

C18

## レーザーアブレーションを用いたマルチデオービットの相対軌道設計 Formation Flying Design for Multi-deorbit Using Laser Ablation

○五十部駿, 正木翔, 吹井柊太, 吉村康広, 花田俊也 (九州大学),  
板谷優輝, 藤原智章, 福島忠徳 (スカパーJSAT 株式会社)

○ISOBE Shun, MASAKI Kakeru, FUKII Shuta, YOSHIMURA Yasuhiro, HANADA Toshiya (Kyushu University),  
ITAYA Yuki, FUJIHARA Tomoaki, FUKUSHIMA Tadanori (SKY Perfect JSAT Corporation)

能動的デブリ除去の一つに、レーザー照射により表面から放出する物質の反作用を利用する手法がある。このレーザーアブレーションを用いたデブリ除去ミッションでは、デブリに非接触であるため安全性が高い。さらに取付デバイスや燃料を必要としないため、単一のターゲットを軌道離脱するだけでなく、複数のターゲットを同時に軌道離脱するマルチデオービットへの拡張が見込まれる。本発表では、ターゲットの近傍軌道へランデブー後の軌道離脱フェーズにおける、サービス衛星と複数ターゲットのフォーメーションを提案する。レーザー照射時間、衝突回避性能を評価指標とし、レーザーシステムの制約を満たす2つのフォーメーションを設計する。またサービス衛星の姿勢変更を伴うフォーメーションを含む2つの案について検討を行う。

To remediate the orbital environment, active debris removal (ADR) from low Earth orbit is required. Laser ablation is a vital technology for contactless active debris removal, where a service satellite irradiates laser pulses to a target satellite to generate the ablation force for deorbiting. Since the ADR method using a laser requires no deorbiting device to attach, the ADR by laser enables simultaneously deorbiting multi-targets, which is a promising ADR technology. As a preliminary study of multi-deorbit, this paper designs the formation with respect to multi targets to maximize the laser duration or minimize collision probability. Furthermore, the laser system has significant constraints such as laser focal length, laser irradiating angle, and camera angle. Thus, the designed formations must satisfy the constraints of the laser system. To this end, two formations that require attitude control or no attitude control are proposed. Their performances are compared in terms of safety and deorbit efficiency.

Nov. 30, 2022

# C18. Formation Flying Design For Multi-Deorbit Using Laser Ablation

## レーザアブレーションを用いた マルチデオービットの相対軌道設計

Shun Isobe<sup>1)</sup>, Kakeru Masaki<sup>1)</sup>, Shuta Fukii<sup>1)</sup>, Yasuhiro Yoshimura<sup>1)</sup>, Toshiya Hanada<sup>1)</sup>  
Yuki Itaya<sup>1) 2)</sup>, Tomoaki Fujihara<sup>2)</sup> and Tadanori Fukushima<sup>2)</sup>  
(<sup>1)</sup> Kyushu University, (<sup>2)</sup> SKY Perfect JSAT Corporation)

五十部駿<sup>1)</sup>, 正木翔<sup>1)</sup>, 吹井柁太<sup>1)</sup>, 吉村康広<sup>1)</sup>, 花田俊也<sup>1)</sup>  
板谷優輝<sup>1) 2)</sup>, 藤原智章<sup>2)</sup>, 福島忠徳<sup>2)</sup>  
(<sup>1)</sup> 九州大学, (<sup>2)</sup> スカパーJSAT株式会社)

Wednesday, November 30<sup>th</sup>, 2022  
10<sup>th</sup> Space Debris Workshop

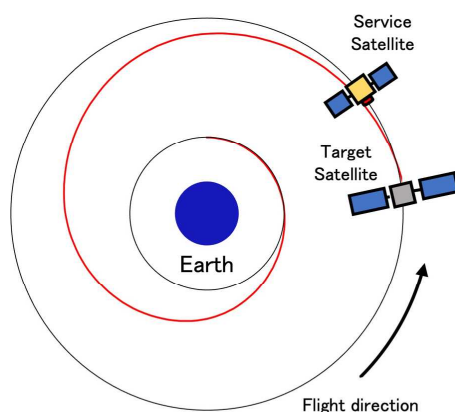


九州大学

KYUSHU UNIVERSITY Formation flying design for multi-deorbit using laser ablation 1

