

Seventh Aerodynamics Prediction Challenge (APC-7)  
2021/06/30, Online



# Aerodynamic Analysis of NASA-CRM at Low Speed and High Angle of Attack conditions Using Hierarchical Cartesian Mesh and Recursive Fitting Method

階層型直交格子と再帰的なフィッティングを用いた  
低速・高迎角条件におけるNASA-CRM巡航形態の空力予測

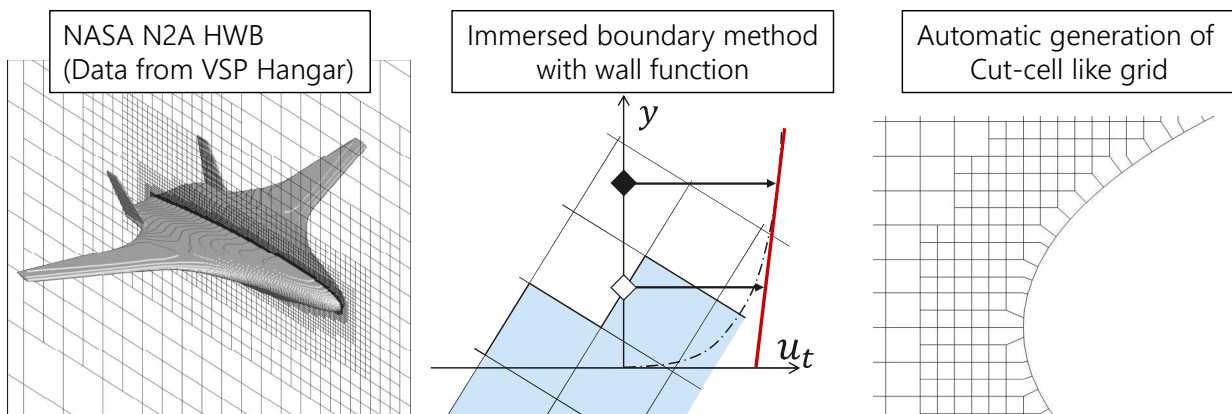
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(The University of Tokyo)



## Background



- Development of **UTCart** for aerodynamic designing of aircraft.
  - Automatic grid generation based on octree structure.
  - Compressible RANS/DDES simulation with wall function.
  - Immersed Boundary method (**IBM**) on stair-step grids.
  - Simulation on cut-cell like grid is also developed<sup>1,2</sup>.



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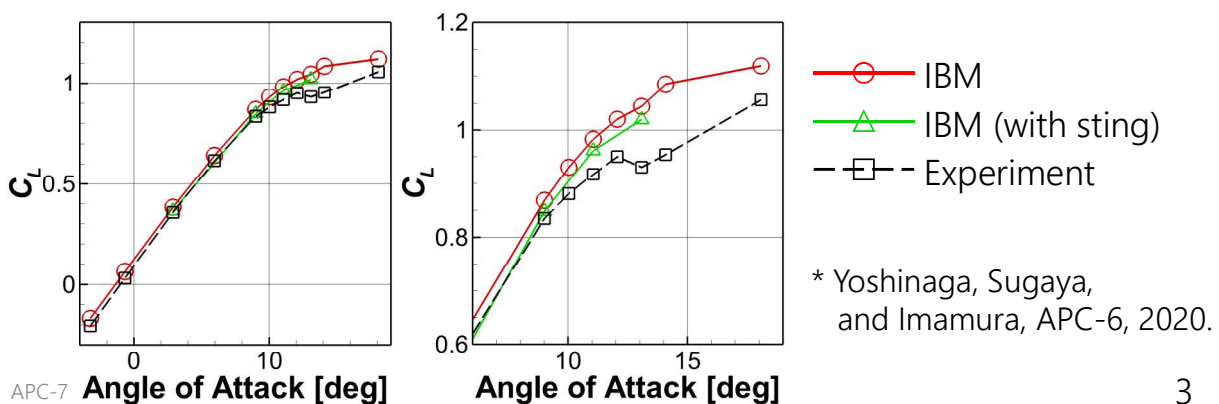
1. Harada, Tamaki, Takahashi, and Imamura, AIAA J, 2017.  
2. 菅谷 和 今村, 日本航空宇宙学会論文集, 2020.

