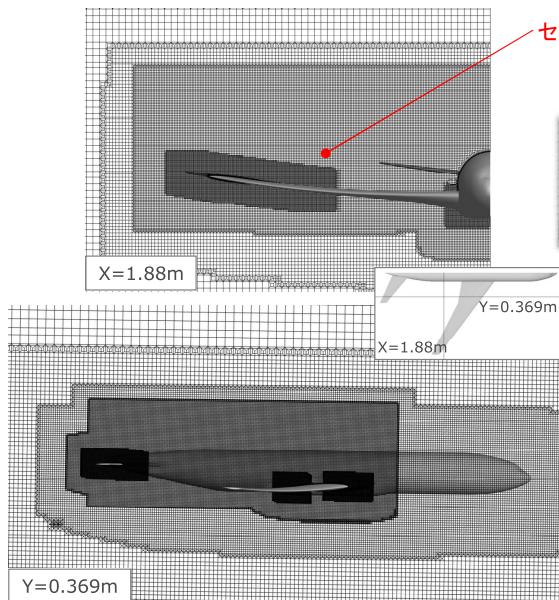
21KT009601



15

## Grid (HexaGrid)

空間セル数: 1830万セル  
最小格子幅:  $8.3 \times 10^{-6}$  m



© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

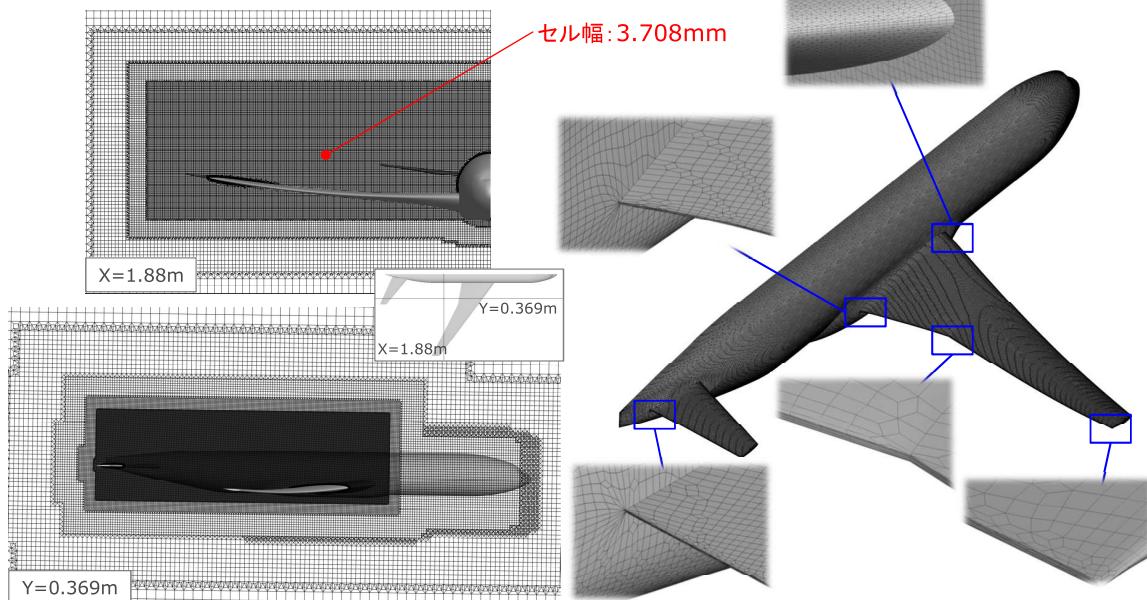
21KT009601



16

## Grid (BOXFUN)

空間セル数: 4260万セル  
最小格子幅:  $5.2 \times 10^{-6}$  m



© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

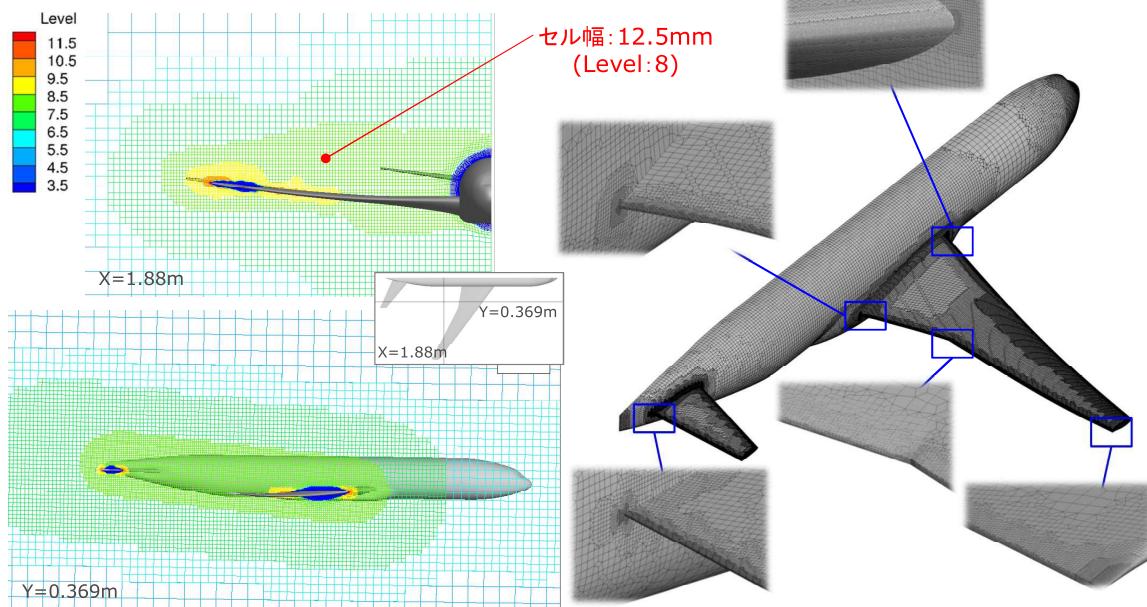
21KT009601



17

## Grid (Cflow-Coarse)

空間セル数: 1260万セル  
最小格子幅:  $8.0 \times 10^{-6}$  m



© 2021 Kawasaki Heavy Industries, Ltd. All Rights Reserved

21KT009601



18

## Grid (Cflow-Medium)

空間セル数: 2480万セル  
最小格子幅:  $8.0 \times 10^{-6}$  m