1. Background 2. Preliminaries 3. Design 4. Evaluation and Conclusion

### Deorbit service using laser ablation



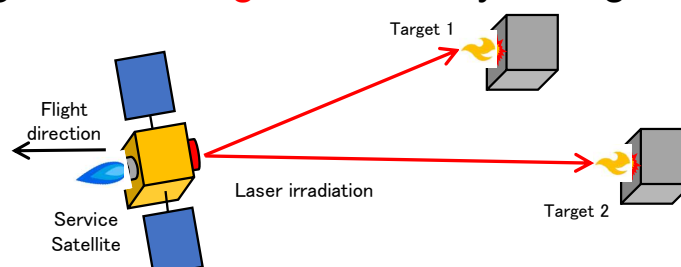
#### Mission Scenario

Descent altitude using force generated by laser ablation

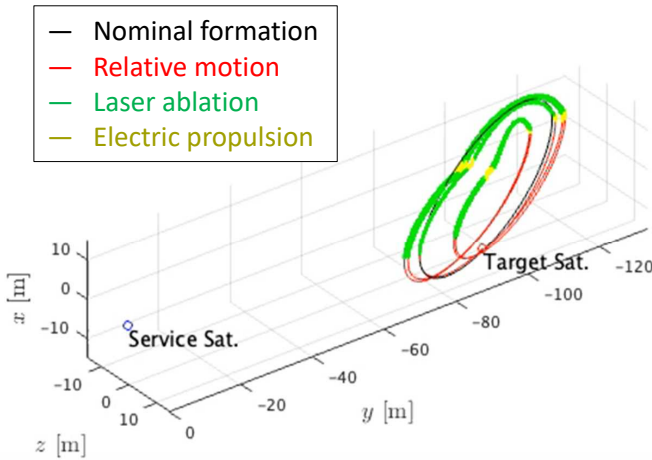
#### Advantages [1,2]

- Contactless debris removal
- Adaptability to Tumbling Objects
- No need to carry deorbit fuel

➡ Extending to **multi-target** deorbit by a single service satellite



## Deorbit Phase



Relative motion respect to the service satellite

### Nominal formation

- The relative motion periodically returns to the nominal formation.
- Forming the nominal formation when not irradiating the laser.

### Outcome of this research

Nominal formation design and evaluation for multi-deorbit using laser ablation

## Relative motion [3,4]

### Relative Orbital Elements (ROE)

$$\begin{bmatrix} \delta a \\ \delta \lambda \\ \delta e_x \\ \delta e_y \\ \delta i_x \\ \delta i_y \end{bmatrix} = \begin{bmatrix} (a_d - a)/a \\ (u_d - u) + (\Omega_d - \Omega) \cos i \\ e_{xd} - e_x \\ e_{yd} - e_y \\ i_d - i \\ (\Omega_d - \Omega) \sin i \end{bmatrix}$$

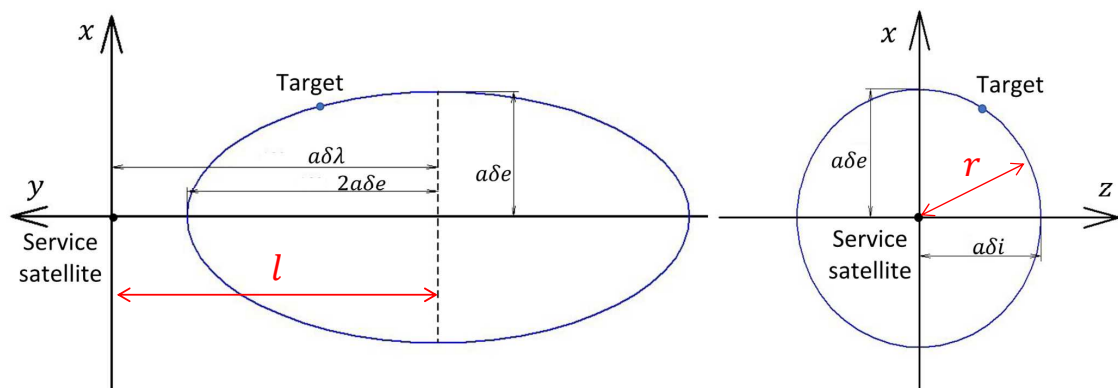
### Safety Ellipses

- Bounded in-plane motion
- Target doesn't intersect the tangential axis.