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## Results of APC-6\* (IBM simulation)

- A fair agreement of aerodynamics between UTCart and experiment at low AoA.
- Large  $CL$  than that of experiment at high AoA.
- Influence of numerical methods on aerodynamics prediction needs to be investigated.
- Further study of dependency on grid size is necessary.



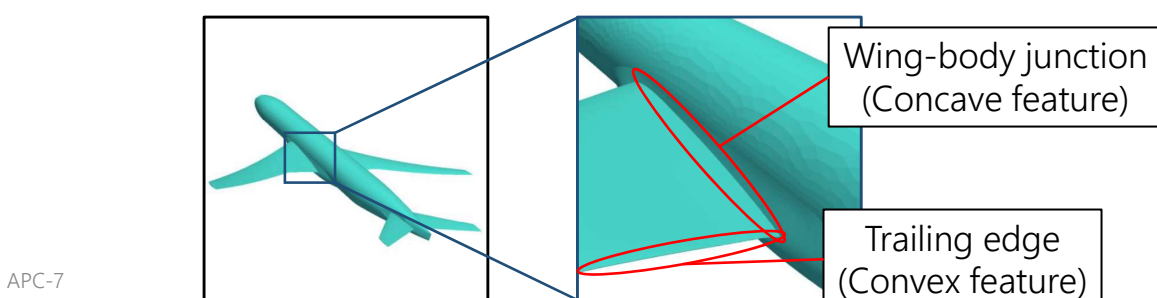
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## Objective



Investigate prediction accuracy of flow simulation around NASA-CRM using Recursive Fitting Method.

- Cartesian grid based automatic body-fitted grid generation.
  - Geometric features are approximately represented.
- Comparison with simulation using IBM (APC-6).
  - Conservation laws are satisfied in simulation using Recursive Fitting Method (RFM), as opposed to IBM.



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## Recursive Fitting Method (RFM)\*

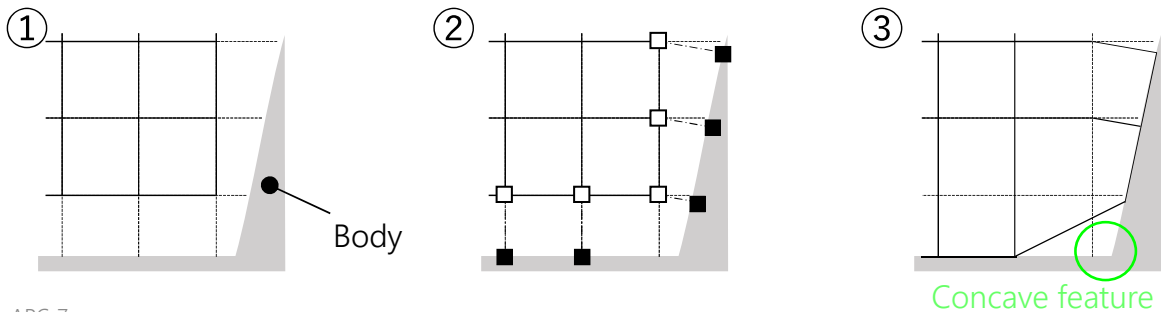
1. Generate the stair-step grid.
2. Calculate the closest points to the vertices of the cell faces.
3. Extend fluid cells to body surfaces.

○ Automatic grid generation around two- and three-dimensional bodies.

△ Cell faces does not match body surfaces around geometric features.

- Wing-body juncture, Trailing edge,...

→ Necessary to modify cells around features.



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\* 菅谷 and 今村, 日本航空宇宙学会論文集, 2020.<sup>5</sup>

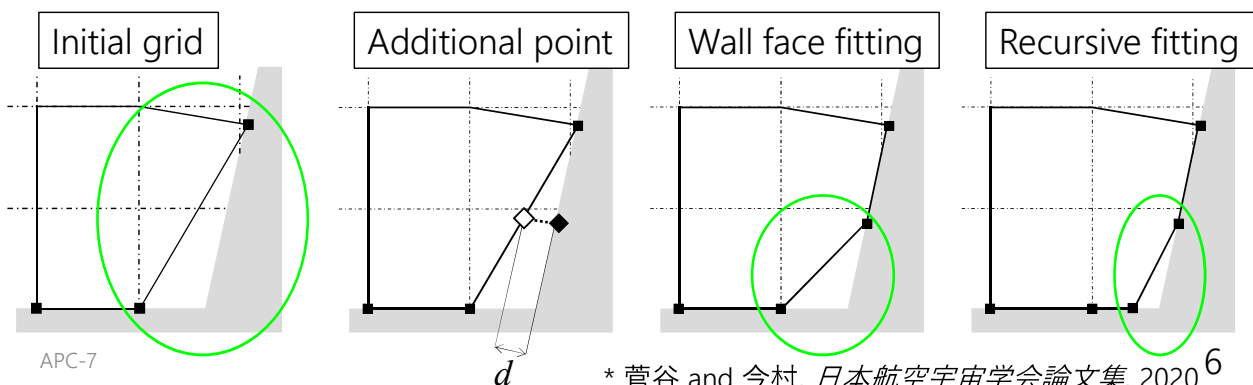


## Recursive Fitting Method (RFM)\*

- Recursively fitting the wall face to body surfaces
- Modified the cell properties which is necessary for flow simulation

$$\frac{\partial(Q_c V_i)}{\partial t} + \sum_{j \in \text{neighbor}(i)} F(Q_i, Q_j, \mathbf{n}_{ij}) s_{ij} = 0$$

- The number of cells and cell faces are kept unchanged.
- Repeating fitting procedure recursively until the distance between wall face and wall becomes smaller than user-specified parameter.



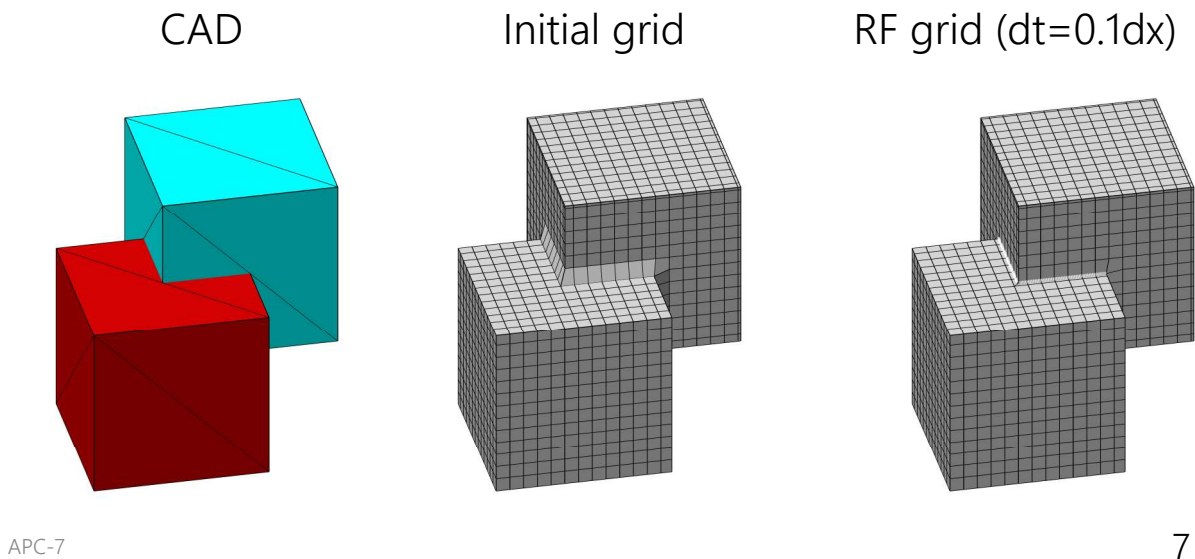
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\* 菅谷 and 今村, 日本航空宇宙学会論文集, 2020.<sup>6</sup>