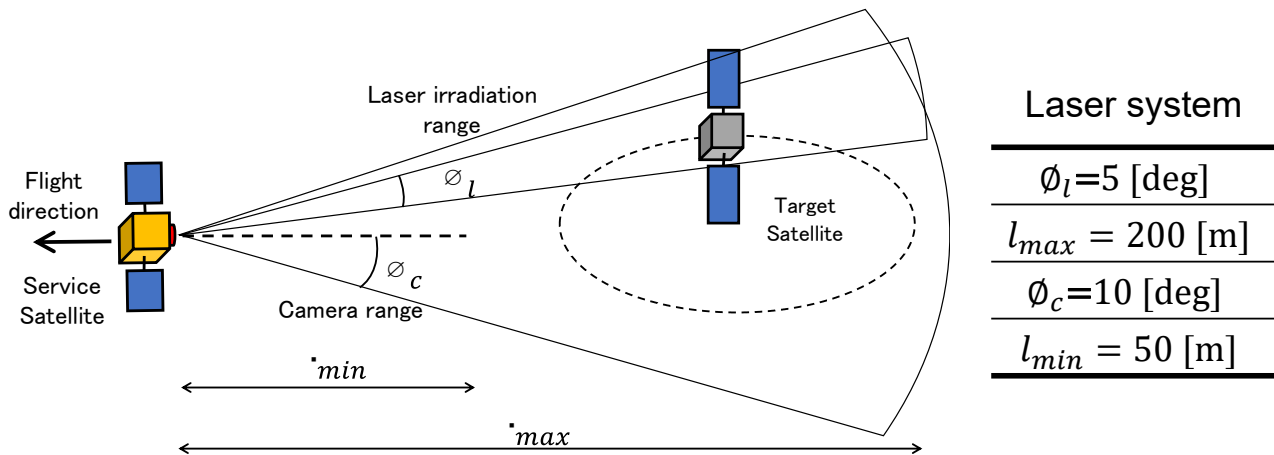
### In this research

$$a\delta a = 0 \quad \delta \mathbf{e} \parallel \delta \mathbf{i} \quad a\delta \lambda = l \quad a\delta e = a\delta i = r$$

Formation parameters =  $l, r$



## Constraint



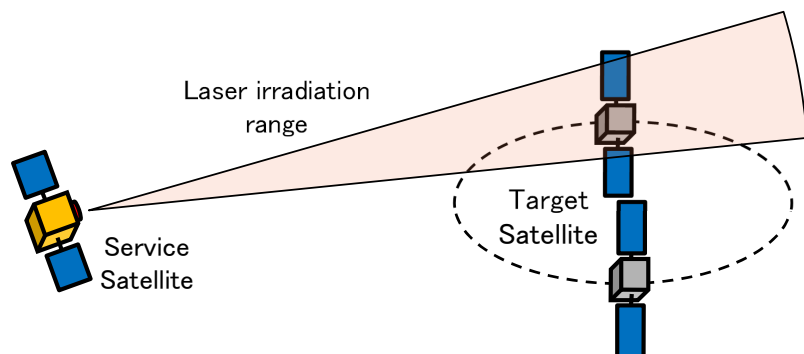
- Always capturing the targets by the camera
- Limited laser and camera range