## Example of RF grid

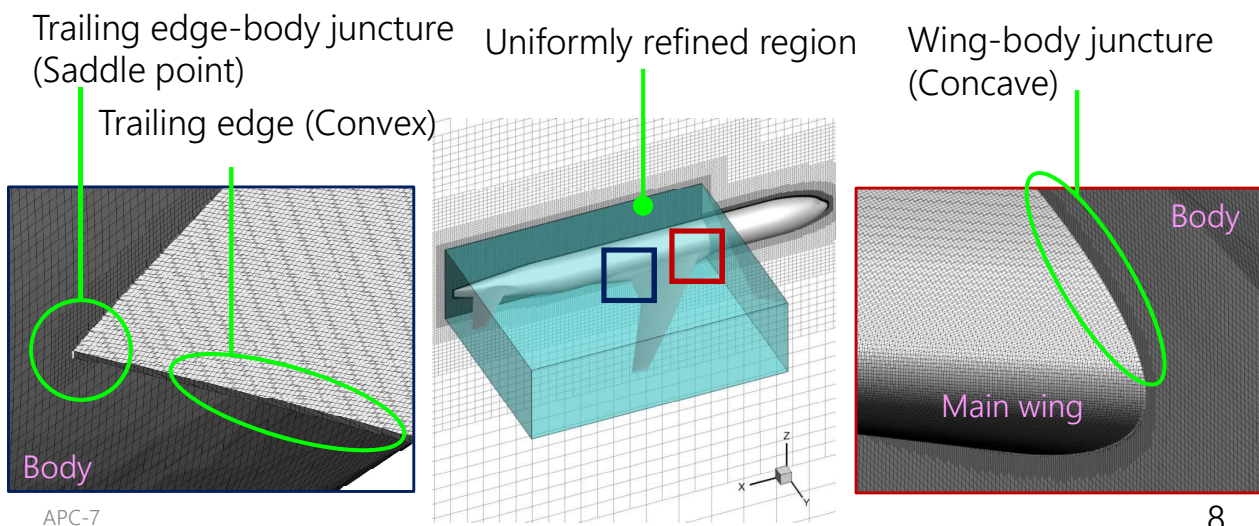
- Grid generation around Intersecting cubes.
- Features are approximately represented in RF grid.



## Computational Grid Setting

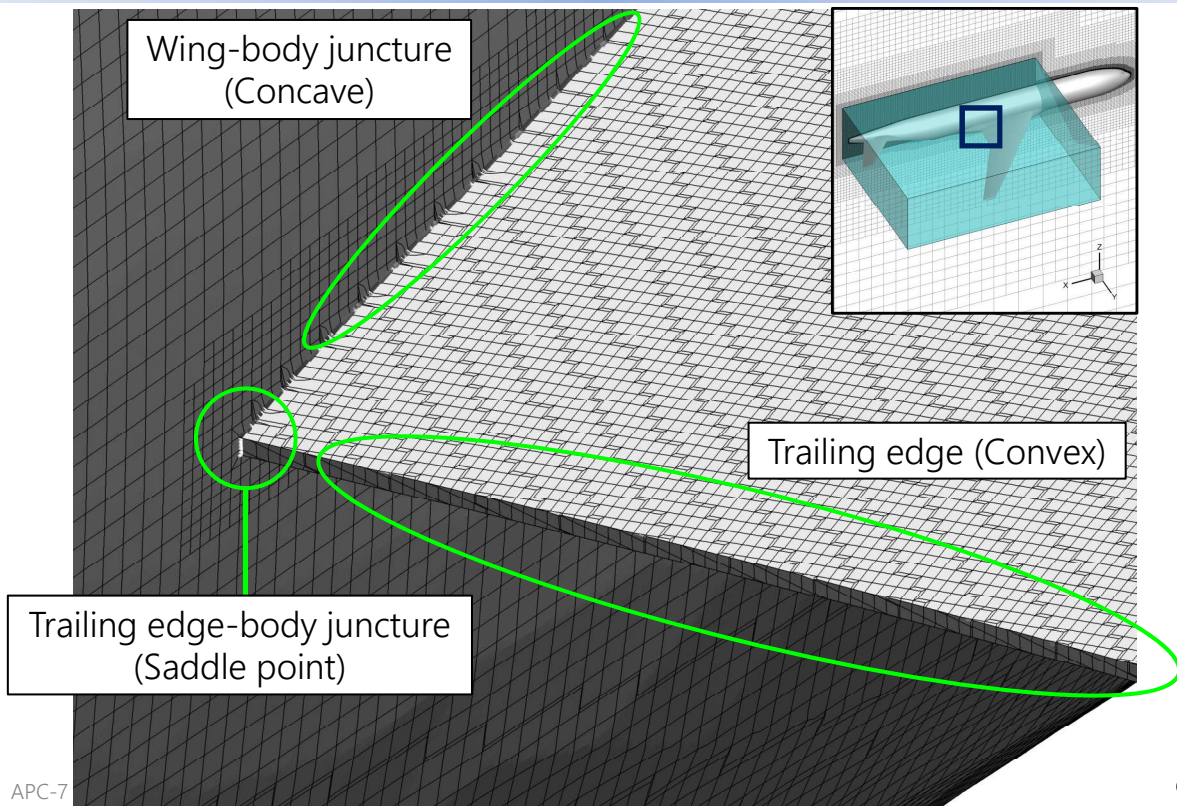


- Same grid setting as APC-6.
- Total cell number: 68.5 M
- $C_{MAC}/\Delta x \sim 655$ ,  $y^+ = 40 \sim 100$  on main wing
- Uniformly refined region between main wing and tail.





# Computational Grid of NASA-CRM



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## Numerical methods



- Turbulence Model (Steady) : SA-noft2-R (Crot=1)
  - Turbulence Model (Unsteady) : DDES-protected\*
    - RANS region is protected even when the stream-wise grid size is small.
  - **Wall Function** : **SA wall model**
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- Inviscid flux : Linear reconstruction+ SLAU
    - **Limiter for recursively modified cells.**
  - Viscous flux : 2nd order Central difference
- 
- Time integration(Steady) : MFGS + Local Time Stepping
    - Start from free-stream conditions.
  - Time integration(Unsteady) : MFGS + BDF2 with 5 Inner Iteration
    - Restart form RANS results.
    - Courant number  $\sim 1$  at wake region.

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\* 玉置 *et al.*, 第49期年会講演会講演集, 2018. 10



## Case 1

### Steady Simulation

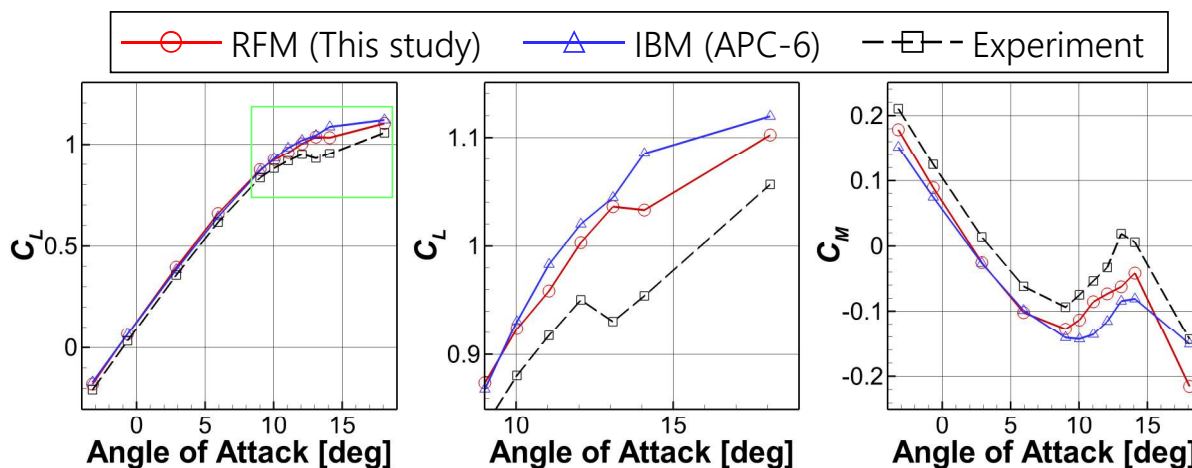
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## Alpha sweep



- A fair agreement between RFM, IBM, and exp. at low AoA.
- Predicted  $CL$  and  $CM$  using RFM is closer to exp. than those of IBM at high AoA.
- $CL$  decrease at AoA = 13.08 to 14.08 [deg] in RFM simulation.