➔ Evaluate the closest distance and laser irradiation time

## Design Policy

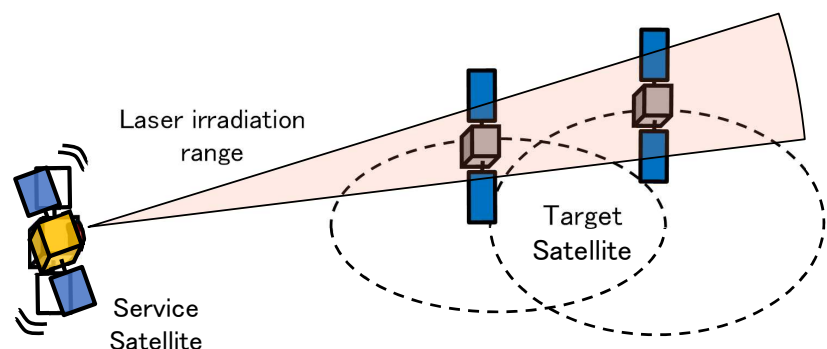
### Formation 1

- Same relative orbit
- One by one irradiating laser
- No attitude control

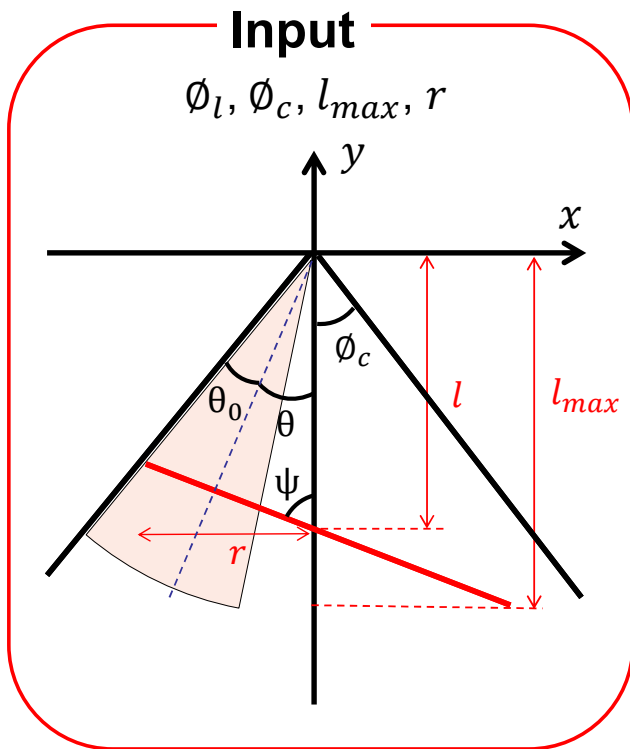


### Formation 2

- Different relative orbit
- Always irradiating laser
- Need attitude control



### Formation 1



**output**

$l, \theta$

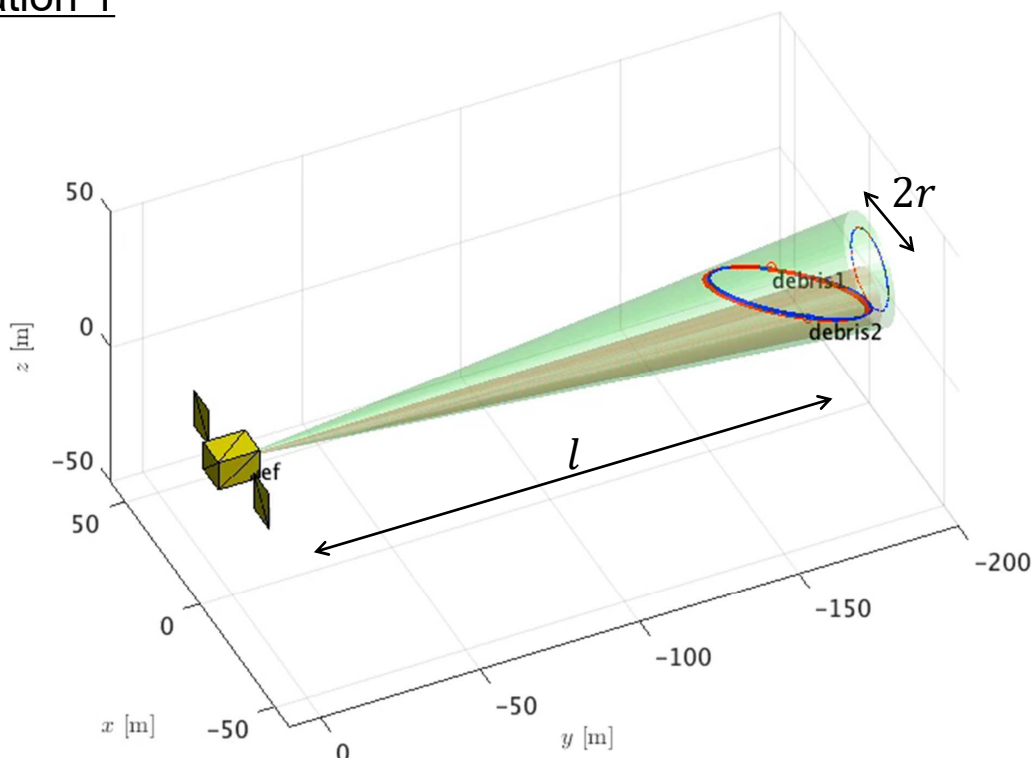
$$r_{max} = \frac{\tan \phi_c}{1 + 4 \tan \phi_c} l_{max} \quad l = l_{max} - 2r$$

$$\theta = \frac{-\text{atan} \left( \frac{l \sqrt{-l^2 \tan(\theta_0)^2 + 4 r^2 \tan(\theta_0)^2 + r^2 + 2 r^2}}{l^2 - 4 r^2} \right)}{\text{atan} \left( \frac{l \sqrt{-l^2 \tan(\theta_0)^2 + 4 r^2 \tan(\theta_0)^2 + r^2 - 2 r^2}}{l^2 - 4 r^2} \right)} \quad \theta_0 = \frac{\phi_l}{2}$$