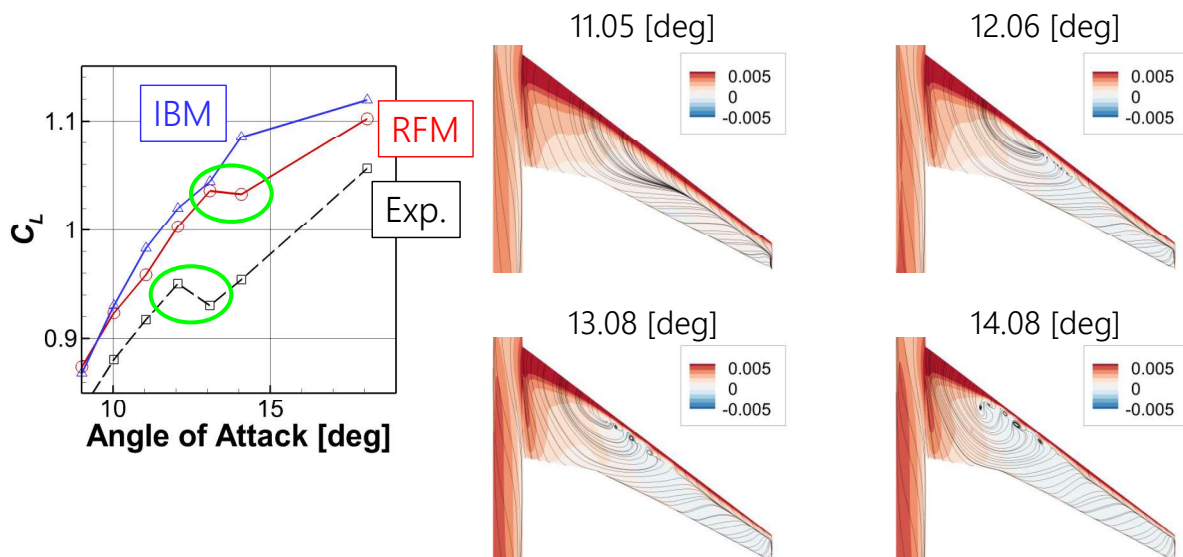
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# Streamline and skin friction

- Separating region ( $C_f < 0$ ) gradually expands as AoA increases.
- Causing discrepancy of  $C_L$  between RFM and experiment.
  - $C_L$  of exp. suddenly changes at AoA=12 due to large flow separation\*.



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\* Uchiyama et al. AIAA Paper 2019-2190.

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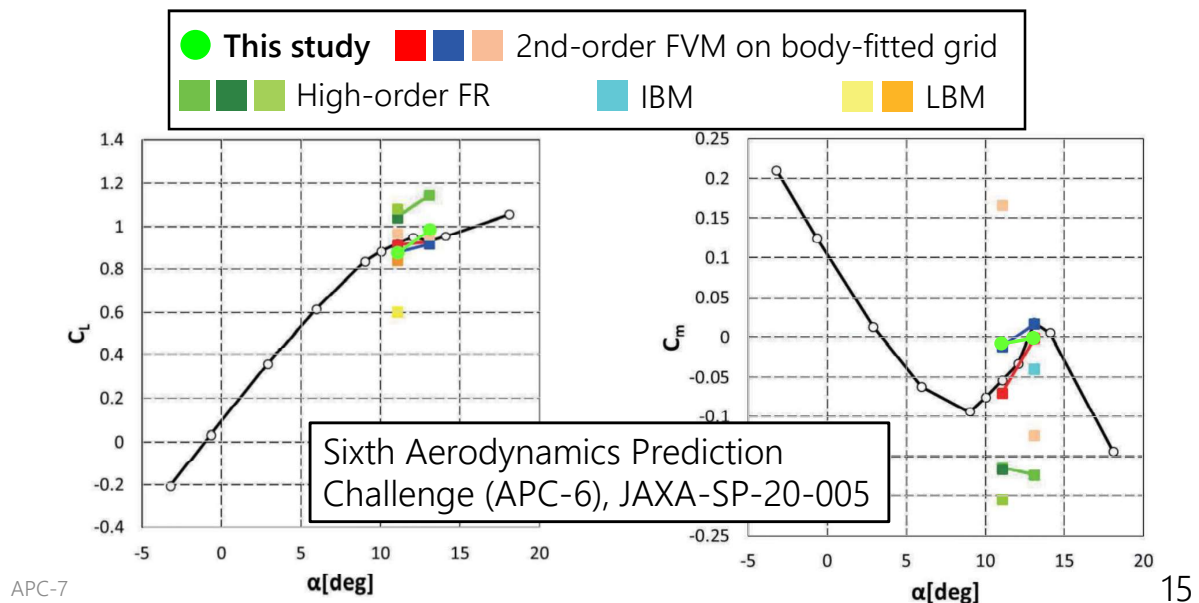
## Case 2

## Unsteady Simulation

## Comparison of aerodynamics coefficients



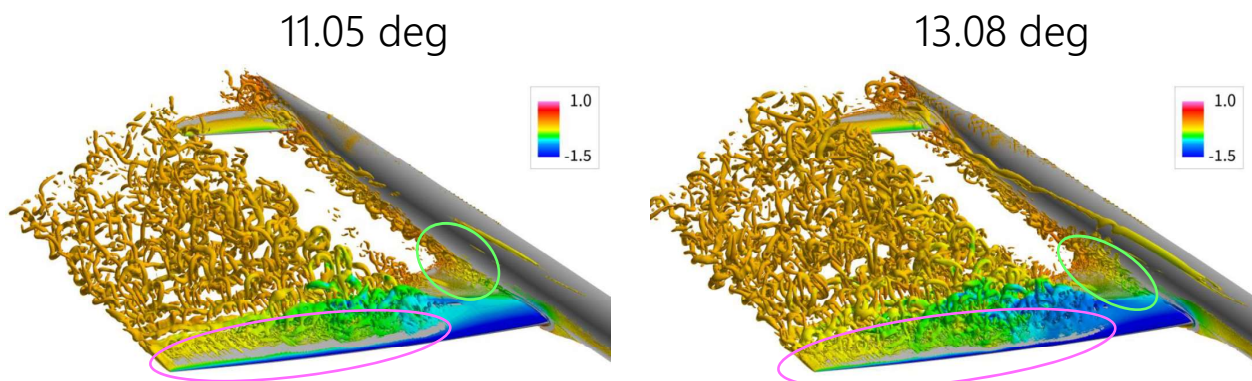
- Reasonable prediction of  $CL$  and  $CM$ .
- Similar results to simulations of 2nd-order FVM on body-fitted grids.



## Q criterion



- Massive flow separation on main wing.
- Position of leading edge separation moves upstream as AoA increases.
- Vortices from wing-body junction.
  - Interfering with tail wing.





# Conclusion



**Turbulent flow simulation around NASA-CRM was conducted by using UTCart and Recursive Fitting Method.**

- Automatic grid generation based on Cartesian grids.
  - Geometric features are approximately represented.
  - Conservation laws are satisfied.
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- In steady simulation,  $CL$  and  $CM$  of Recursive Fitting method are closer to exp. than those of Immersed Boundary method.
  - Reasonable prediction of unsteady aerodynamic coefficients
    - similar to those of 2nd-order FVM on conventional body-fitted grid.

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# Appendix

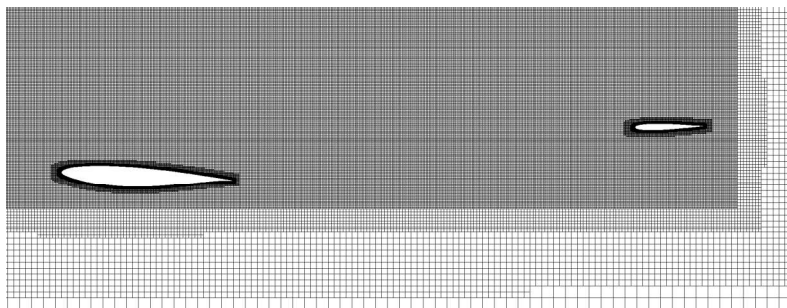
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## Details of grid setting

- Grid size
  - Main wing, tail :  $0.00153 C_{MAC}$
  - Body :  $0.00306 C_{MAC}$
  - Wake :  $0.0122 C_{MAC}$
- Domain size:  $200C_{MAC} \times 200C_{MAC} \times 200C_{MAC}$
- Time for grid generation
  - Immersed Boundary (APC-6): 31 min.
  - Recursive Fitting Method (This study) : 49 min.