**Result**

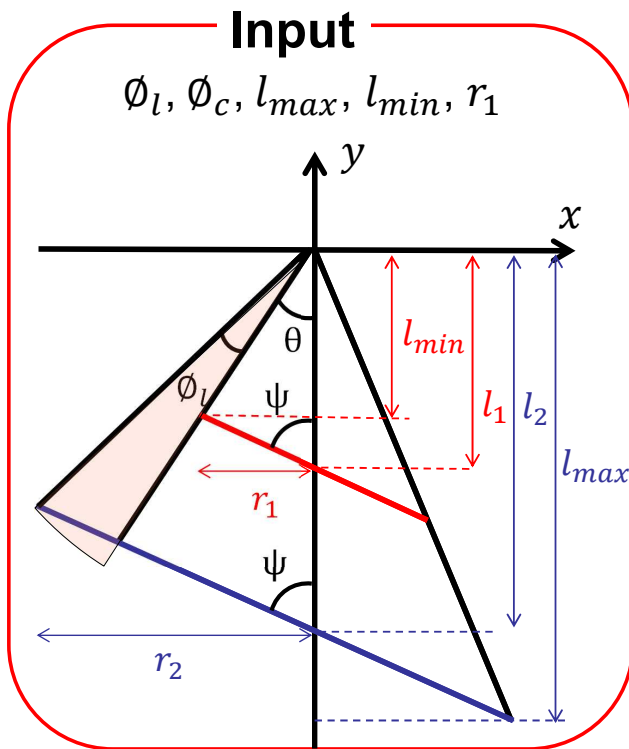
$r$ [m]	12.0
$l$ [m]	176.0
$\theta$ [deg]	2.53
laser irradiation time [%]	27.2
closest distance [m] (in RN plane )	24.0 (24.0)

### Formation 1





## Formation 2



## output

$r_2, l_1, l_2$

$$r_2 = \frac{l_{max}}{1 + \frac{2r_1}{l_{min} + 2r_1}(1 + W)} r_1 \quad \begin{cases} W = \frac{\sin \phi_l \sin \psi}{\sin \theta \sin(\phi_l + \theta + \psi)} \\ \theta = \arctan \frac{r_1}{l_{min}} \\ \psi = \arctan \frac{1}{2} \end{cases}$$

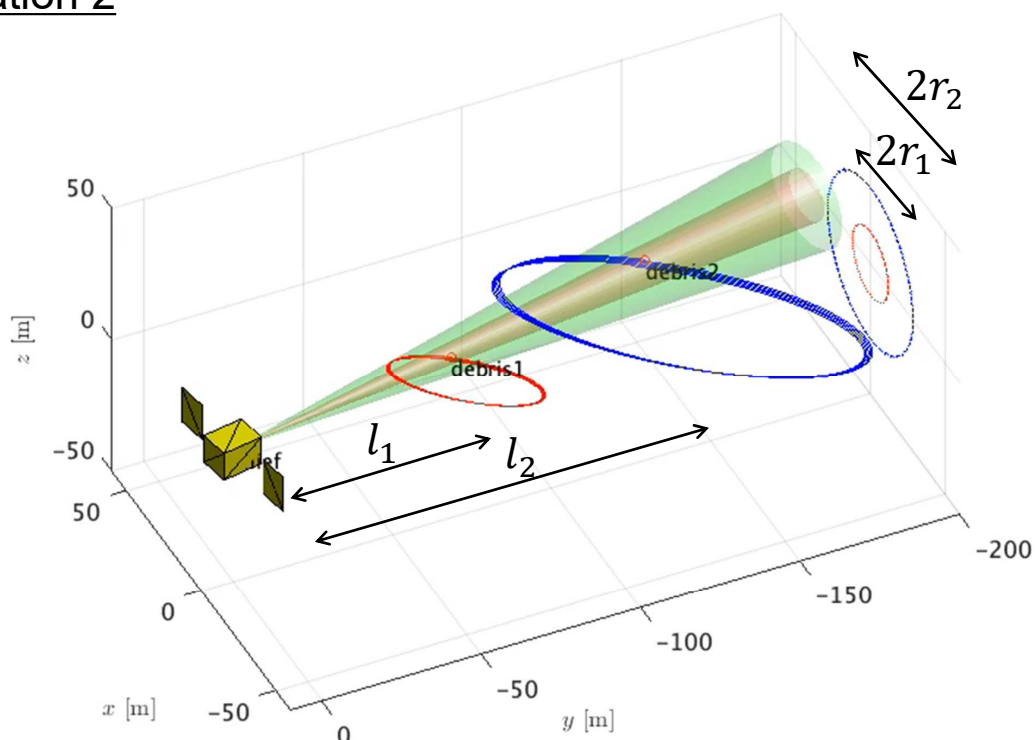
$$l_1 = l_{min} + 2r_1 \quad l_2 = l_{max} - 2r_2$$