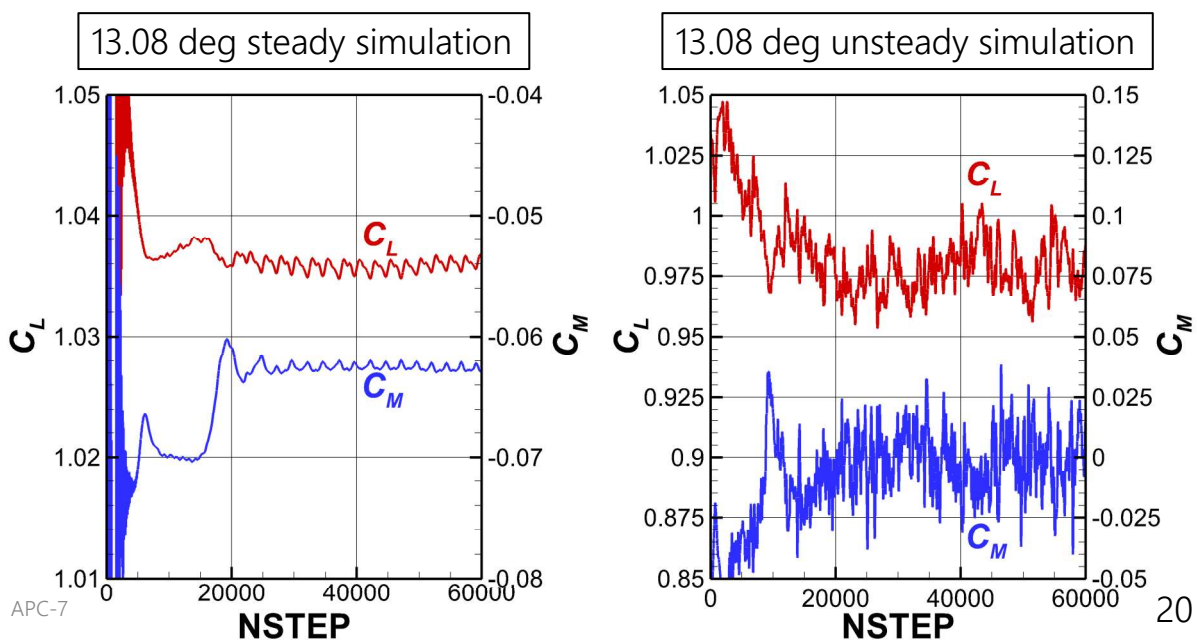
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## Time histories of $C_L$ and $C_M$

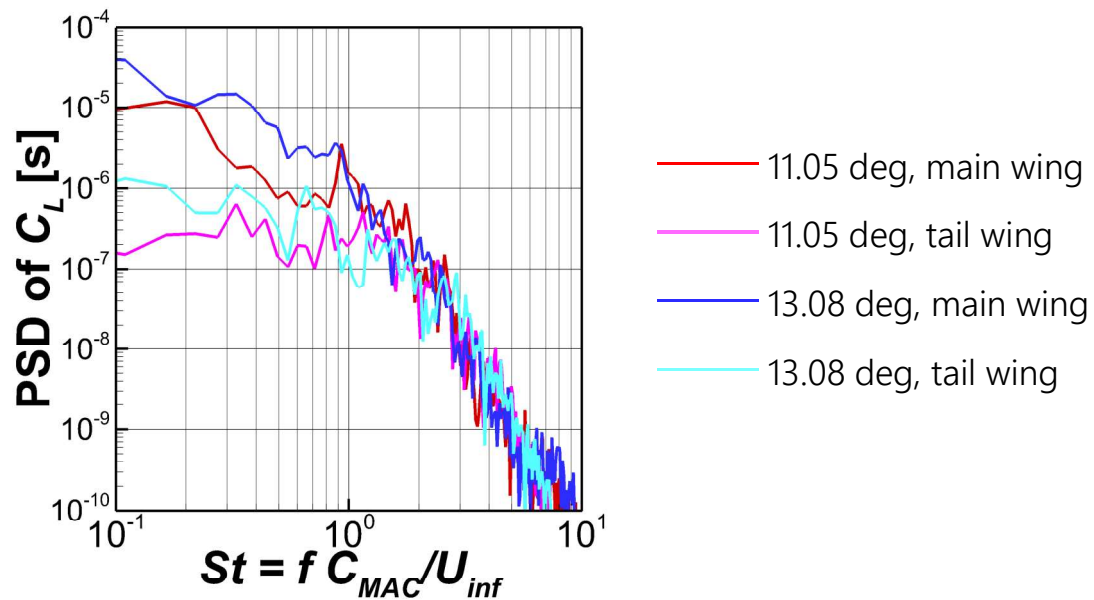
- Initial conditions
  - Steady: Free stream conditions.
  - Unsteady: results of steady RANS simulation.





## PSD of Lift coefficient (Unsteady)

- PSD becomes large as AoA increases.
- Peak of PSD of main wing around  $St \sim 1$  in simulation at  $AoA = 11.05$  deg.



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