## Result

$r_1$ [m]	12.0
$l_1$ [m]	74.0
$r_2$ [m]	28.6
$l_2$ [m]	142.8
laser irradiation time[%]	100.0
closest distance [m] (in RN plane)	39.2 (16.6)

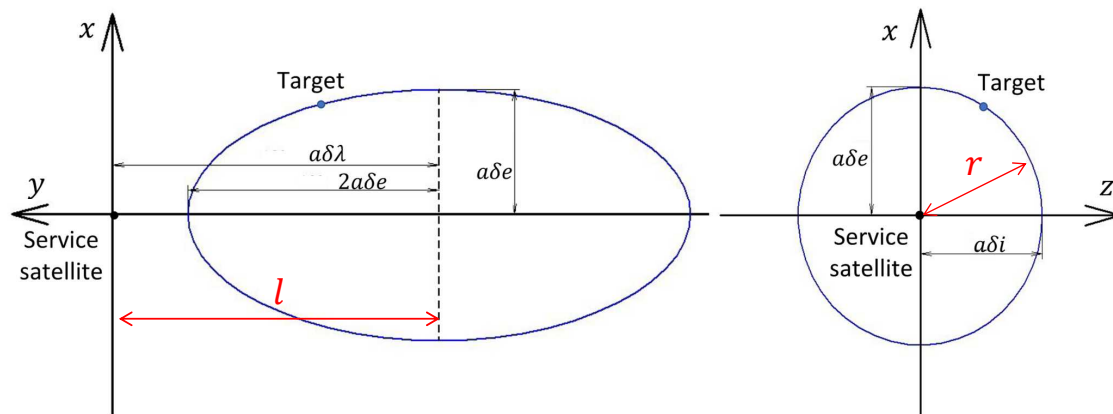


## Formation 2



## Evaluation

	Result	
	Formation 1	Formation 2
$r_1$ [m]	9.0 – 12.9	5.0 – 21.0
laser irradiation time [%]	40.5 – 25.0	100
closest distance [m] (in RN plane )	18.0 – 26.0 (18.0 – 25.8)	70.0 – 19.3 (16.5 – 12.9)



## Conclusion

- As the first step of multi-deorbit, this research designed two nominal formations.  
Formation 1 → No attitude control  
Formation 2 → Need attitude control
- Formation 2 has longer laser irradiation time and better collision avoidance performance.
- The user should select the formation based on whether or not attitude control.

### Future works

- Orbit Control for configuration of the formation
- Analysis of safety between non-cooperating objects



## References

- [1] Fukushima, T., Hirata, D., Adachi, K., Itaya, Y., Yamada, J., Tsuno, K., Ogawa, T., Saito, N., Sakashita, M., & Wada, S. (2021). *End-of-Life Deorbit Service with a Pulsed Laser Onboard a Small. April*, 20–23.
- [2] Shirasawa, Y., Komatsu, Y., Tsutsui, Y., Katsumata, H., & Wada, A. (2021). *Concept Study of Spacecraft System for End-of-Life Deorbit Service Using Low-Thrust Formation. April*, 20–23.
- [3] D'Amico, S. (2005). Relative Orbital Elements as Integration Constants of Hill's Equations. *Space Flight Technology, German Space Operations Center*, 1, 3–12.
- [4] Guffanti, T., D'Amico, S., & Lavagna, M. (2017). Long-term analytical propagation of satellite relative motion in perturbed orbits. *Advances in the Astronautical Sciences*, 160, 2387–2417.
- [5] Tsuno, K., Wada, S., Ogawa, T., Ebisuzaki, T., Fukushima, T., Hirata, D., Yamada, J., & Itaya, Y. (2020). Impulse measurement of laser induced ablation in a vacuum. *Optics Express*, 28(18), 25723. <https://doi.org/10.1364/oe.399119>